

This program was made for calculation of Cp,Cq  
of windmill which we made , so if you want to  
calculate Cp,Cq of another windmill , you must  
change call statement's parameter and SUBROUTINE  
CLCD .

```
*****
DIMENSION R(51),C(51),SOL(51),FAI(51),A0(51),B0(51),CQ(20)
DIMENSION ALD(51),ALPHA1(51),A(51),B(51),CP(20),XXX(20)
PARAMETER (ALPHA0=4.0)
```

```
1  WRITE(5,*) ' DESIGN X=? '
   READ(5,*) XX0
   WRITE(5,*)
   WRITE(5,*) ' NUMBER OF DIVISION ? '
   READ(5,*) ND
   WRITE(5,*)
   WRITE(5,*) ' PITCH ANGLE ? '
   READ(5,*) PA
   WRITE(5,*) ' DO YOU NEED GRAPH OF ALPHA,a,b ? '
   READ(5,*) NG

   CALL SFAI(XX0,ALPHA0,8,97.5,0.06,125.0,625.0,ND,R,C,SOL,
J      FAI,ALD,A0,B0,1)

   IF(NG.NE.1) GO TO 150
   CALL GRAPH1('r',5,2,125.0,625.0,'ALPHA',7,2,-20.0,50.0)
   DO 5 I=1,8
   XX=REAL(I)*0.5
   CALL ALPAB(XX,ND,R,SOL,ALD,PA,ALPHA1,A,B)
   IF(I.EQ.8) THEN
   NC=1
   ELSE
   NC=2
   END IF
   CALL GRAPH2(51,R,ALPHA1,0,1,NC)
5  CONTINUE
   CALL PSPACE(1)

   CALL GRAPH1('r',5,2,125.0,625.0,'a',3,2,0.0,0.3)
   DO 10 I=1,8
   XX=REAL(I)*0.5
   CALL ALPAB(XX,ND,R,SOL,ALD,PA,ALPHA1,A,B)
   IF(I.EQ.8) THEN
   NC=1
   ELSE
   NC=2
   END IF
   CALL GRAPH2(51,R,A,0,1,NC)
10 CONTINUE
   CALL PSPACE(1)

   CALL GRAPH1('r',5,2,125.0,625.0,'b',10,2,0.0,1.0)
   DO 20 I=1,8
   XX=REAL(I)*0.5
   CALL ALPAB(XX,ND,R,SOL,ALD,PA,ALPHA1,A,B)
```

```

IF(I.EQ.8) THEN
NC=1
ELSE
NC=2
END IF
20  CALL GRAPH2(51,R,B,0,1,NC)
    CONTINUE
    CALL PSPACE(4)

150  CALL PRON
    CALL SPACE(5,2)
    WRITE(5,200) XX0,PA
200  FORMAT('          X=',F3.1,'          PITCH ANGLE=',F5.1)
    CALL PROFF

DO 30 I=1,20
XXX(I)=REAL(I)*0.2
CALL ALPAB(XXX(I),50,R,SOL,ALD,PA,ALPHA1,A,B)
CALL IITA(XXX(I),50,R,A,B,CP(I),CQ(I))
30  CONTINUE
    CALL PSPACE(2)
    CALL GRAPH1('X',5,2,0.0,5.0,'CP',4,2,0.0,0.4)
    CALL GRAPH2(20,XXX,CP,0,1,1)
    CALL PSPACE(10)
    CALL GRAPH1('X',5,2,0.0,5.0,'CQ',4,2,0.0,0.4)
    CALL GRAPH2(20,XXX,CQ,0,1,1)
    CALL PSPACE(11)
    CALL PRON
    CALL SPACE(5,10)
    DO 40 I=1,20
    WRITE(5,*)
    WRITE(5,100) XXX(I),CP(I),CQ(I)
40  CONTINUE
100  FORMAT('          X=',F3.1,'          CP=',F6.3,'          CQ=',F6.3)
    CALL SPACE(5,16)
    CALL PROFF
    WRITE(5,*) ' CONTINUE ?  1---YES  2---NO'
    READ(5,*) IC
    IF(IC.EQ.1) GO TO 1
END

```

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\*\*\*\*\* PROGRAM FOR CALCULATION OF TWIST ANGLE OF BLADE \*\*\*\*\*

SUBROUTINE SFAI (XX,ALPHA0,NB,C1,C2,RR,RT,NN,R,C,SOL, 86  
 FAI,ALD,A,B,KK)

--INPUT--

XX : Design tip speed ratio  
 ALPHA0 : Attack angle at maximum L/D  
 NB : Number of blade  
 C1,C2 :  $C(R)=C1-C2*R$  (mm)  
 RR : Radius from center of windmill to cone of blade  
 RT : Radius from center of windmill to tip of blade  
 NN : Number of division (radius)

--OUTPUT--

R : Radius (mm)  
 C : Chord length (mm)  
 SOL : Solidity  
 FAI : Angle between plane of rotation and relative  
 flow velocity in the plane of rotation  
 ALD : Design angle of blade  
 A : Axial interference factor  
 B : Tangential interference factor  
 KK : Choice for display 1-- show 2-- not show

J SUBROUTINE SFAI (XX,ALPHA0,NB,C1,C2,RR,RT,NN,R,C,SOL,  
 FAI,ALD,A,B,KK)

DIMENSION R(NN+1),C(NN+1),SOL(NN+1),X(100),ALD(NN+1)  
 DIMENSION Z1(89),Z2(11),Z3(500),A(NN+1),B(NN+1),FAI(NN+1)  
 CHARACTER STAR(100)\*1  
 PARAMETER (PAI=3.141593)

CALL CLCD(ALPHA0,CL,CD)

M=NN+1

STEP=(RT-RR)/REAL(NN)

DO 1 I=1,100

STAR(I)=' '

1 CONTINUE

DO 10 I=1,M

R(I)=STEP\*REAL(I)+RR-STEP

C(I)=C1-C2\*R(I)

SOL(I)=NB\*C(I)/(2.0\*PAI\*R(I))

X(I)=XX\*R(I)/RT

10 CONTINUE

DO 60 I=1,M

A1=SOL(I)\*X(I)\*CL-SOL(I)\*CD

A2=SOL(I)\*X(I)\*CD+SOL(I)\*CL

DO 20 L1=1,89

PP=REAL(L1)

PR=PAI\*PP/180.0

Z1(L1)=(A1-4.0\*COS(PR))\*TAN(PR)+4.0\*X(I)\*COS(PR)+A2

IF(Z1(L1).LT.0.0) GO TO 100

20 CONTINUE

GO TO 200

100 DO 30 L2=1,11

PP=REAL(L1)+REAL(L2)/10.0-1.1

PR=PAI\*PP/180.0

Z2(L2)=(A1-4.0\*COS(PR))\*TAN(PR)+4.0\*X(I)\*COS(PR)+A2

IF(Z2(L2).LT.0.0) GO TO 300

30 CONTINUE

```

200 PR=PAI*40.0/180.0
Z3(1)=(A1-4.0*COS(PR))*TAN(PR)+4.0*X(I)*COS(PR)+A2
DO 40 L3=2,500
PP=REAL(L3)/10.0+39.9
PR=PAI*PP/180.0
Z3(L3)=(A1-4.0*COS(PR))*TAN(PR)+4.0*X(I)*COS(PR)+A2
IF((Z3(L3)-Z3(L3-1)).GE.0.0) GO TO 50
40 CONTINUE
50 FAI(I)=REAL(L3)/10.0+39.8
STAR(I)='*'
GO TO 500

300 PP=REAL(L1)+REAL(L2)/10.0-1.15
PR=PAI*PP/180.0
Z4=(A1-4.0*COS(PR))*TAN(PR)+4.0*X(I)*COS(PR)+A2
IF(Z4.GE.0.0) THEN
FAI(I)=REAL(L1)+REAL(L2)/10.0-1.1
ELSE
FAI(I)=REAL(L1)+REAL(L2)/10.0-1.2
END IF
ALD(I)=FAI(I)+ALPHA0

500 PR=PAI*FAI(I)/180.0
E=4.0*COS(PR)+SOL(I)*(CL*TAN(PR)+CD)
A(I)=SOL(I)*(CL*TAN(PR)+CD)/E
B(I)=SOL(I)*(CL-CD*TAN(PR))/(X(I)*E)
CALL DISPLY(KK,RR,R(I),FAI(I),A(I),B(I),STAR(I))
60 CONTINUE
RETURN
END

SUBROUTINE DISPLY(KK,RR,R,FAI,A,B,S)
CHARACTER S*1
GO TO (10,20) KK
10 IF((ABS(R-RR)).LT.0.001) WRITE(5,*) ' '
WRITE(5,*) R,FAI,A,B,S
20 RETURN
END

```

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SUBROUTINE CLCD(A,CL,CD)

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--INPUT--

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A : Effective attack angle

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--OUTPUT--

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CL : Lift coefficient

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CD : Drag coefficient

```

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*****
SUBROUTINE CLCD(A,CL,CD)
DIMENSION CLO(22),CDO(22)
DATA CLO/-.2269,-.1647,-.115,-.0528,.0653,.2393,.3947,
J .5253,.631,.7055,.805,.8485,.8672,.805,.7397,.6869,.6496,
J .6434,4*.631/
DATA CDO/.0622,.0528,.0404,.0342,.028,.028,.028,.0249,
J .0249,.0289,.0398,.0522,.0746,.0964,.1181,.1337,.1492,
J .1616,.1741,.1865,.2145,.2424/
IF (A.LT.-12.0) THEN
C0=-12.0-A
C1=(CLO(2)-CLO(1))/2.0
C2=(CDO(2)-CDO(1))/2.0
CL=CLO(1)-C1*C0
CD=CDO(1)-C2*C0
RETURN
ELSE IF (A.GE.30.0) THEN
C0=A-30.0
C1=(CLO(22)-CLO(21))/2.0
C2=(CDO(22)-CDO(21))/2.0
CL=CLO(22)+C1*C0
CD=CDO(22)+C2*C0
RETURN
END IF
A1=(A+14.0003)/2.
I1=INT(A1)
A2=A/2.
I2=INT(A2+0.00003)
IF(A.GE.0.0) THEN
B1=ABS(A2-REAL(I2))
ELSE
B1=1.0-ABS(A2-REAL(I2))
END IF
CL=B1*(CLO(I1+1)-CLO(I1))+CLO(I1)
CD=B1*(CDO(I1+1)-CDO(I1))+CDO(I1)
RETURN
END
*****

```

SUBROUTINE ALPAB (XX,ND,R,SOL,ALD,PA,ALPHA,A,B)

--INPUT--

XX : Tip speed ratio  
 ND : Number of division (radius)  
 R : Radius  
 SOL : Solidity  
 ALD : Designed angle of blade  
 PA : Pitch angle

--OUTPUT--

ALPHA : Effective attack angle  
 A : Axial interference factor  
 B : Tangential interference factor

```

SUBROUTINE ALPAB (XX,ND,R,SOL,ALD,PA,ALPHA,A,B)
DIMENSION R(ND+1),SOL(ND+1),ALD(ND+1),ALPHA(ND+1)
DIMENSION A(ND+1),B(ND+1)
PARAMETER (PAI=3.141593)
DO 30 I=1,ND+1
S=SOL(I)
X=XX*R(I)/R(ND+1)
AD=ALD(I)+PA
DO 10 J1=1,101
AA=81.0-REAL(J1)
BB=(AD-AA)*PAI/180.0
CALL CLCD(AA,CL,CD)
Z1=(S*X*CL-S*CD-4.0*COS(BB))*TAN(BB)
Z=Z1+4.0*X*COS(BB)+S*X*CD+S*CL
IF(Z.LE.0.0) GO TO 100
CONTINUE
10 DO 20 J2=1,11
AA=82.1-REAL(J1)-REAL(J2)/10.0
BB=(AD-AA)*PAI/180.0
CALL CLCD(AA,CL,CD)
Z1=(S*X*CL-S*CD-4.0*COS(BB))*TAN(BB)
Z=Z1+4.0*X*COS(BB)+S*X*CD+S*CL
IF(Z.LE.0.0) GO TO 200
CONTINUE
20 DO 30 J3=1,11
AA=82.15-REAL(J1)-REAL(J2)/10.0
BB=(AD-AA)*PAI/180.0
CALL CLCD(AA,CL,CD)
Z1=(S*X*CL-S*CD-4.0*COS(BB))*TAN(BB)
Z=Z1+4.0*X*COS(BB)+S*X*CD+S*CL
IF(Z.GE.0.0) THEN
ALPHA(I)=82.1-REAL(J1)-REAL(J2)/10.0
ELSE
ALPHA(I)=82.2-REAL(J1)-REAL(J2)/10.0
END IF
CALL CLCD(ALPHA(I),CL,CD)
F=ALD(I)+PA-ALPHA(I)
FR=PAI*F/180.0
E=4.0*COS(FR)+S*(CL*TAN(FR)+CD)
A(I)=S*(CL*TAN(FR)+CD)/E
B(I)=S*(CL-CD*TAN(FR))/(X*E)
CONTINUE
RETURN
END
    
```

10  
100

20  
200

30

\*\*\*\*\* PROGRAM FOR POWER COEFFICIENT \*\*\*\*\*

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SUBROUTINE IITA (XX, ND, R, A, B, CP, CQ)

--INPUT--

XX : Tip speed ratio  
 ND : Number of division (radius)  
 R : Radius  
 A : Axial interference factor  
 B : Tangential interference factor

--OUTPUT--

CP : Power coefficient  
 CQ : Torque coefficient

```

SUBROUTINE IITA (XX, ND, R, A, B, CP, CQ)
DIMENSION R (ND+1), A (ND+1), B (ND+1), F (100)
RT=R (ND+1)
RR=R (1)
STEP=(RT-RR)/REAL (ND)
DO 10 I=1, ND+1
F (I)=(1.0-A (I))*B (I)*(R (I)**3)
CONTINUE
CALL SIMP (ND, STEP, F, F1, ICODE)
CP=8.0*F1*XX**2/RT**4
CQ=CP/XX
RETURN
END
    
```

```

SUBROUTINE SIMP (N, STEP, A, RESULT, CODE)
DIMENSION A (N+1), A2 (100), A4 (100)
M2=N/2-1
M4=M2+1
IX=N/2
X=REAL (IX)
Y=REAL (N)/2.0
IF ((Y-X).GT.0.01) GO TO 30
DO 10 I=1, M2
I2=2*I+1
A2 (I)=A (I2)
CONTINUE
DO 20 I=1, M4
I4=2*I
A4 (I)=A (I4)
CONTINUE
CALL SUM (M2, A2, S2)
CALL SUM (M4, A4, S4)
S=A (1)+A (N)+2.0*S2+4.0*S4
RESULT=STEP*S/3.0
CODE=1
RETURN
30 CALL BELL (2)
WRITE (5, *) '
WRITE (5, *) ' NUMBER OF DIVISION MUST BE AN EVEN NUMBER '
CODE=2
RETURN
END
    
```

```
SUBROUTINE SUM(N,A,S)
DIMENSION A(N)
S=0.0
DO 10 I=1,N
S=S+A(I)
CONTINUE
RETURN
END
```

```
SUBROUTINE BELL(N)
LOGICAL*1 A
DATA A/π007/
DO 10 I=1,N
WRITE(5,100) A
FORMAT('+',A1)
CONTINUE
RETURN
END
```



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SUBROUTINE PSPACE(N)

N : Number of space line

SUBROUTINE SPACE(NO,NOL)

NO : Uuit number

NOL : Number of space

SUBROUTINE PRON

PRINTER ON

SUBROUTINE PROFF

PRINTER OFF

```

SUBROUTINE PSPACE(N)
CALL PRON
CALL SPACE(5,N)
CALL PROFF
RETURN
END

```

```

10 SUBROUTINE SPACE(NO,NOL)
DO 10 I=1,NOL
WRITE(NO,*)
CONTINUE
RETURN
END

```

```

100 SUBROUTINE PRON
LOGICAL*1 A
DATA A/π033/
WRITE(5,100) A,A
FORMAT('+',A1,'[5i',A1,'Ω',f)
RETURN
END

```

```

100 SUBROUTINE PROFF
LOGICAL*1 A
DATA A/π033/
WRITE(5,100) A,A
FORMAT('+',A1,'[4i',A1,'Ω',f)
RETURN
END

```

## \*\*\*\*\* GRAPH DRAWING \*\*\*\*\*

```

SUBROUTINE GRAPH1(XNM,NDX1,NDX2,X0,X1,YNM,NDY1,NDY2,Y0,Y1)

```

```

XNM ,YNM : Axis label
NDX1,NDY1 : Number of rough division
NDX2,NDY2 : Number of fine division
X0 ,Y0 : Minimum value of axis
X1 ,Y1 : Maximum value of axis

```

```

SUBROUTINE GRAPH2(N,XAR,YAR,NP,NL,NC)

```

```

N : Number of points
XAR : X-array
YAR : Y-array
NP : Marker
NL : Line type
NC : Choice for hardcopy 1---Copy 2---No copy

```

```

SUBROUTINE GRAPH1(XNM,NDX1,NDX2,X0,X1,YNM,NDY1,NDY2,Y0,Y1)
LOGICAL*1 XNM(15),YNM(15)
CALL INITGR(5)
CALL CLRTXT
CALL CLRSCR
CALL DPAPER('LIN',NDX1,NDX2,'LIN',NDY1,NDY2,'GRAY3')
CALL LNAXIS('XB',XNM,X0,X1,.TRUE.)
CALL LNAXIS('YL',YNM,Y0,Y1,.TRUE.)
RETURN
END

```

```

SUBROUTINE GRAPH2(N,XAR,YAR,NP,NL,NC)
DIMENSION XAR(N),YAR(N)
CALL PDATA(N,XAR,YAR,'L','GRAY3',NP,NL,...)
IF(NC.EQ.1) THEN
CALL CPYSCR
CALL CLRSCR
END IF
RETURN
END

```

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## APPENDIX B

### The Use of Windmills in Thailand<sup>(14)</sup>

Locally constructed horizontal axis windmills have been used for lifting water for many years. There are 3 basic types of windmills that are usually used in many areas.

#### 1. Low speed sail rotor windmill

This type of windmill has 6 or 8 triangular sails of bamboo matting or cloth mounted on bamboo poles with 6 to 8 m in diameter. The windmill is fixed in direction of prevailing wind as shown in Fig.B.1.



Fig. B.1 Low speed sail rotor windmill

This type of windmill is used for pumping sea water at salt farms, for example, in Samut Songkram and Chonburi.

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<sup>(14)</sup>Exell R. H. B., Thavapalachandran S. and Mukhia P. (1981) The Availability of Wind Energy in Thailand. AIT Research Report No. 134, p. 22.

## 2. High speed wooden rotor windmill

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This type of windmill has 2 or 4 blades which is made from a wooden plank 8 m long, 0.2 m wide and .05 m thick forming a simple airfoil with some twist. The axis of the windmill rotor is supported on a pole and it can be turned manually to face the wind as shown in Fig.B.2.



Fig.B.2 High speed wooden rotor windmill

This windmill is utilized mainly for irrigating rice fields, for example, in Chachoengsao and Pathum Thani.

## 3. Multiblade windmill

From the advantage of starting by itself at a low wind velocity, this type of windmill is becoming popular for pumping water in many areas. The windmill has 3-4 m in diameter and is fixed on a tower about 12-15 m above the ground as shown in Fig.B.3.



Fig. B. 3      Multiblade windmill

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# APPENDIX C

## Experimental Results

Figs. C.1 to C.26 show the experimental results of wind tunnel experiment.

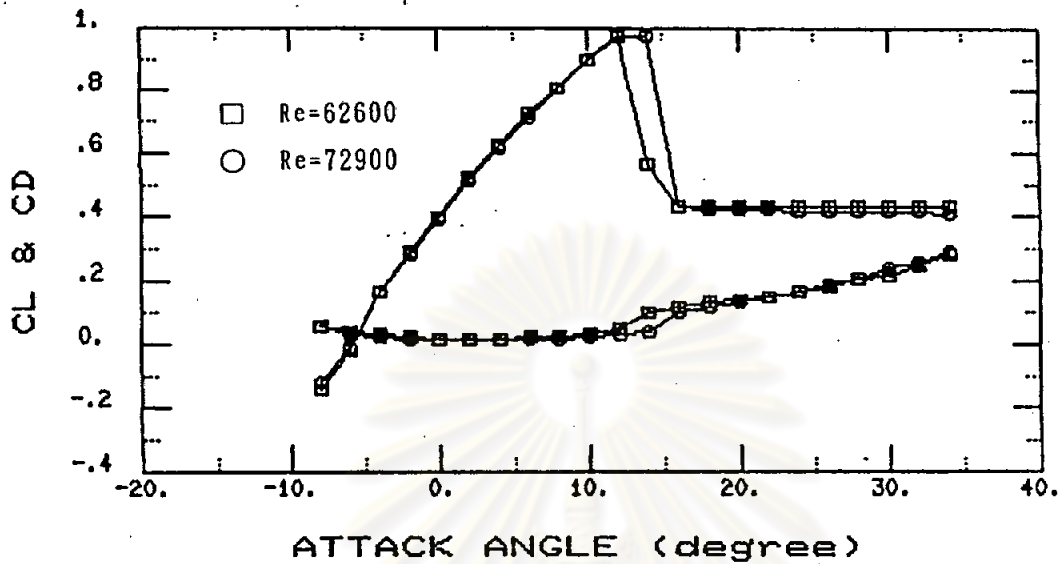


Fig. C.1 Relation of  $C_L, C_D$  vs attack angle (NACA 4418)

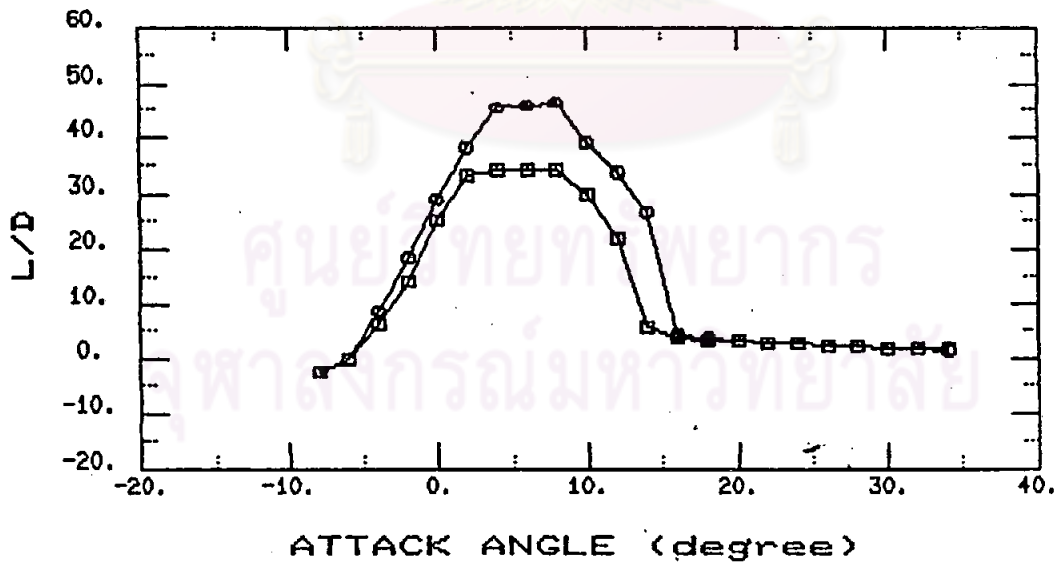


Fig. C.2 Relation of L/D ratio vs attack angle (NACA 4418)

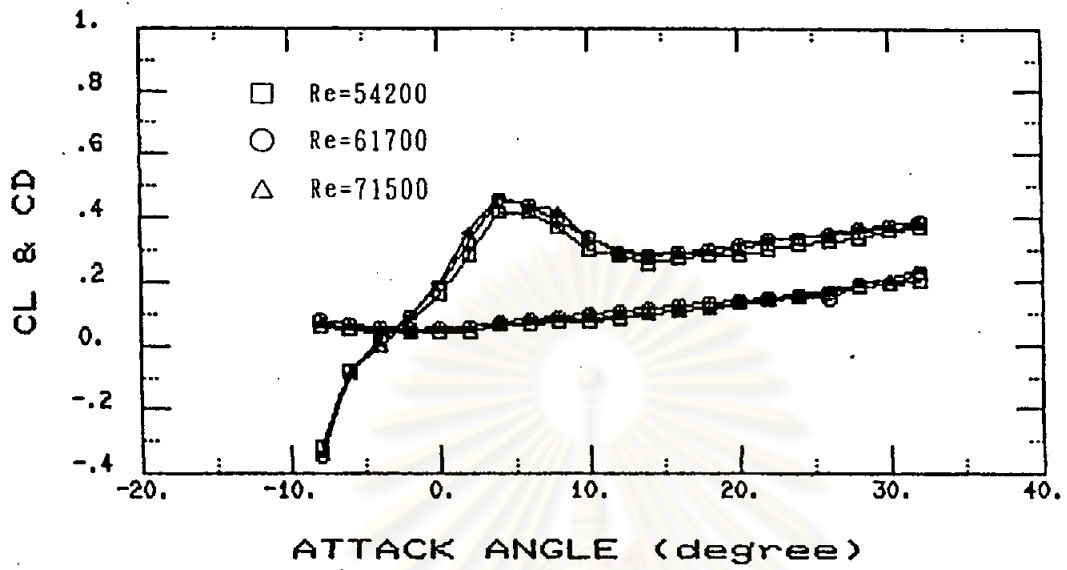


Fig. C.3 Relation of  $C_L, C_D$  vs attack angle (Straight plate)

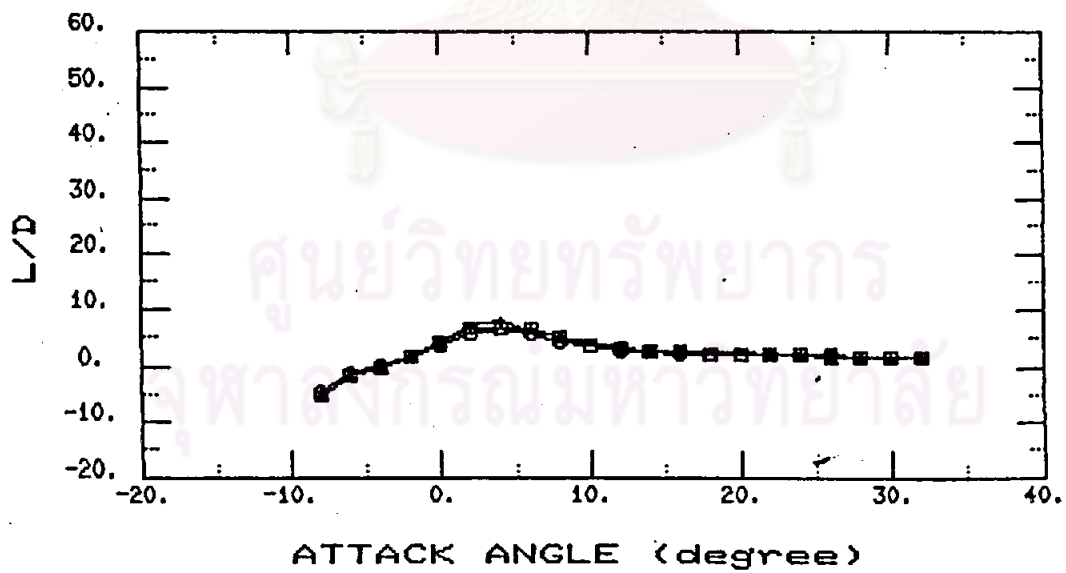


Fig. C.4 Relation of L/D ratio vs attack angle (Straight plate)

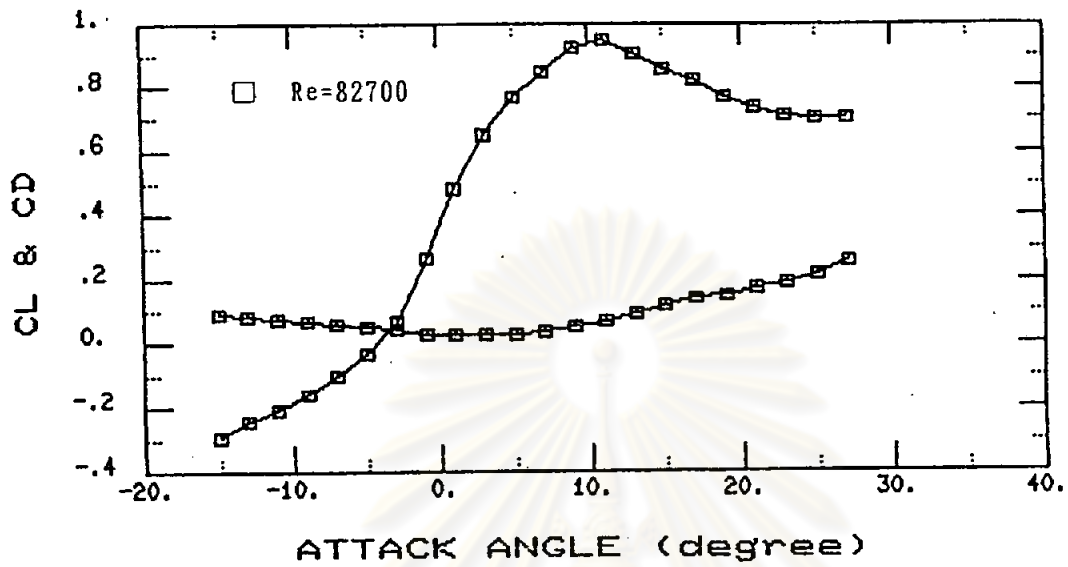


Fig. C.5 Relation of  $C_L, C_D$  vs attack angle (Arched plate No.1)

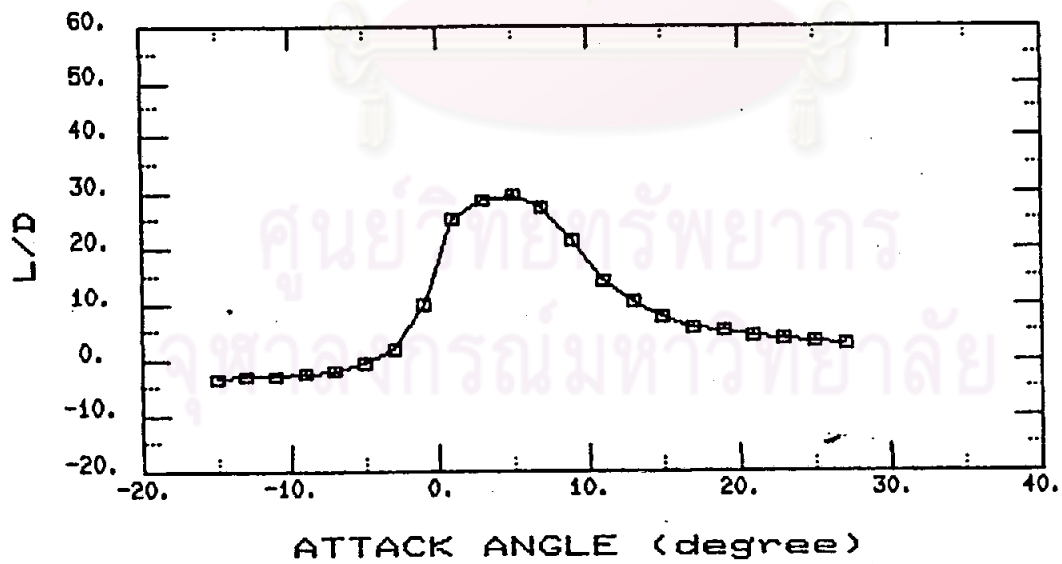


Fig. C.6 Relation of  $L/D$  ratio vs attack angle (Arched plate No.1)



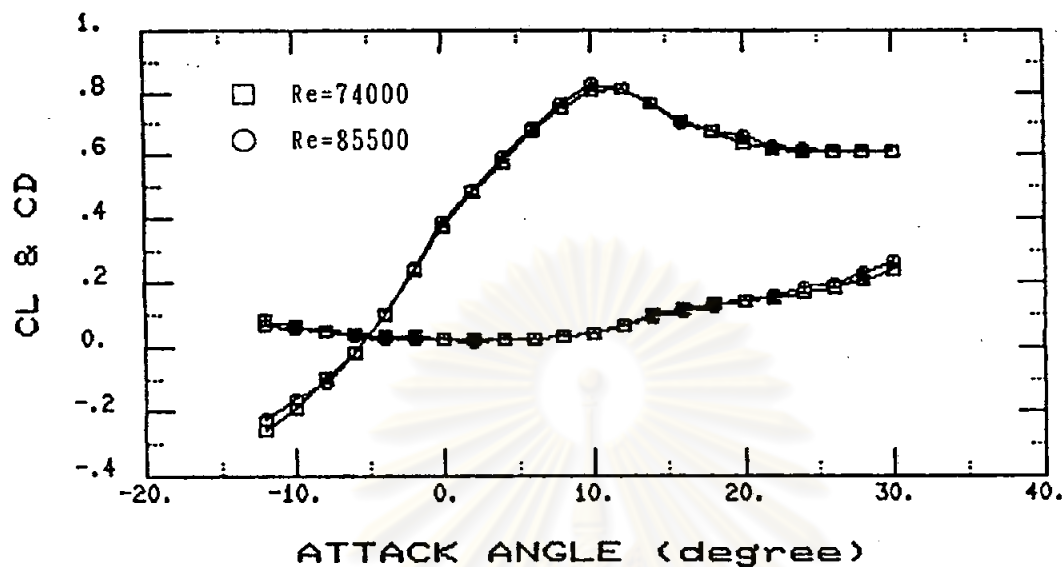


Fig. C.7 Relation of  $C_L, C_D$  vs attack angle (Arched plate No. 2)

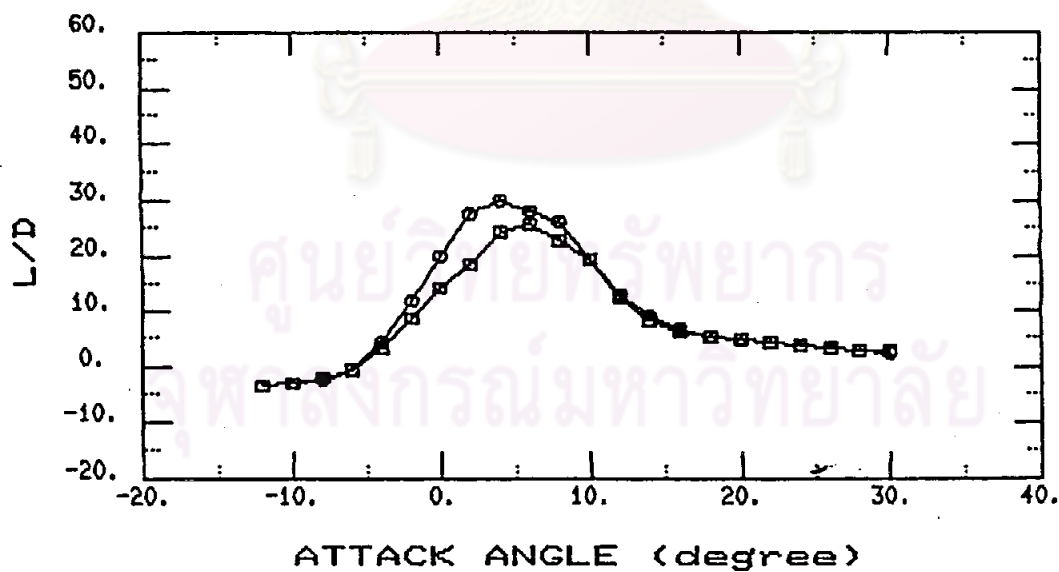


Fig. C.8 Relation of L/D ratio vs attack angle (Arched plate No. 2)

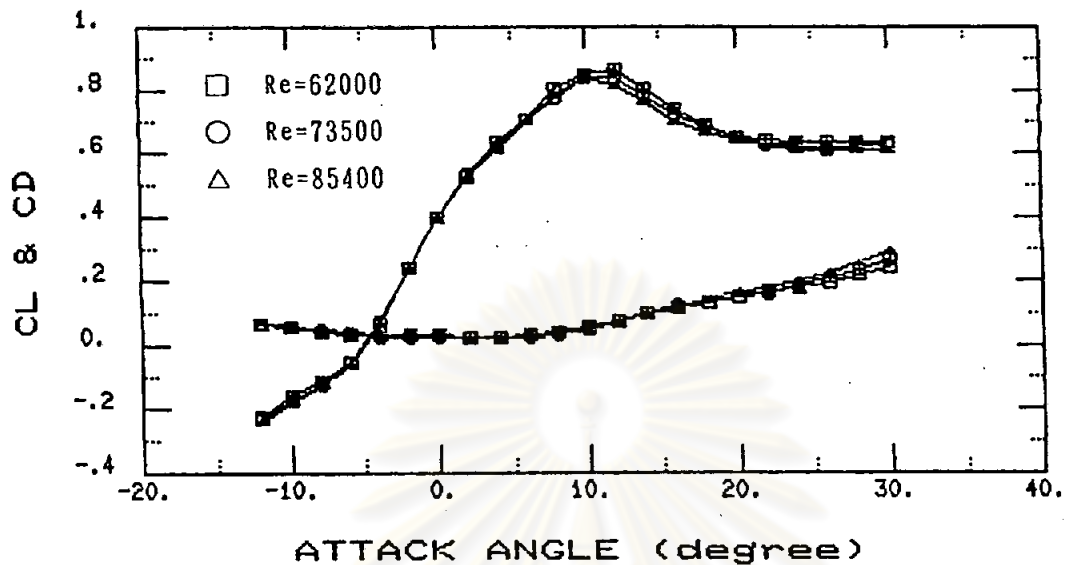


Fig. C.9 Relation of  $C_l, C_d$  vs attack angle (Arched steel plate No. 3)

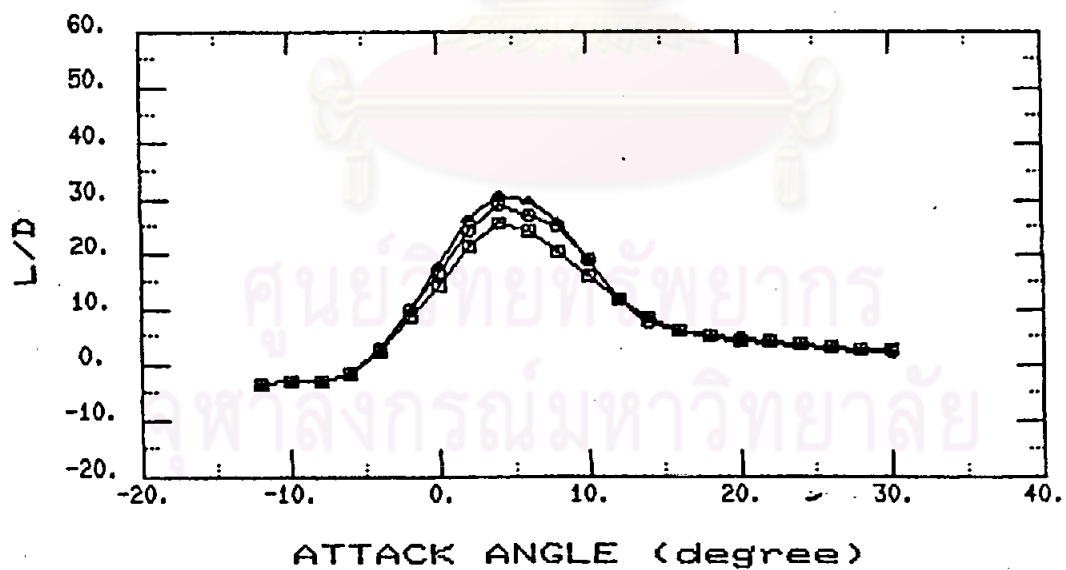


Fig.C.10 Relation of L/D ratio vs attack angle (Arched steel plate No. 3)

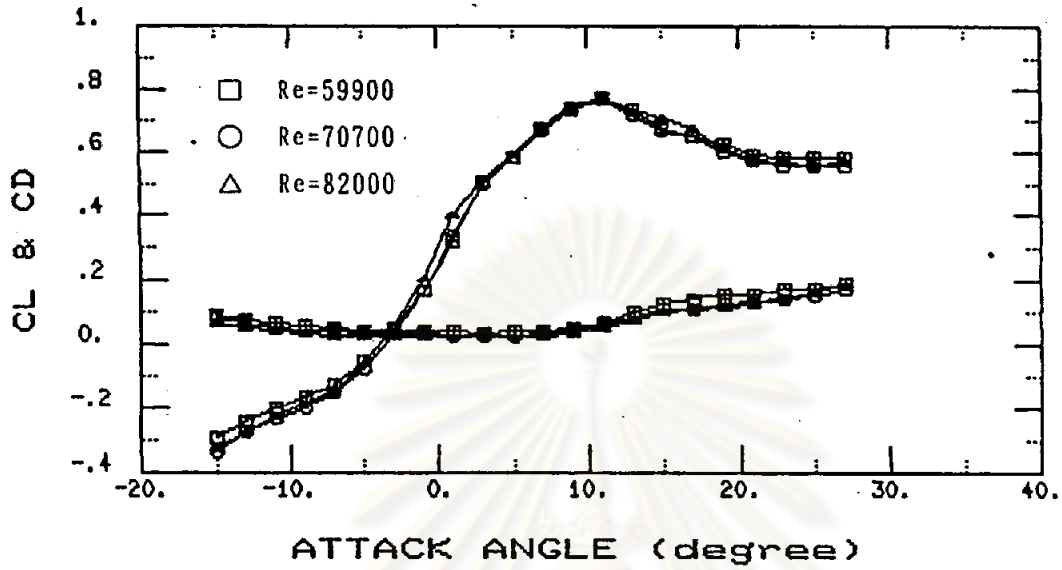


Fig. C.11. Relation of  $C_L, C_D$  vs attack angle (Arched plate No. 4)

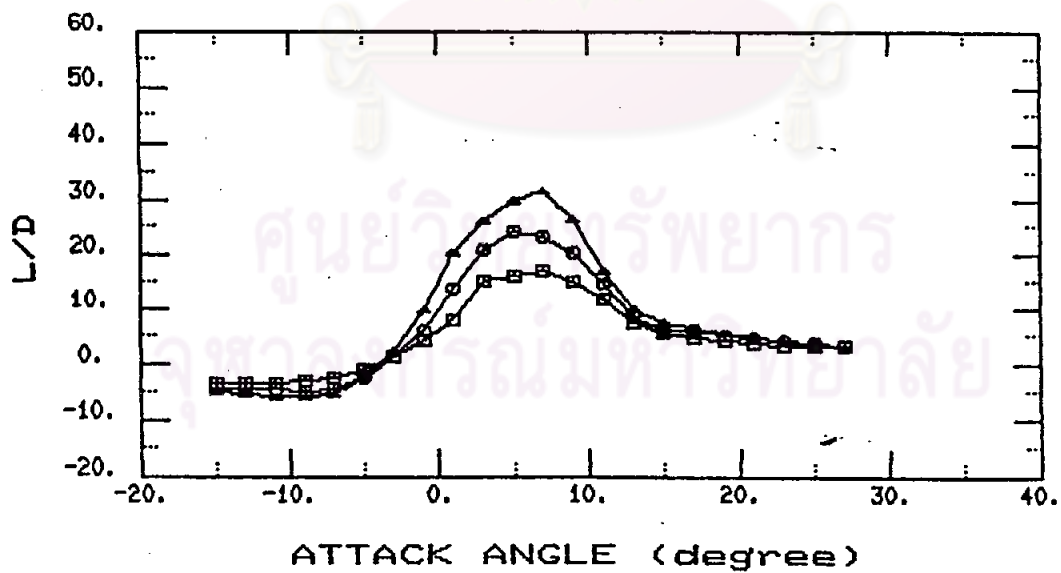


Fig. C.12 Relation of L/D ratio vs attack angle (Arched plate No. 4)

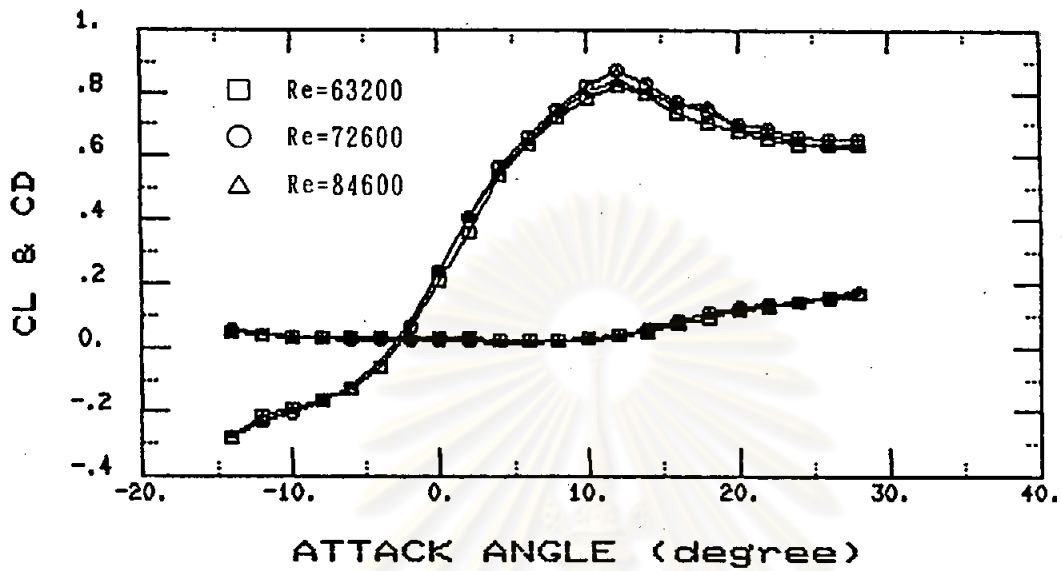


Fig. C.13 Relation of  $C_L, C_D$  vs attack angle (Arched plate No.5)

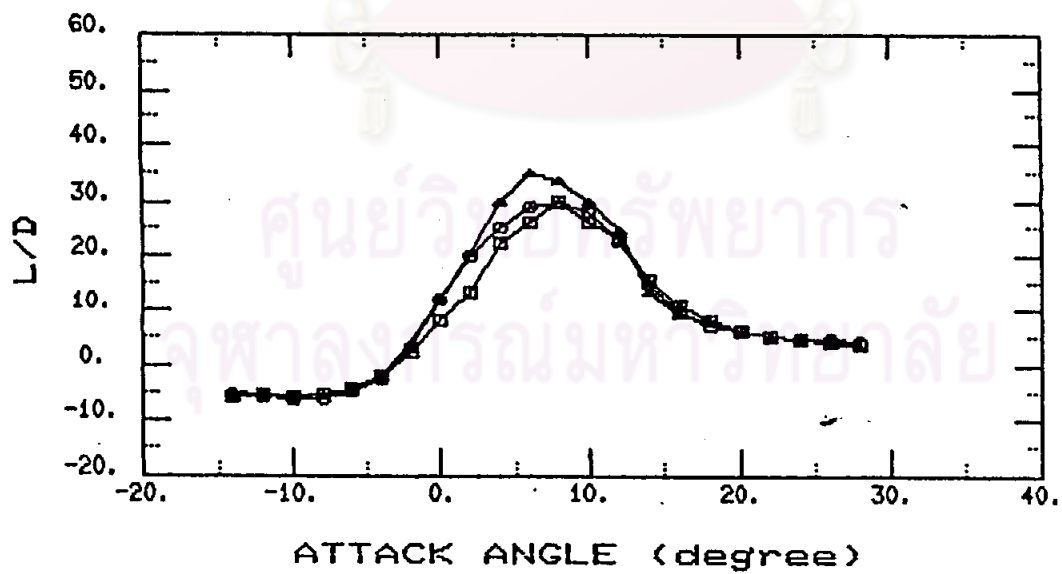


Fig. C.14 Relation of L/D ratio vs attack angle (Arched plate No.5)

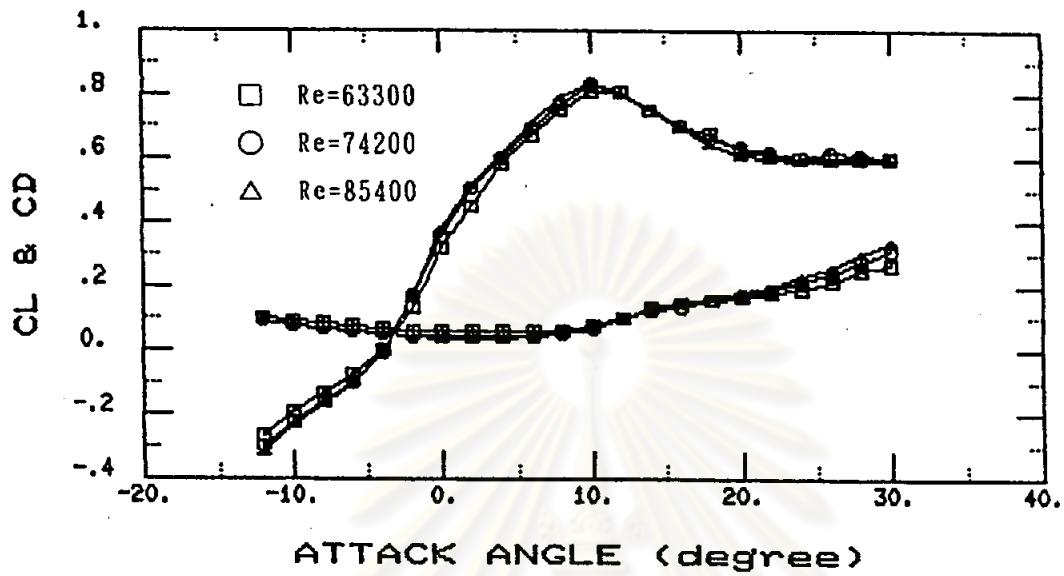


Fig. C.15 Relation of  $C_L, C_D$  vs attack angle (Arched steel plate No. 6)

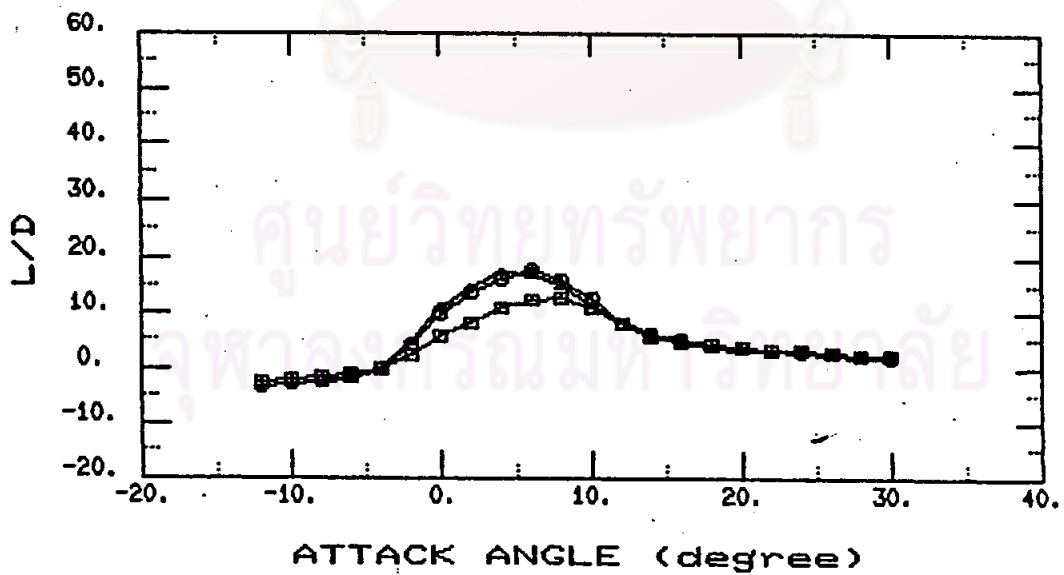


Fig. C.16 Relation of  $L/D$  ratio vs attack angle (Arched steel plate No. 6)

Re = 54000 - 64000

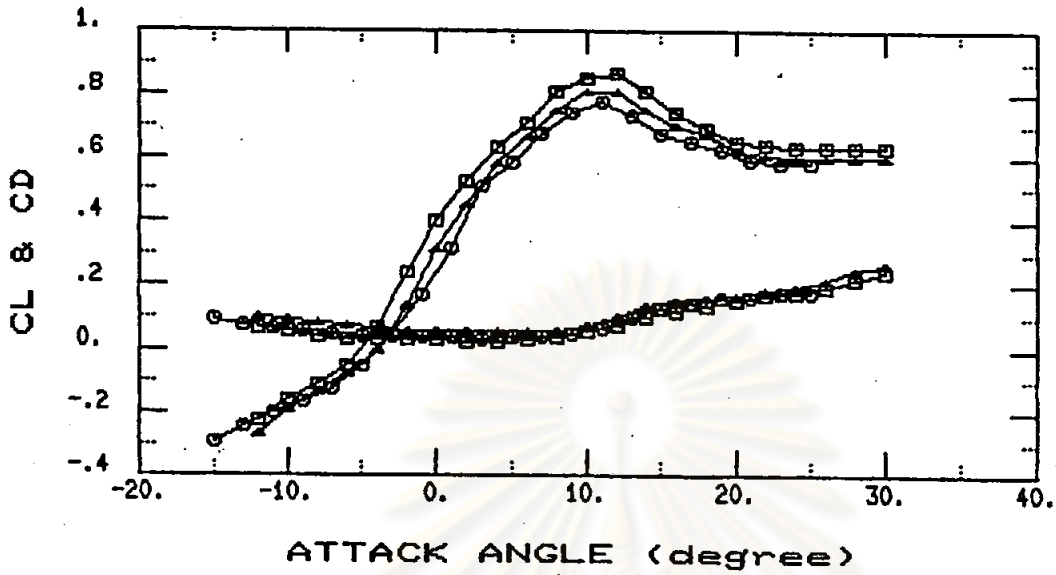


Fig.C.17 Comparison of  $C_L, C_D$  for different types of airfoils

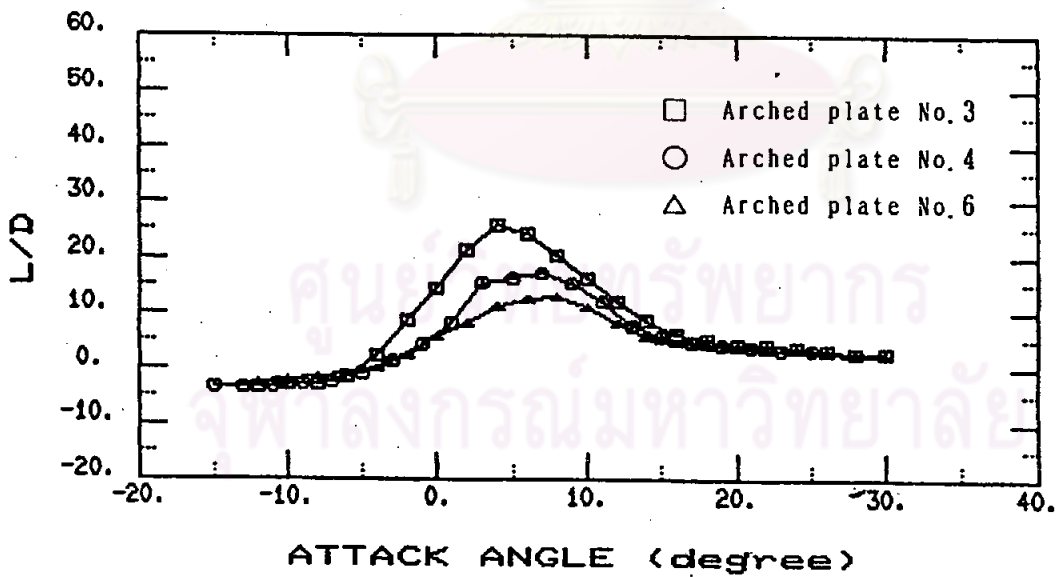


Fig.C.18 Comparison of L/D for different types of airfoils

Re = 61500 - 74500

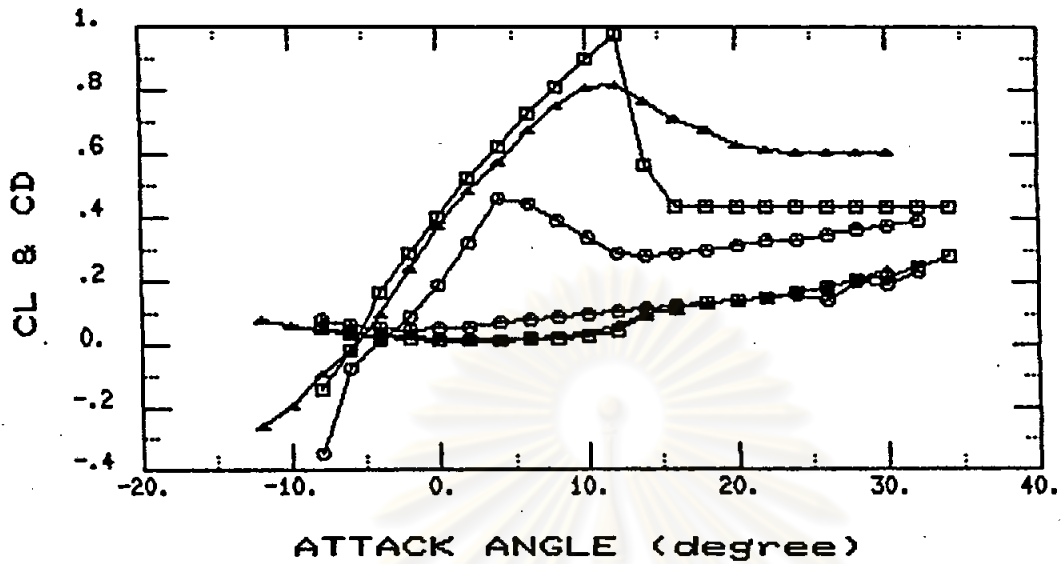


Fig. C.19 Comparison of  $C_L, C_D$  for different types of airfoils

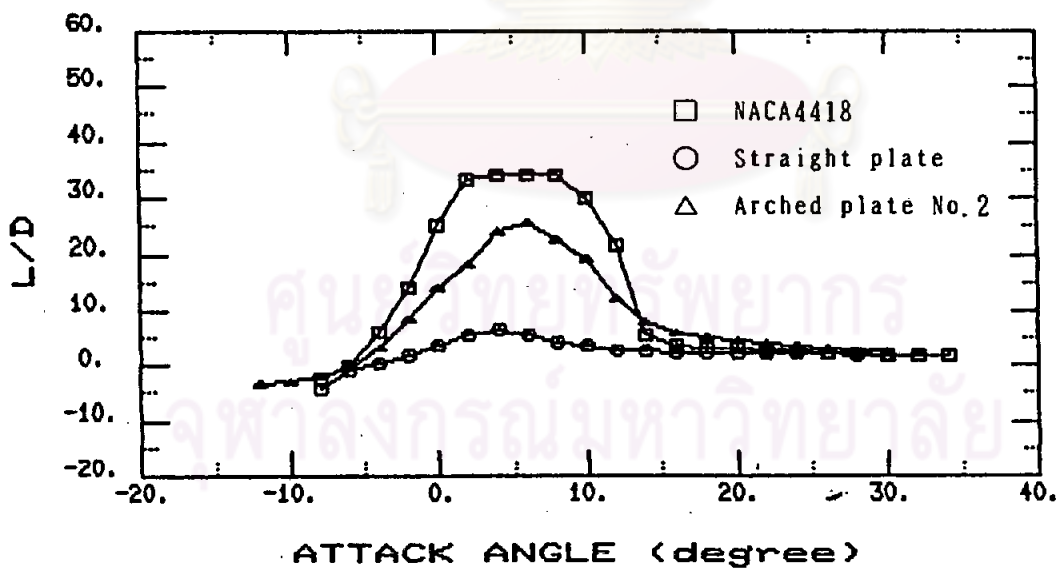


Fig. C.20 Comparison of L/D for different types of airfoils

Re = 61500 - 74500

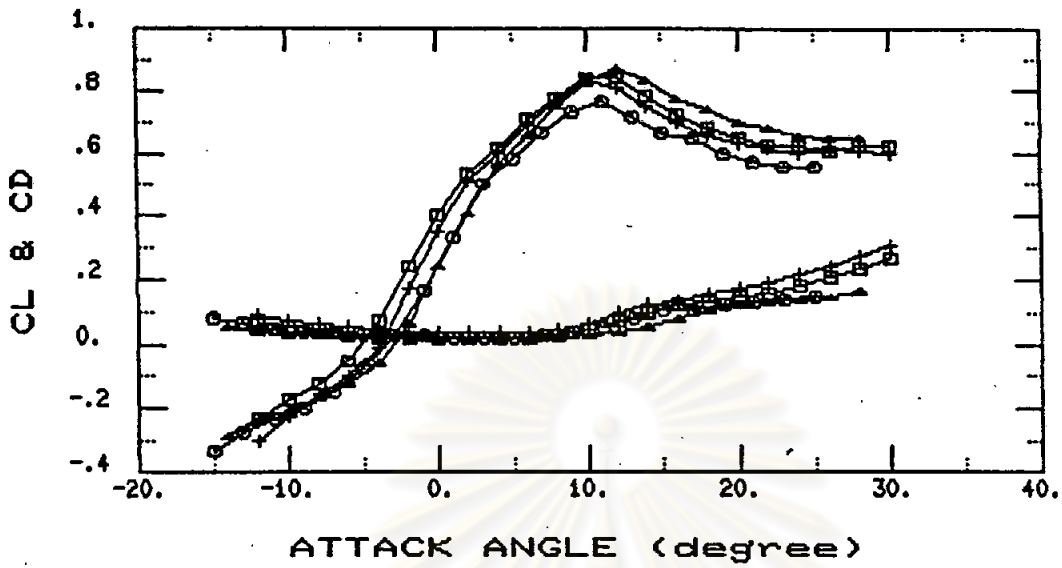


Fig.C.21 Comparison of  $C_L, C_D$  for different types of airfoils

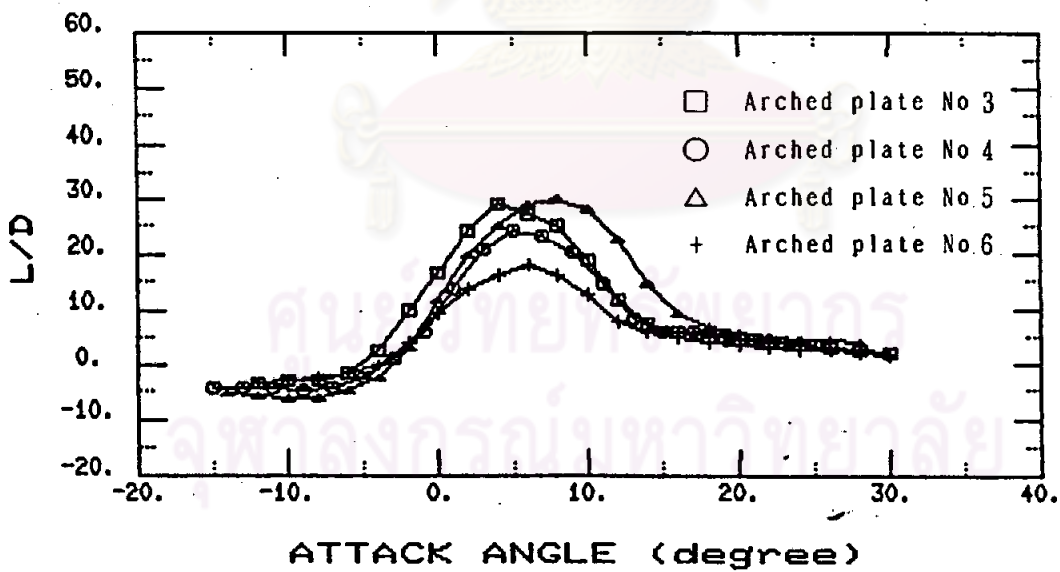


Fig.C.22 Comparison of  $L/D$  for different types of airfoils



Re = 71500 - 85500

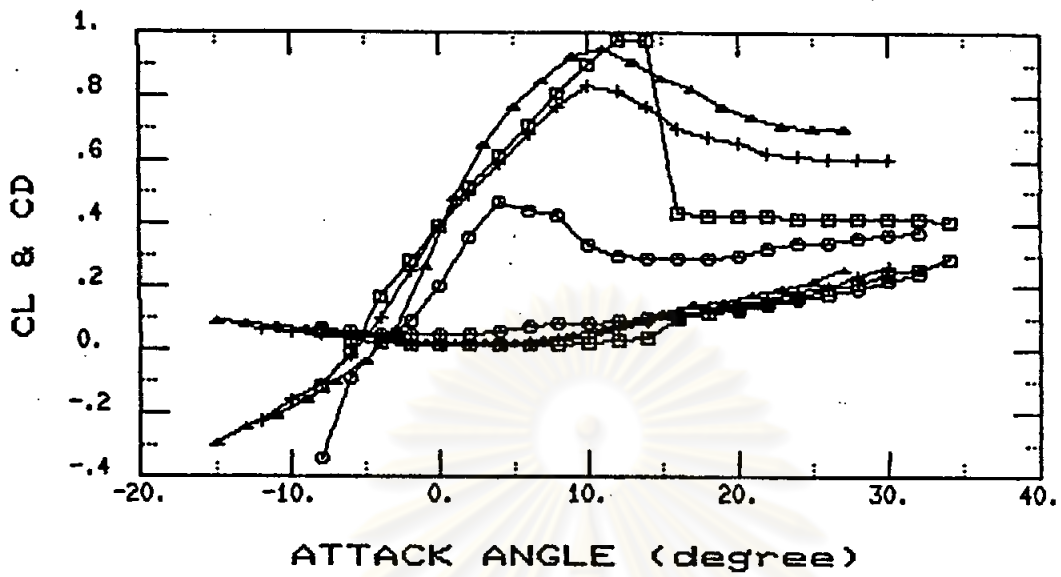


Fig.C.23. Comparison of  $C_L, C_D$  for different types of airfoils

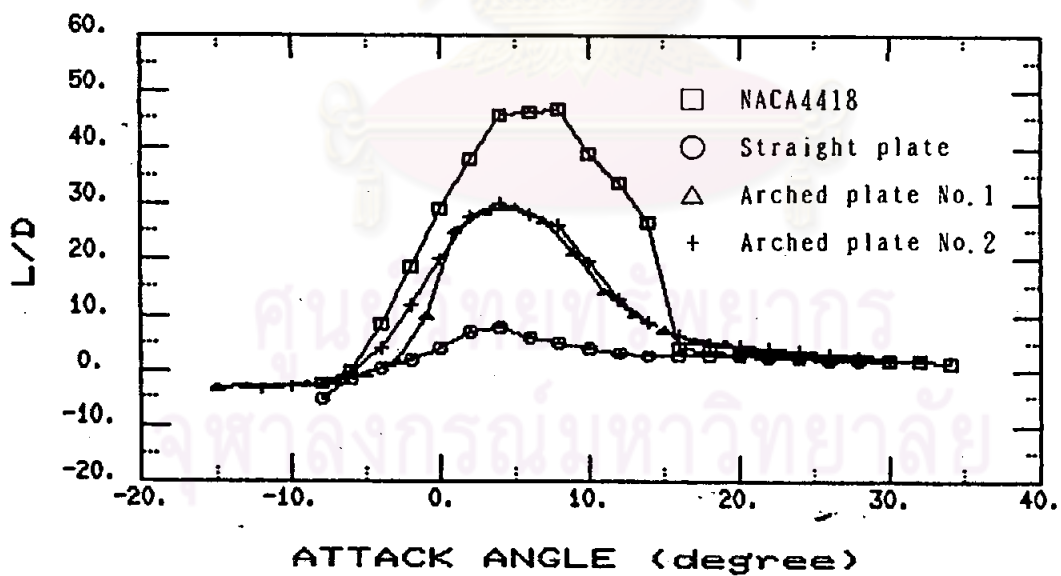


Fig.C.24 Comparison of L/D for different types of airfoils

Re = 71500 - 85500

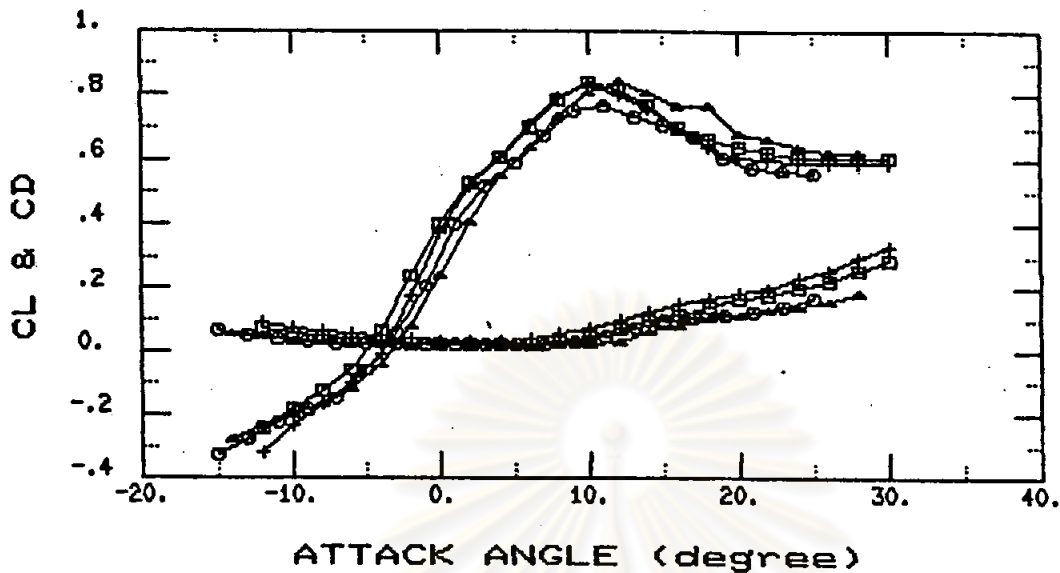


Fig.C.25 Comparison of CL, CD for different types of airfoils

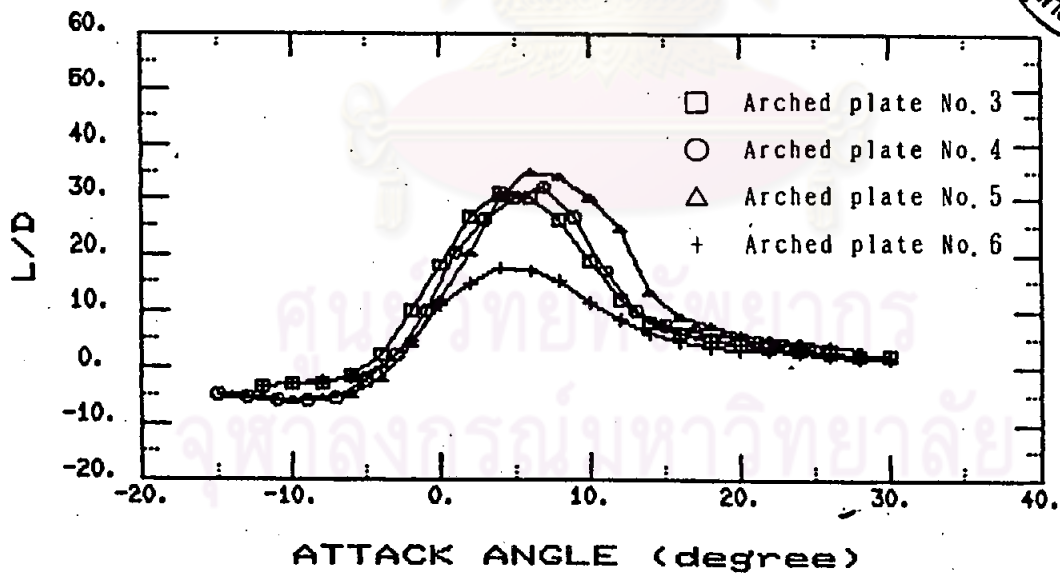



Fig. C.26 Comparison of L/D for different types of airfoils



STRAIGHT PLATE

RE = 46000

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Figures C.27 to C.84 showed the flow visualization results of each model.

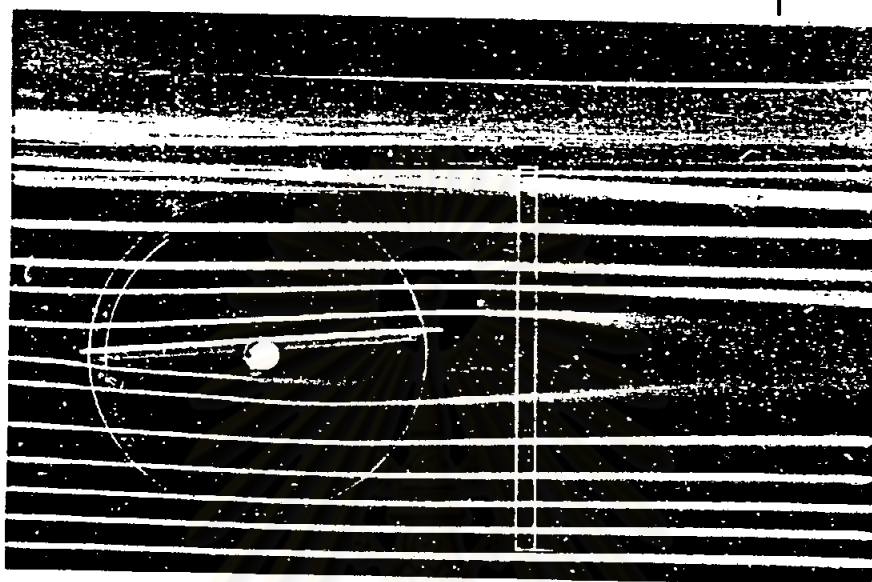


Fig.C.27 Attack angle = - 5 degrees

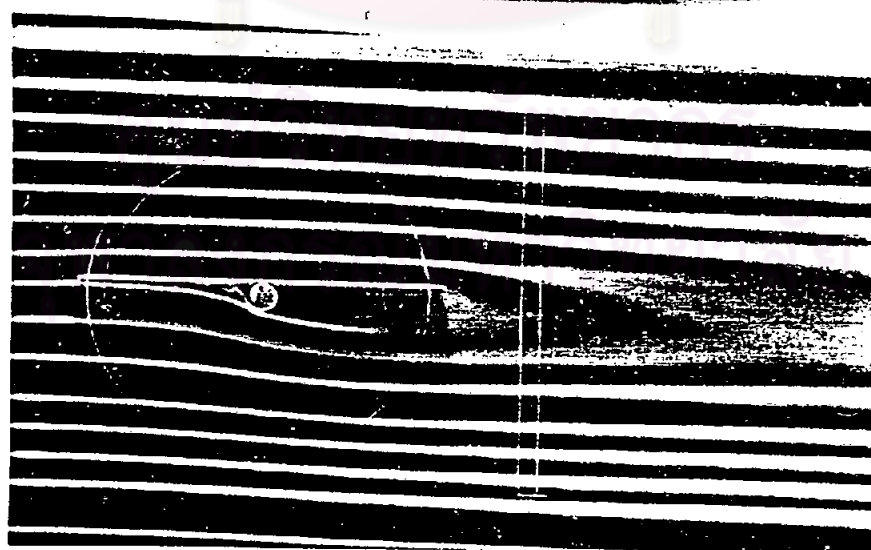


Fig.C.28 Attack angle = 0 degrees

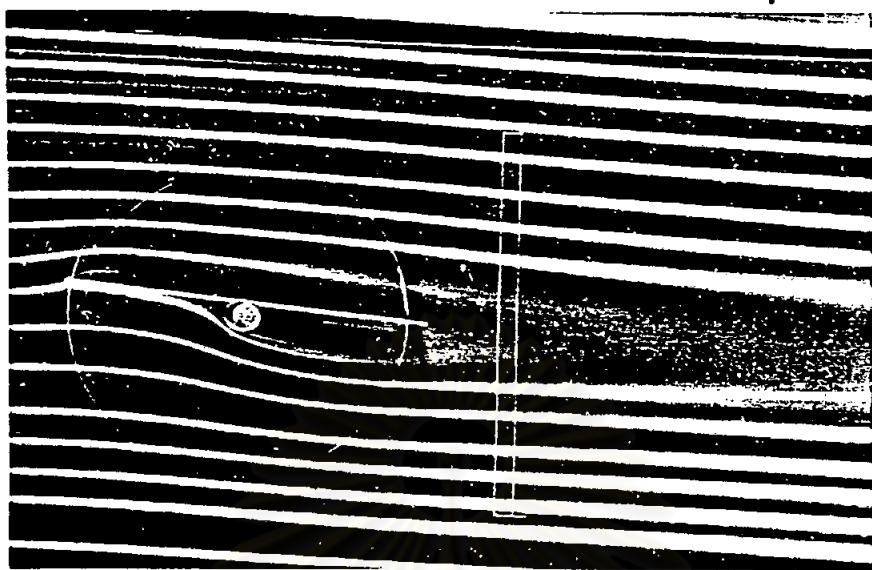


Fig. C.29 Attack angle = 5 degrees

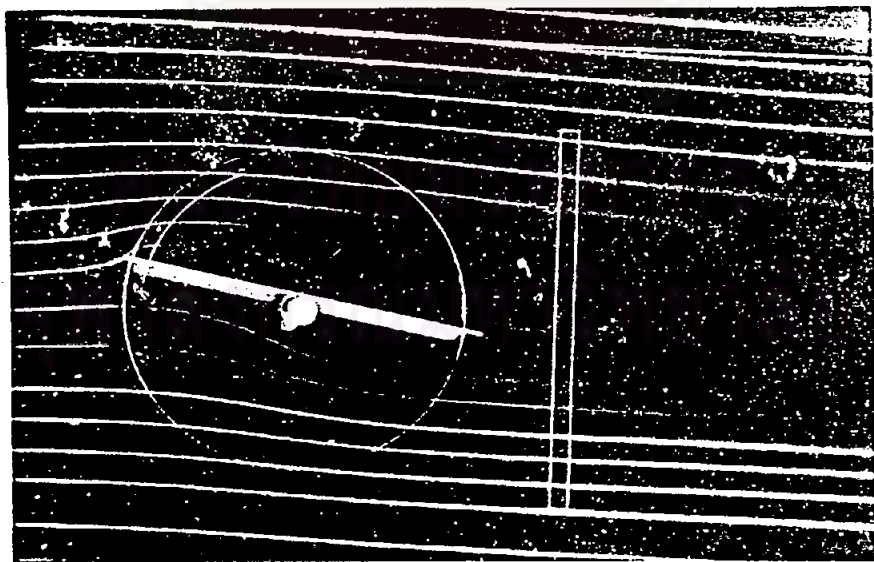


Fig. C.30 Attack angle = 10 degrees

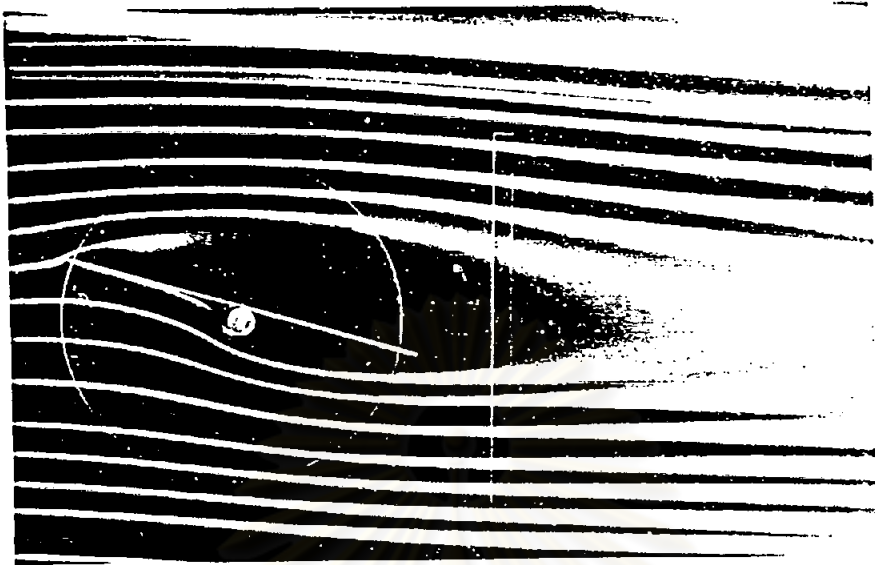


Fig. C.31 Attack angle = 15 degrees

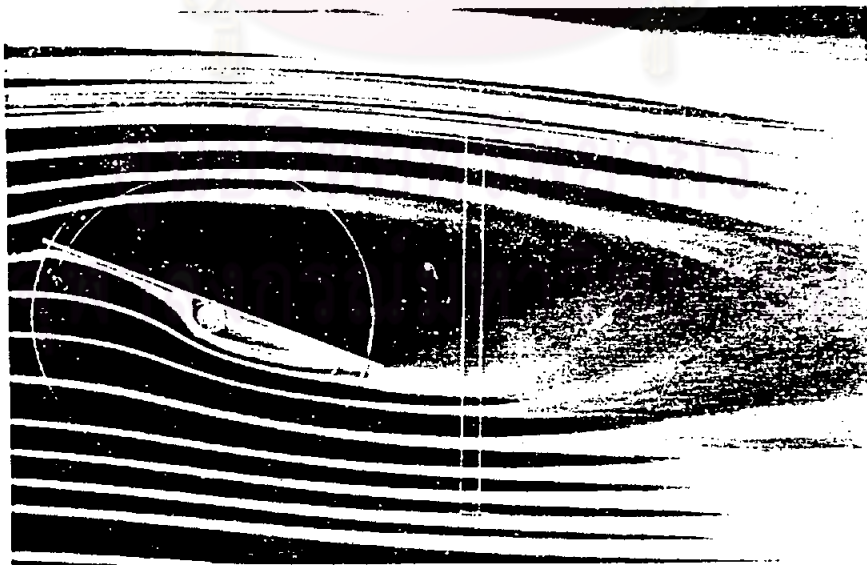


Fig. C.32 Attack angle = 20 degrees

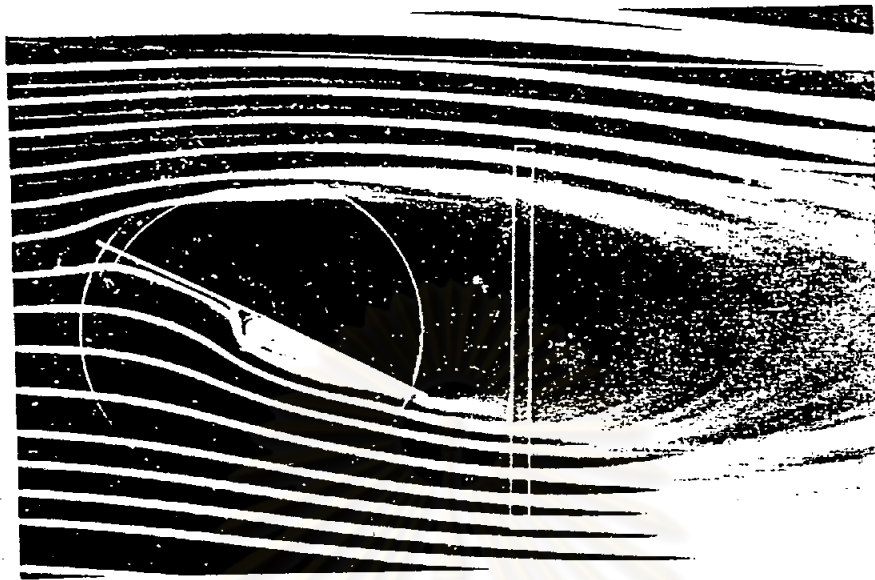


Fig. C.33 Attack angle = 25 degrees

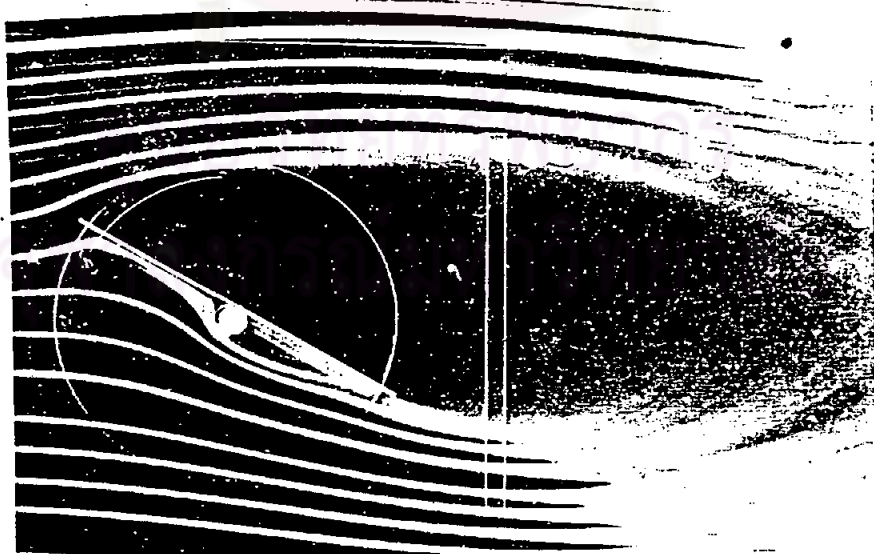


Fig. C.34 Attack angle = 30 degrees

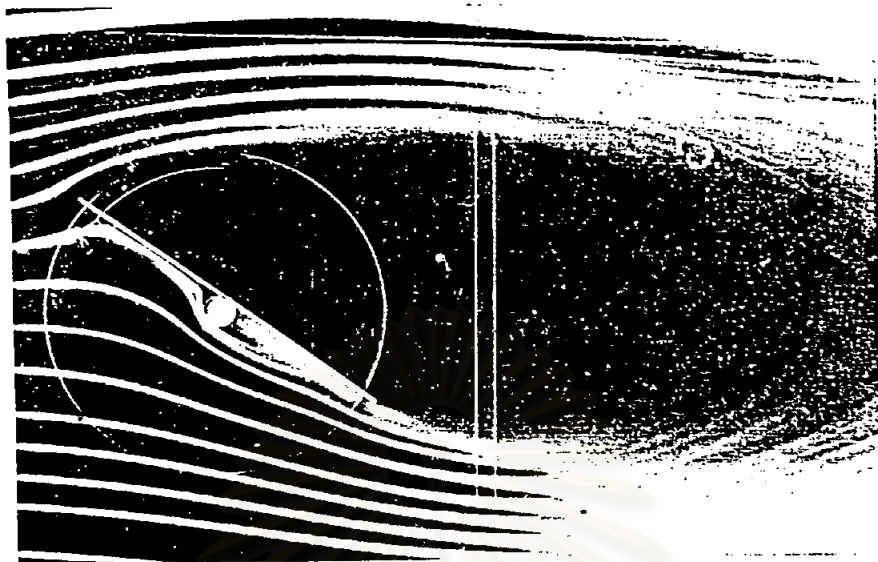


Fig. C.35 Attack angle = 35 degrees

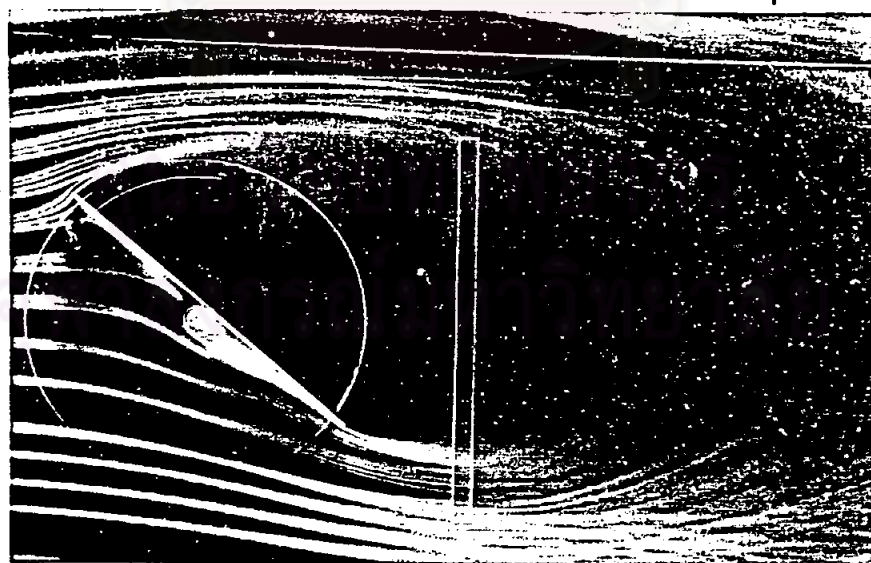


Fig. C.36 Attack angle = 40 degrees





ARCHED PLATE WITH STICK 6mm (NO SPACE)

RE = 64000

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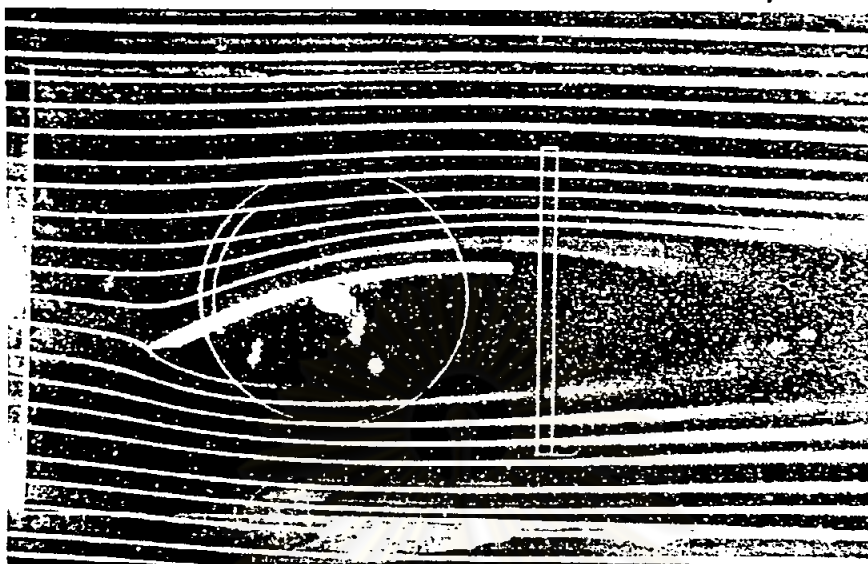


Fig.C.37 Attack angle = -15 degrees

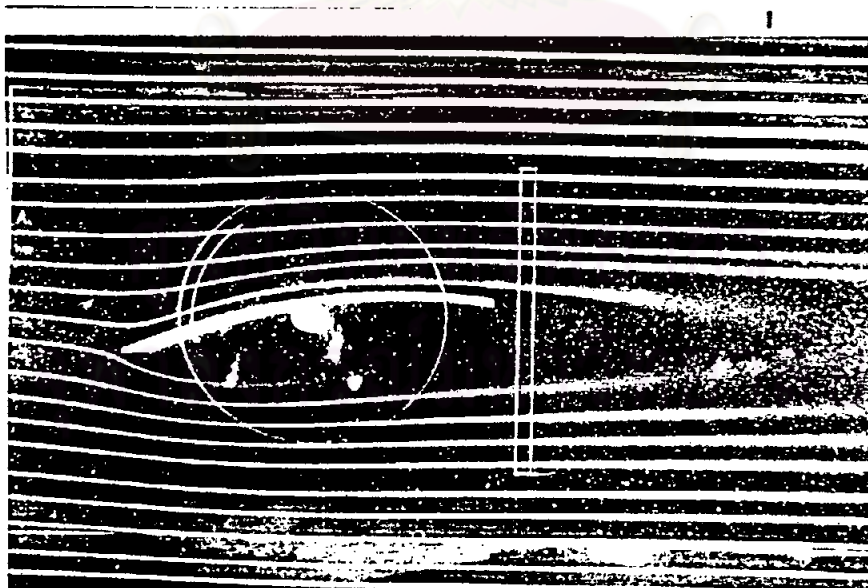


Fig.C.38 Attack angle = -10 degrees

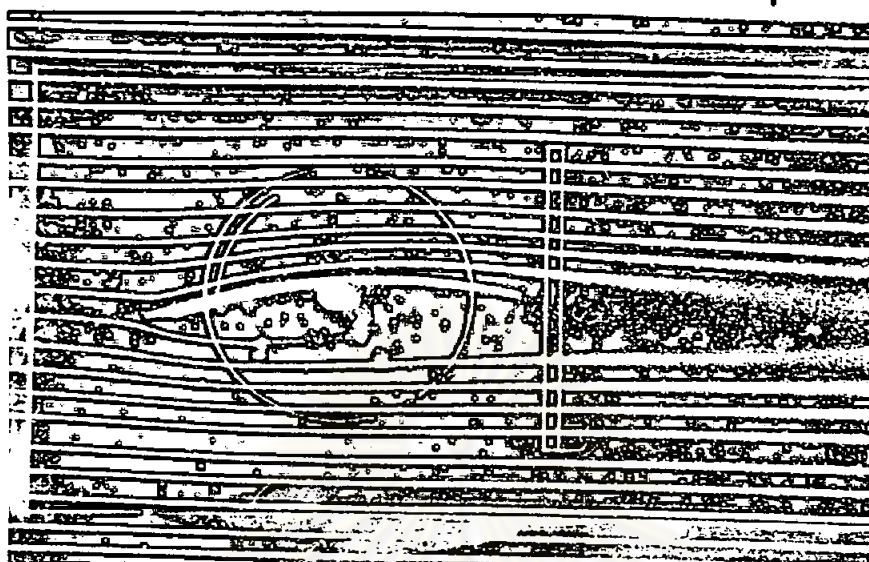


Fig.C.39 Attack angle = - 5 degrees

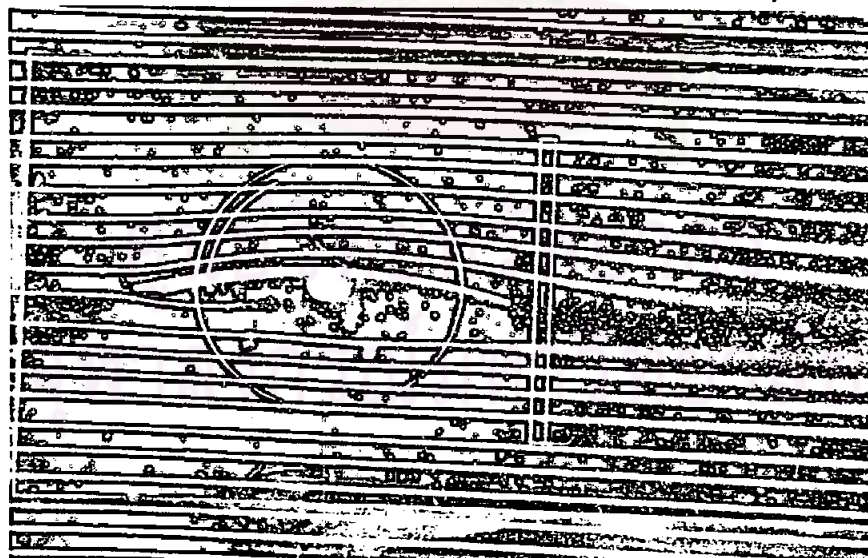


Fig.C.40 Attack angle = 0 degrees

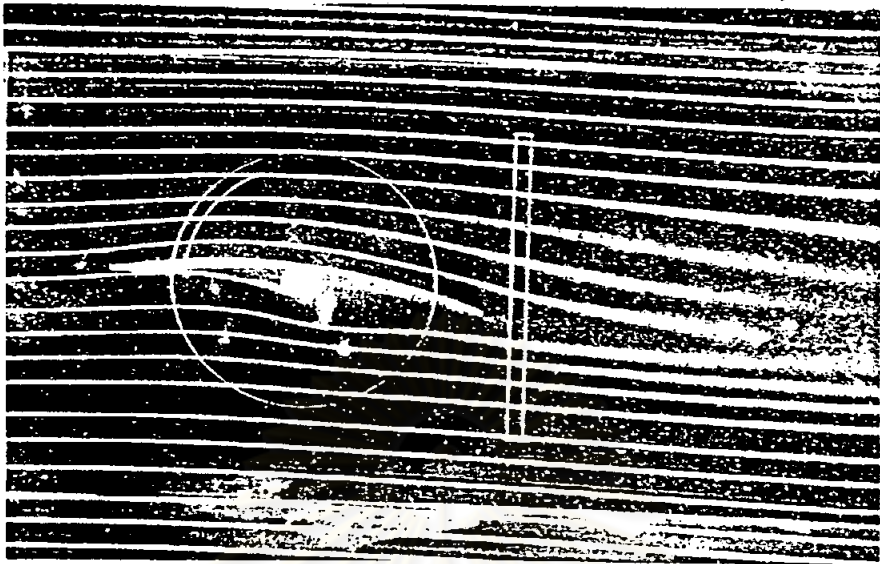


Fig.C.41 Attack angle = 5 degrees

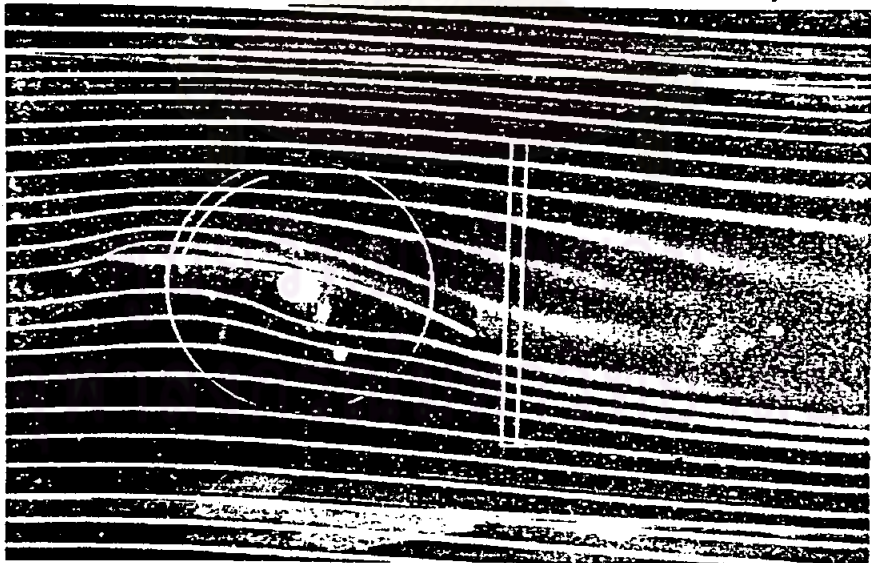


Fig.C.42 Attack angle = 10 degrees

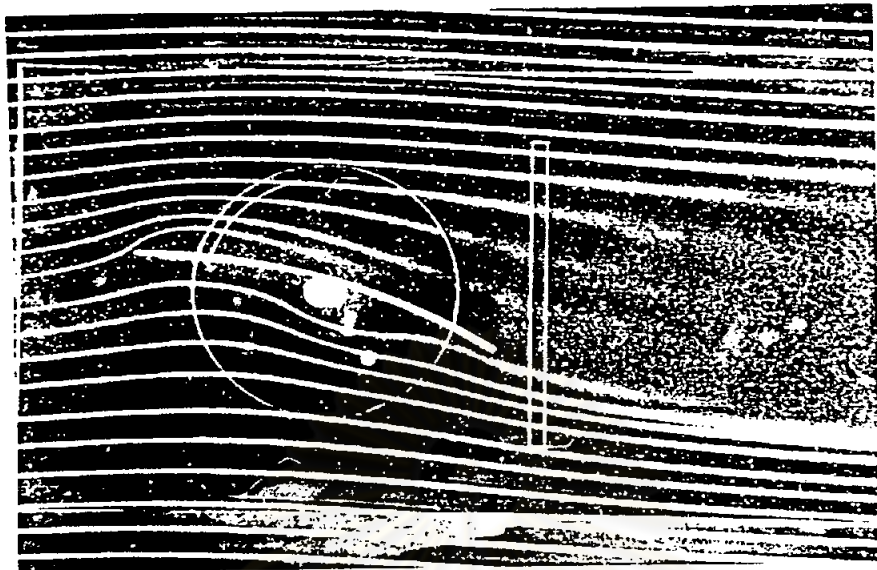


Fig. C.43 Attack angle = 15 degrees

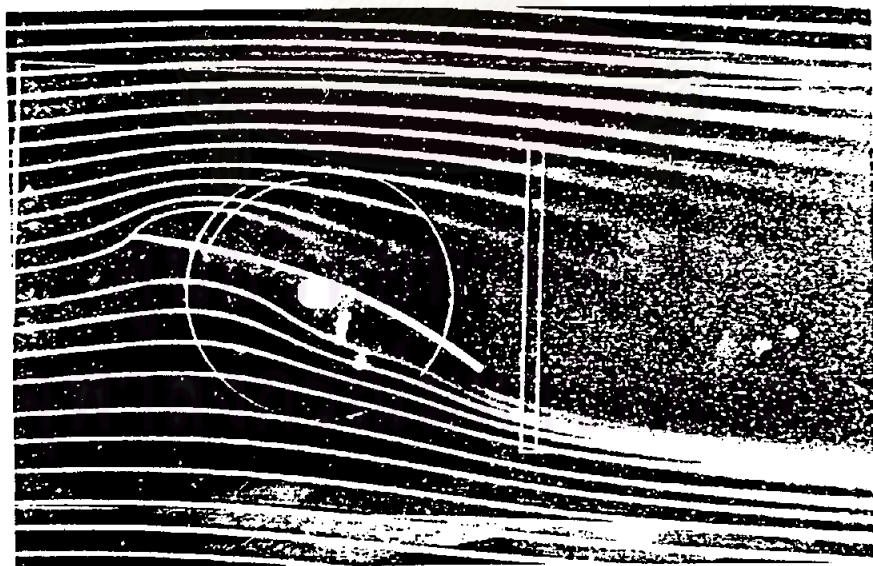


Fig. C.44 Attack angle = 20 degrees



Fig. C.45 Attack angle = 25 degrees

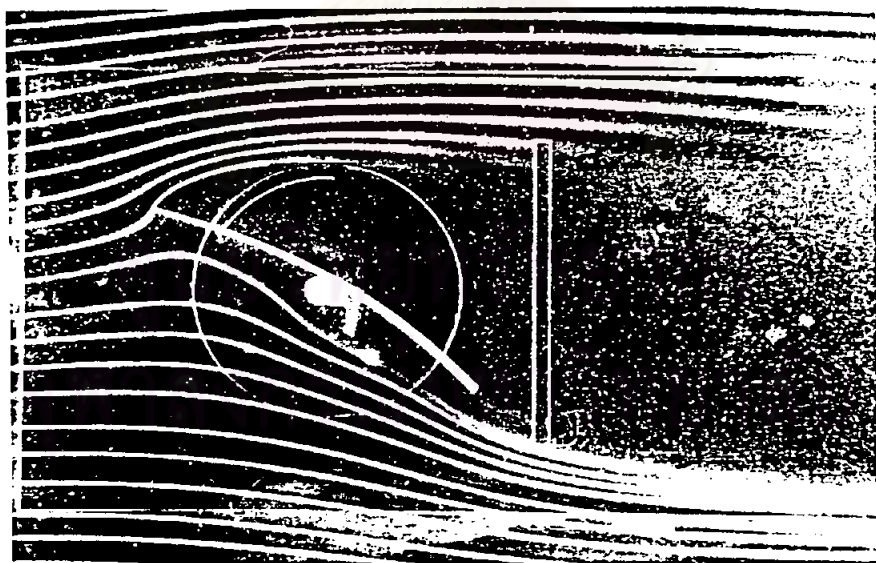


Fig. C.46 Attack angle = 30 degrees

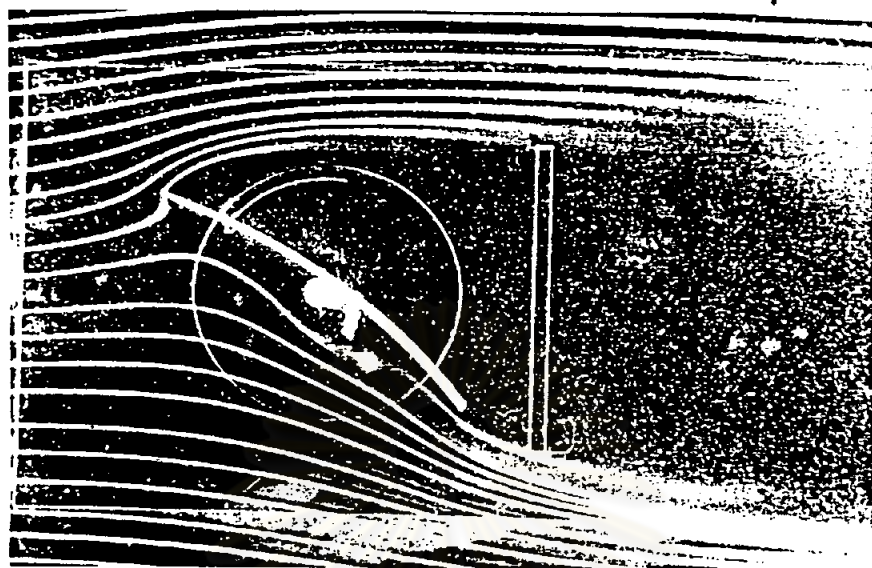


Fig.C.47 Attack angle = 35 degrees

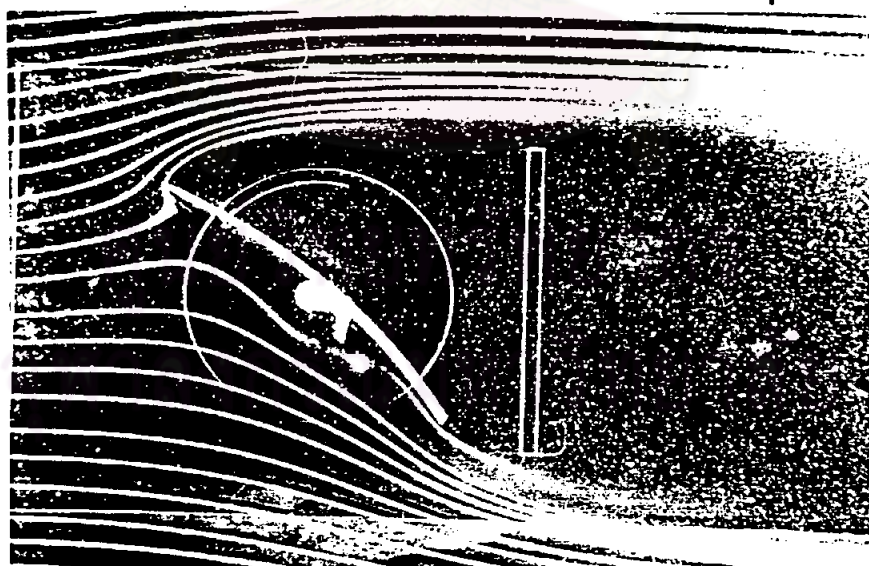



Fig. C.48 Attack angle = 40 degrees



ARCHED PLATE WITH STICK 6 mm (SPACE)

RE = 64000

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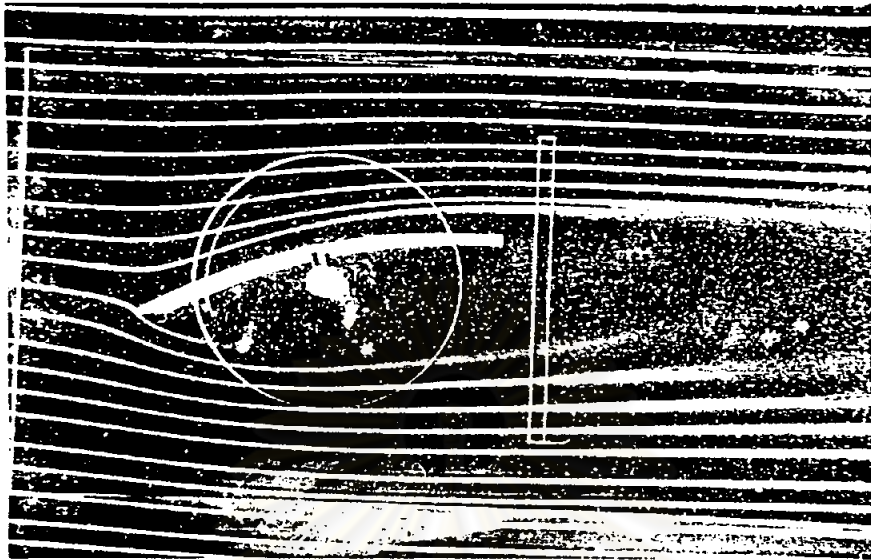


Fig. C.49 Attack angle = -15 degrees

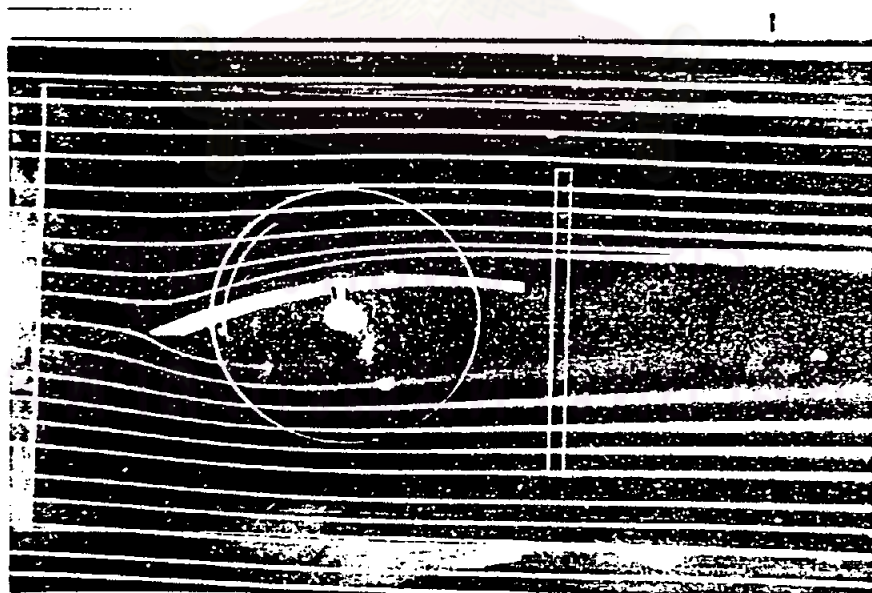


Fig. C.50 Attack angle = -10 degrees

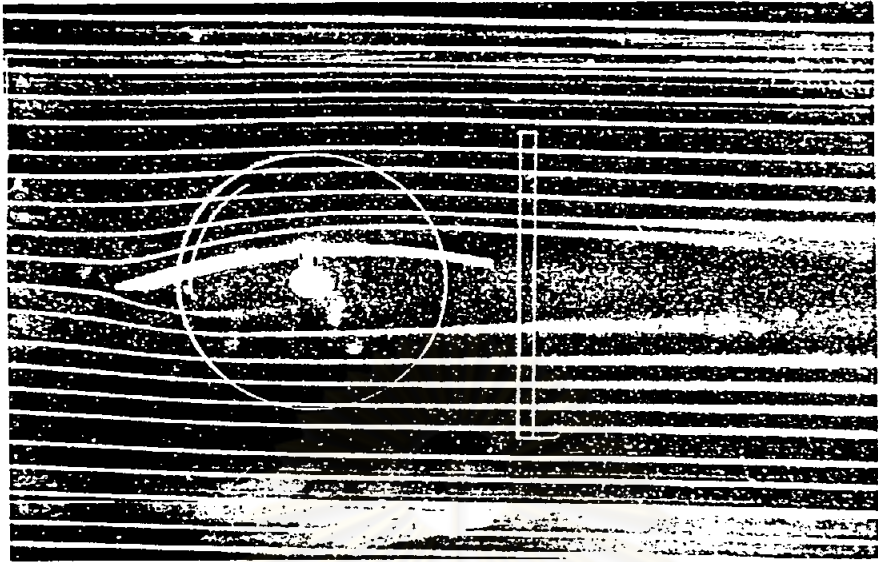


Fig.C.51 Attack angle = - 5 degrees

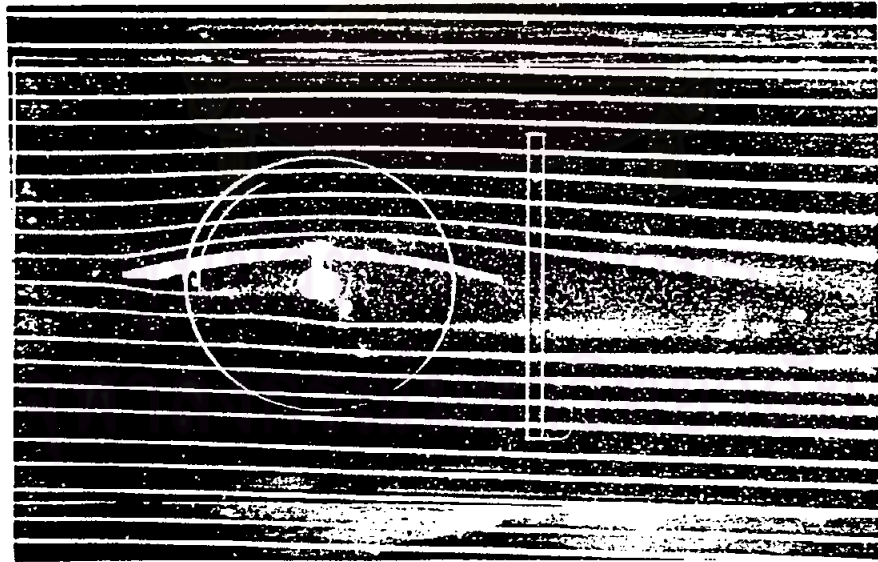


Fig.C.52 Attack angle = 0 degrees



Fig. C.53 Attack angle = 5 degrees

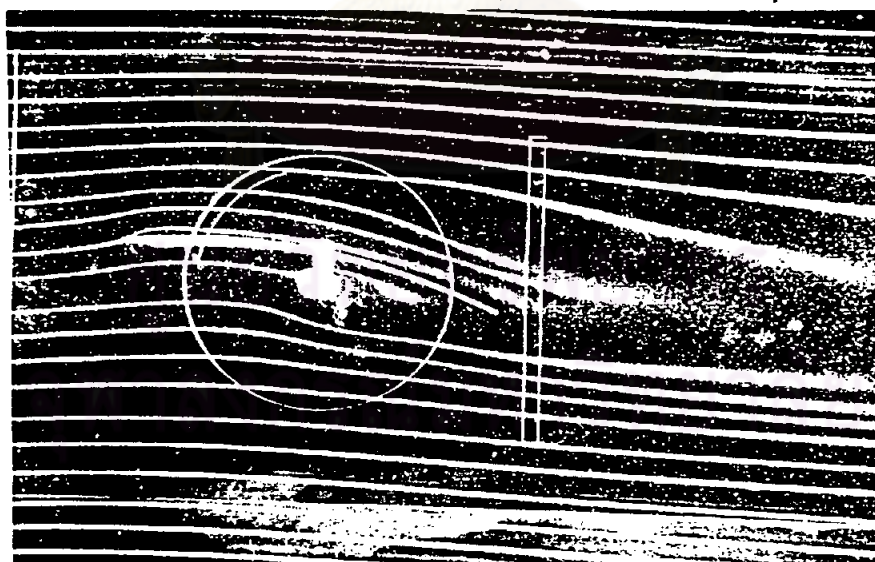


Fig. C.54 Attack angle = 10 degrees

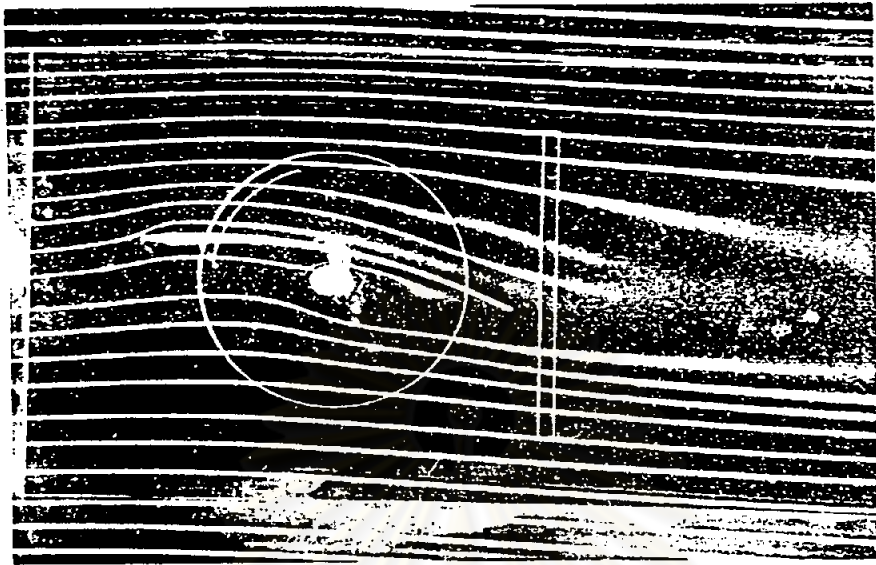


Fig. C.55 Attack angle = 15 degrees

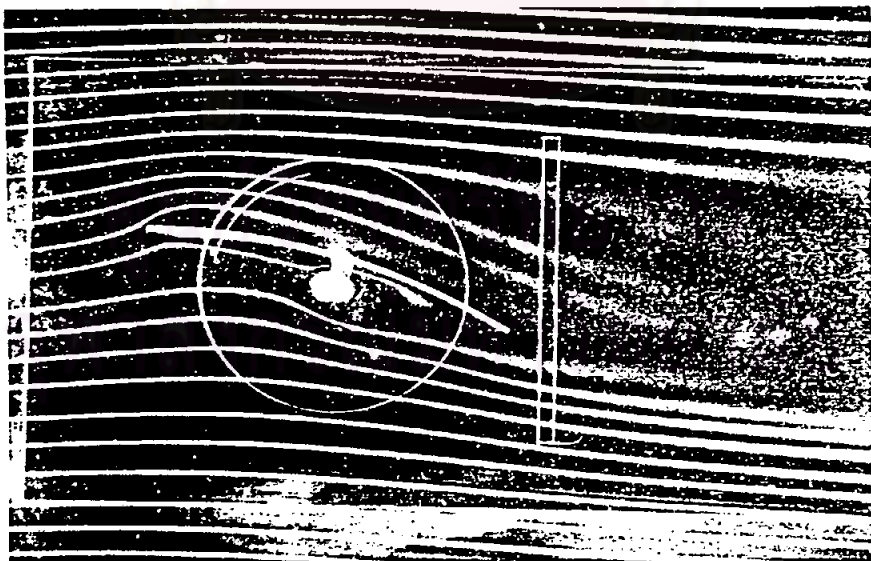


Fig. C.56 Attack angle = 20 degrees

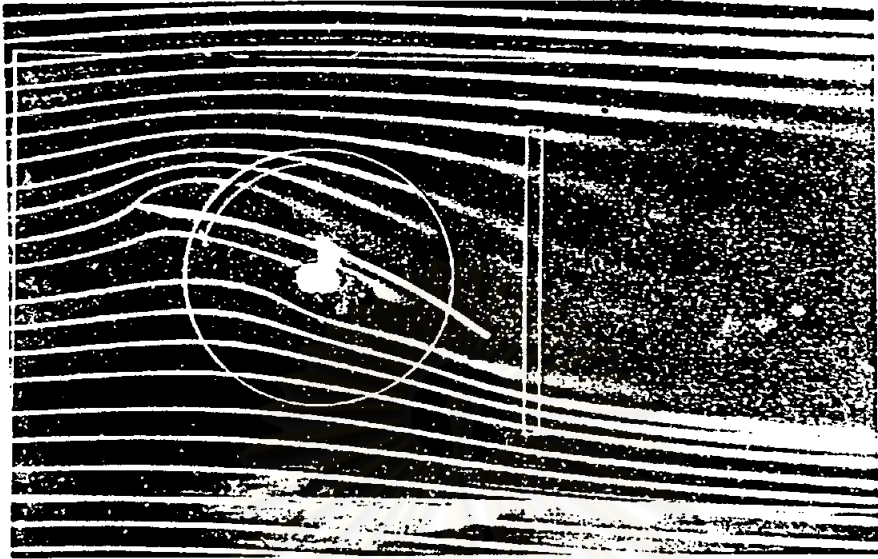


Fig. C.57 Attack angle = 25 degrees

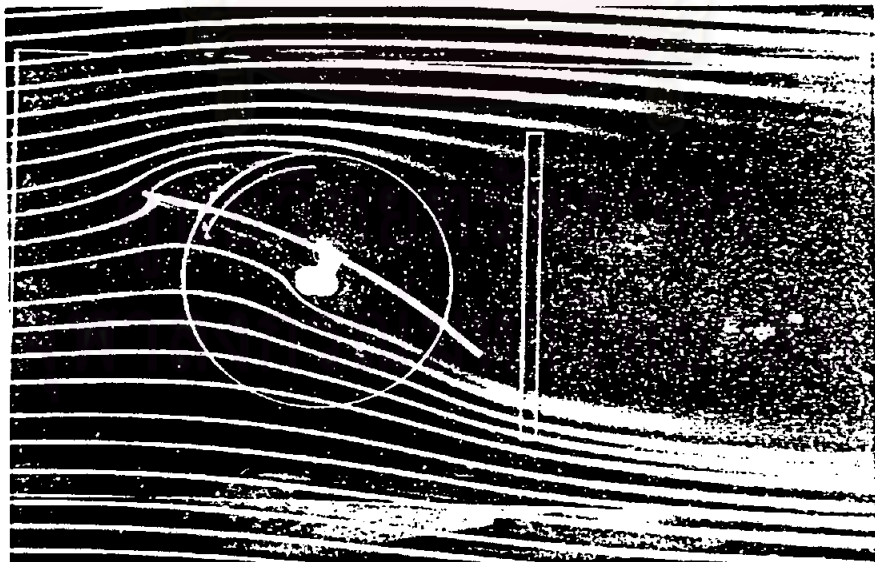


Fig. C.58 Attack angle = 30 degrees

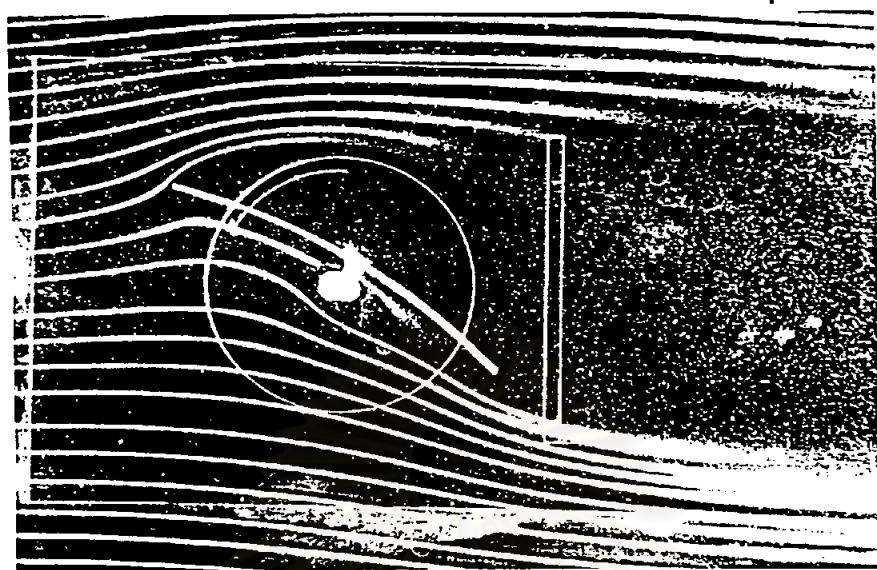


Fig.C.59 Attack angle = 35 degrees

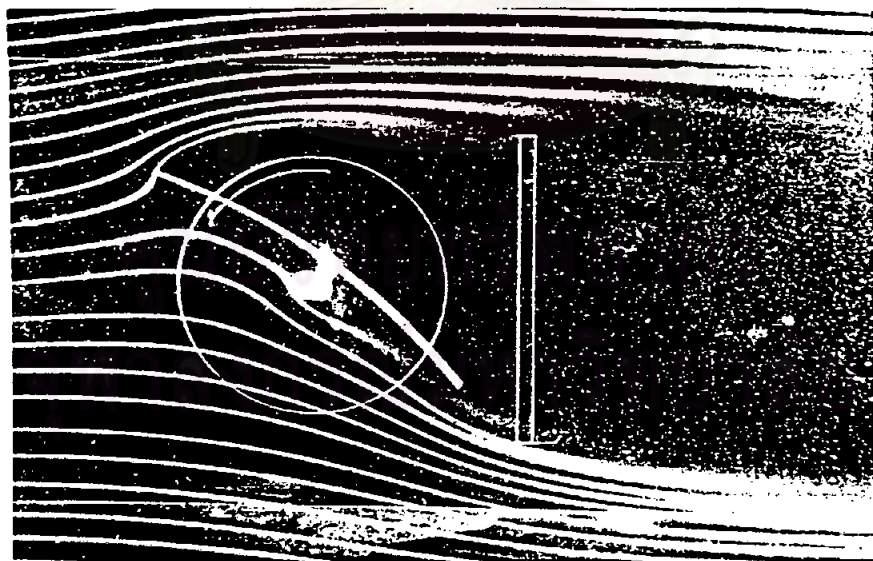


Fig.C.60 Attack angle = 40 degrees

ARCHED PLATE WITH STICK AT FRONT

RE = 64000

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จุฬาลงกรณ์มหาวิทยาลัย

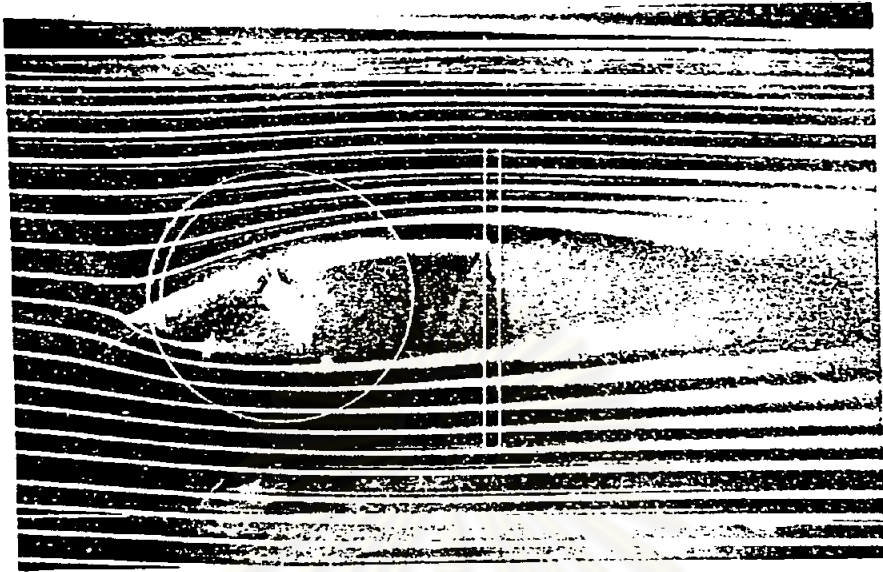


Fig. C.61 Attack angle = -15 degrees

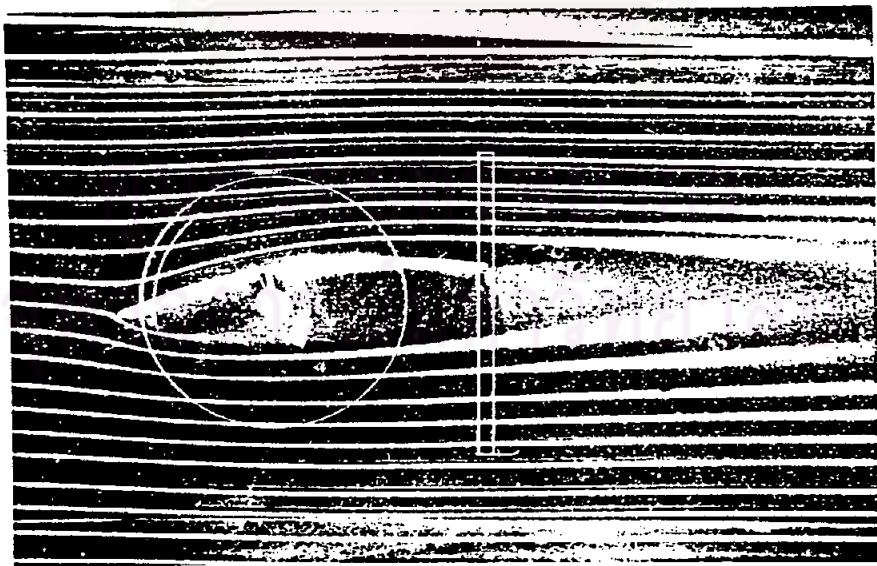


Fig. C.62 Attack angle = -10 degrees



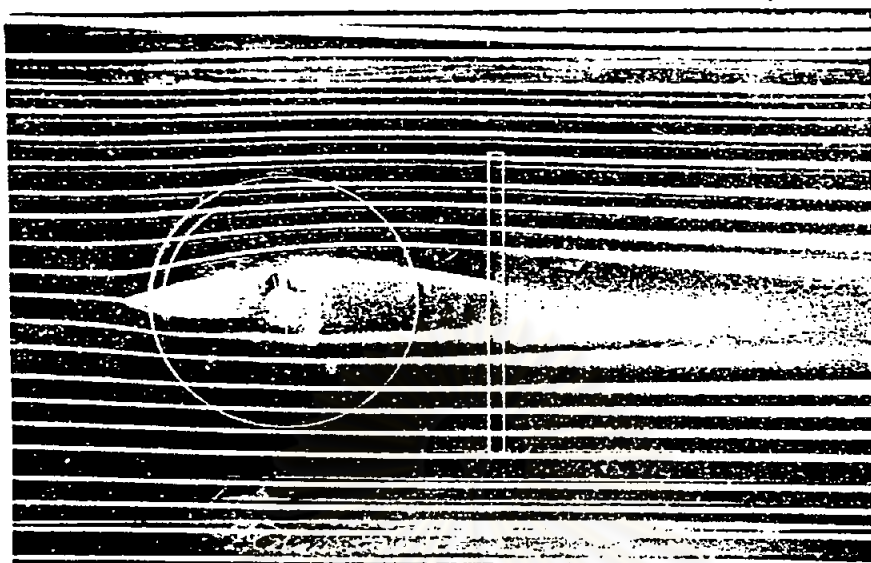


Fig. C.63 Attack angle = -5 degrees

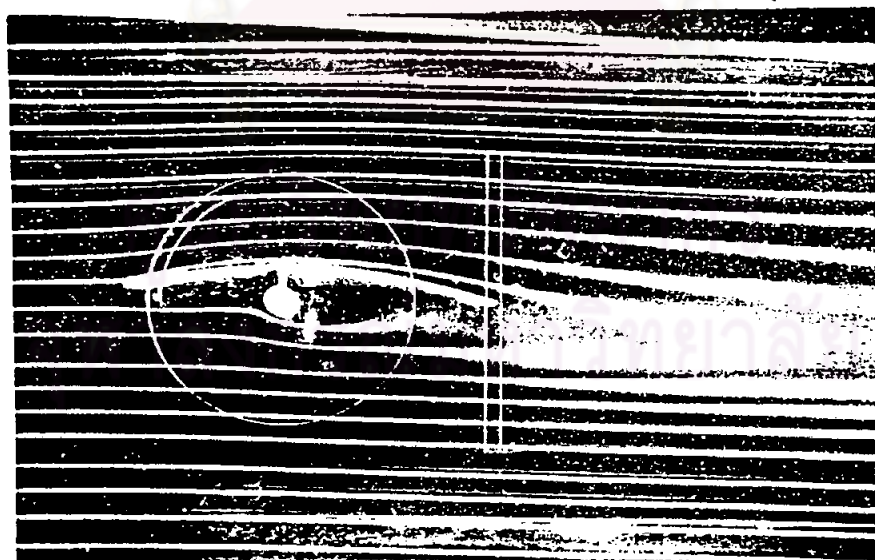


Fig. C.64 Attack angle = 0 degrees

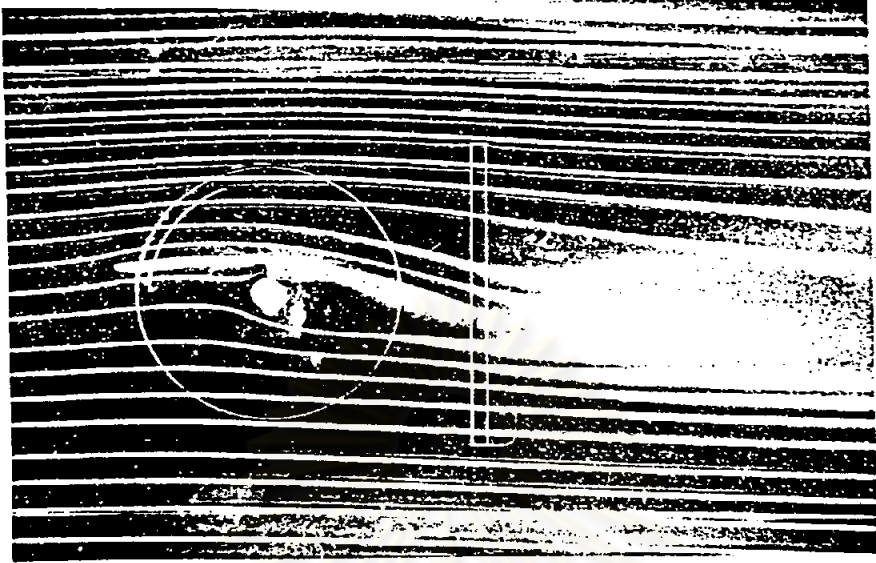


Fig.C.65 Attack angle = 5 degrees

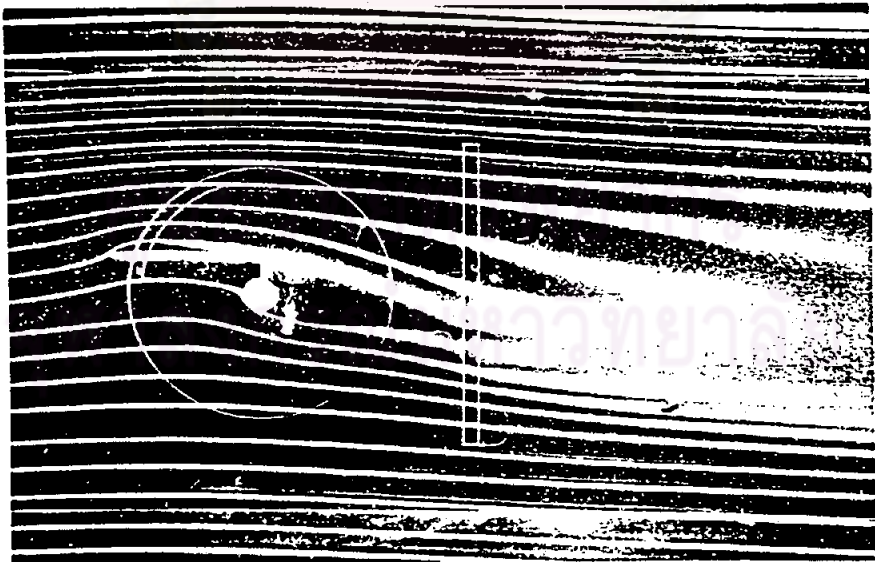


Fig.C.66 Attack angle = 10 degrees



Fig. C.67 Attack angle = 15 degrees

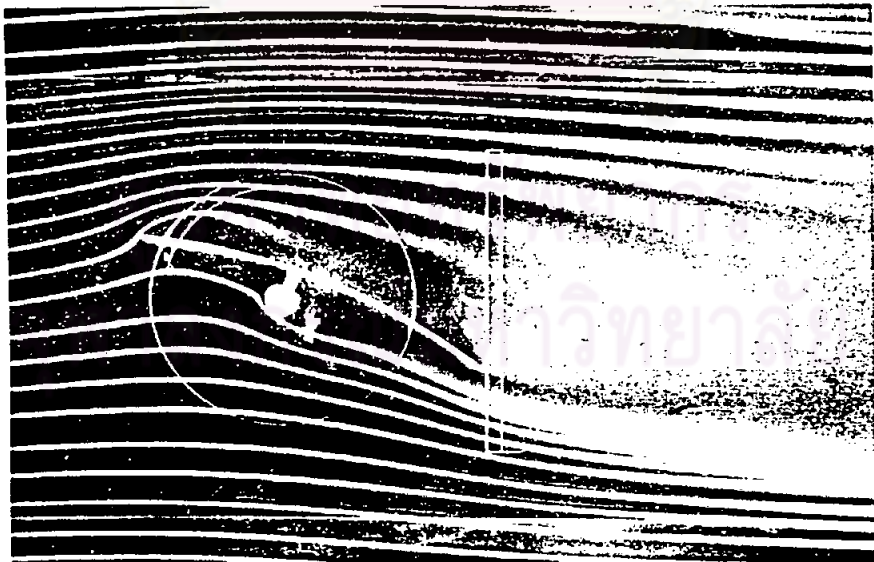


Fig. C.68 Attack angle = 20 degrees

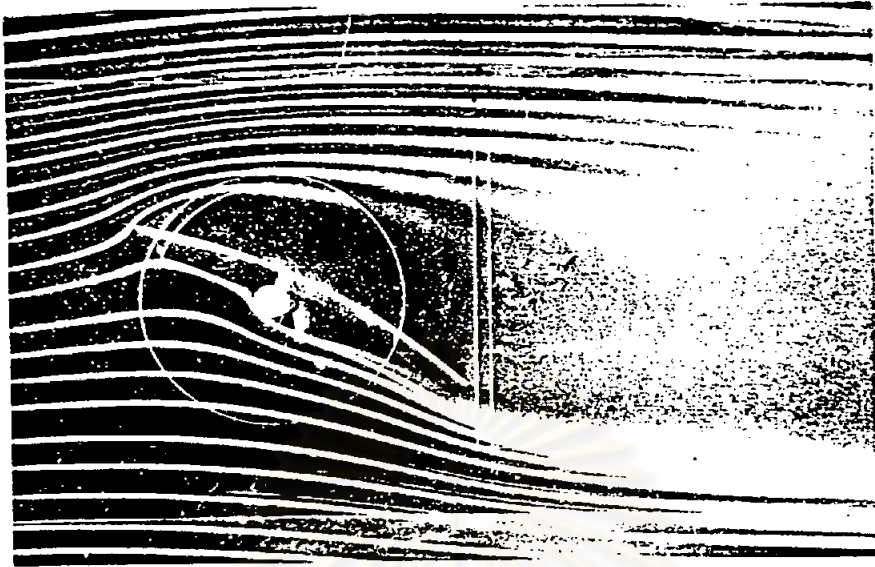


Fig. C.69 Attack angle = 25 degrees

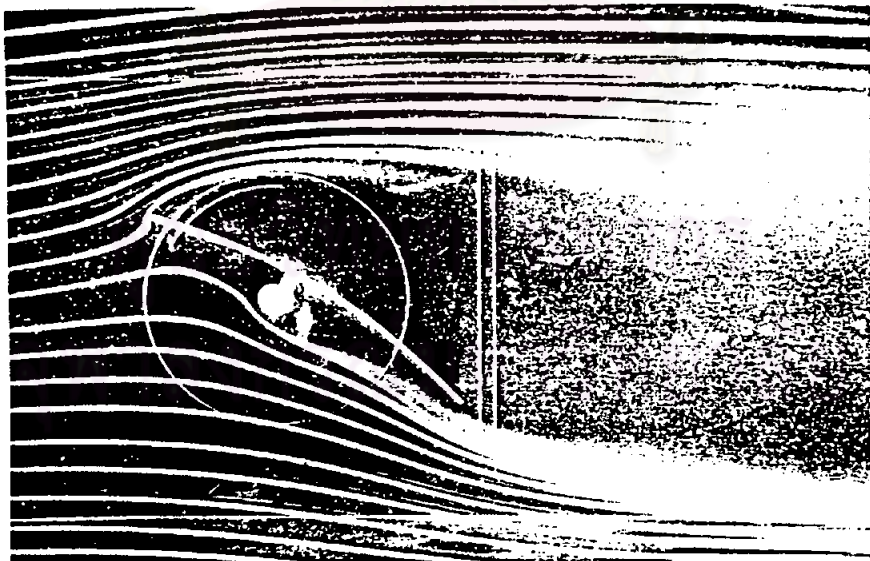


Fig. C.70 Attack angle = 30 degrees

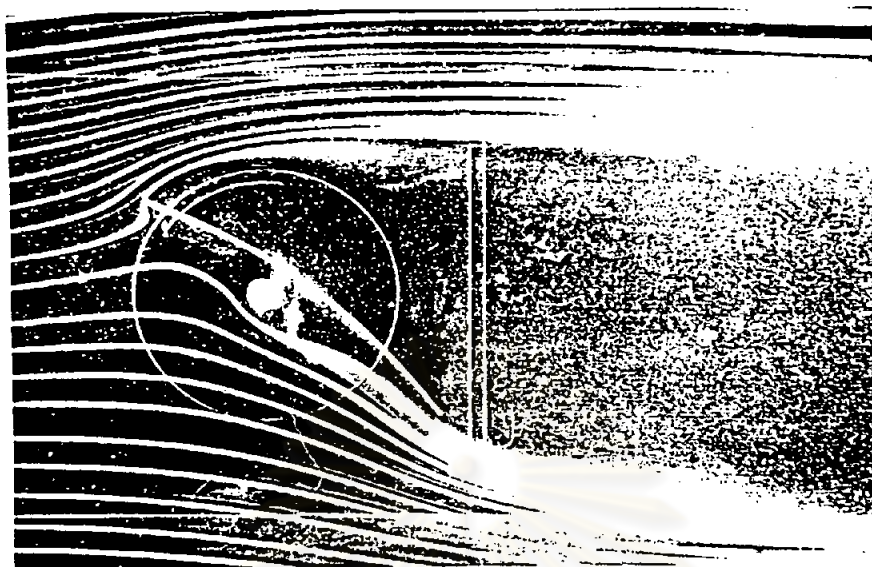


Fig. C.71 Attack angle = 35 degrees

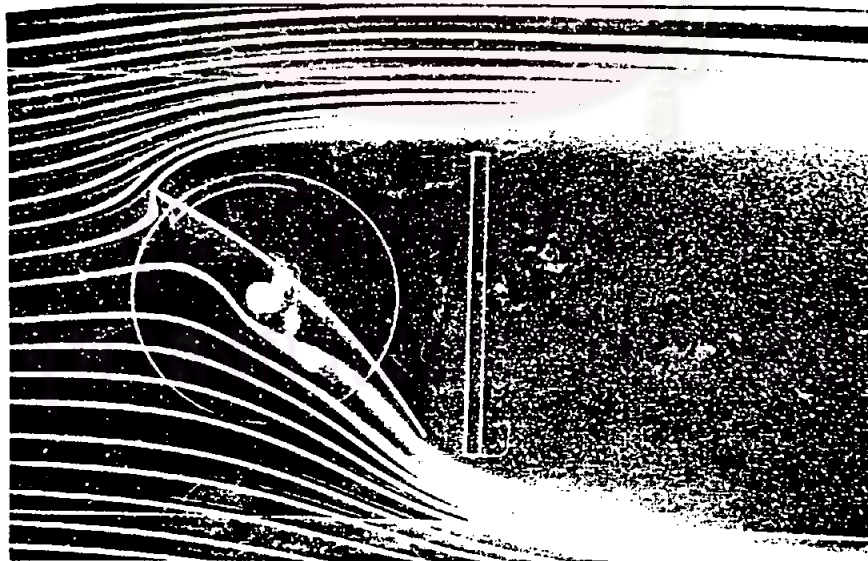



Fig. C.72 Attack angle = 40 degrees



ARCHED PLATE WITH STICK AT BACK

RE = 64000

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Fig. C.73 Attack angle = -15 degrees

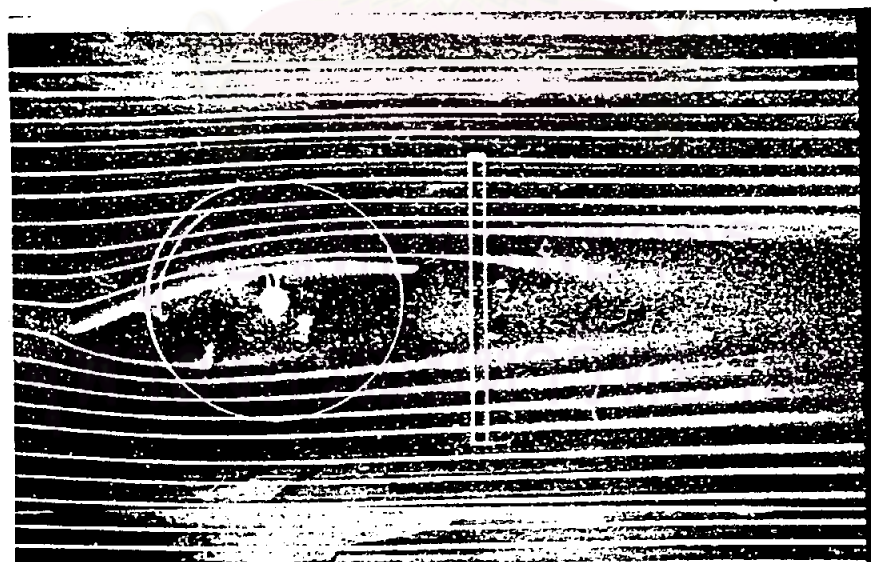


Fig. C.74 Attack angle = -10 degrees



Fig. C.75 Attack angle =  $-5$  degrees

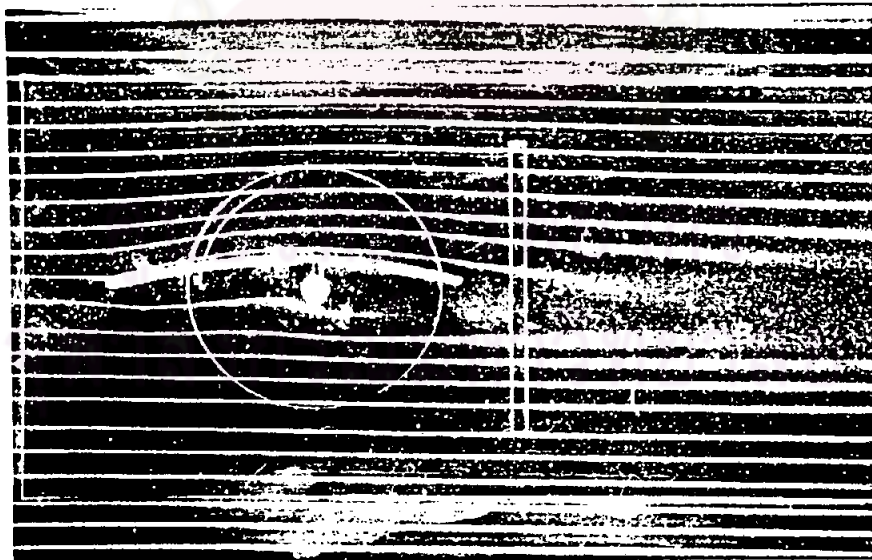


Fig. C.76 Attack angle =  $0$  degrees



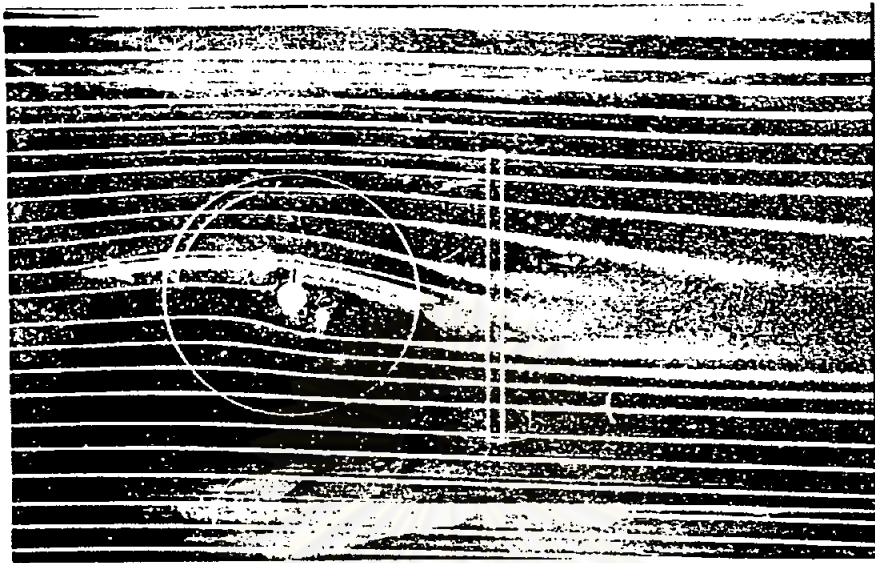


Fig. C.77 Attack angle = 5 degrees

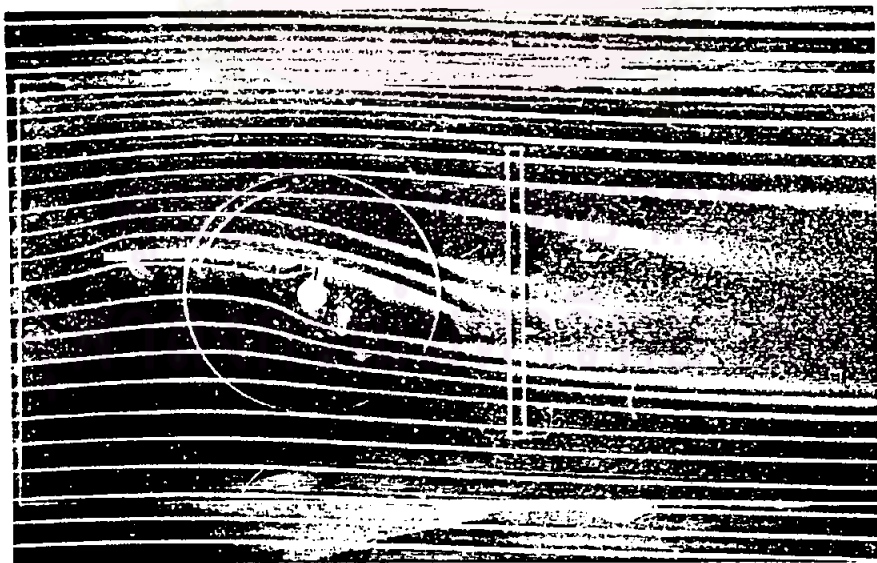


Fig. C.78 Attack angle = 10 degrees

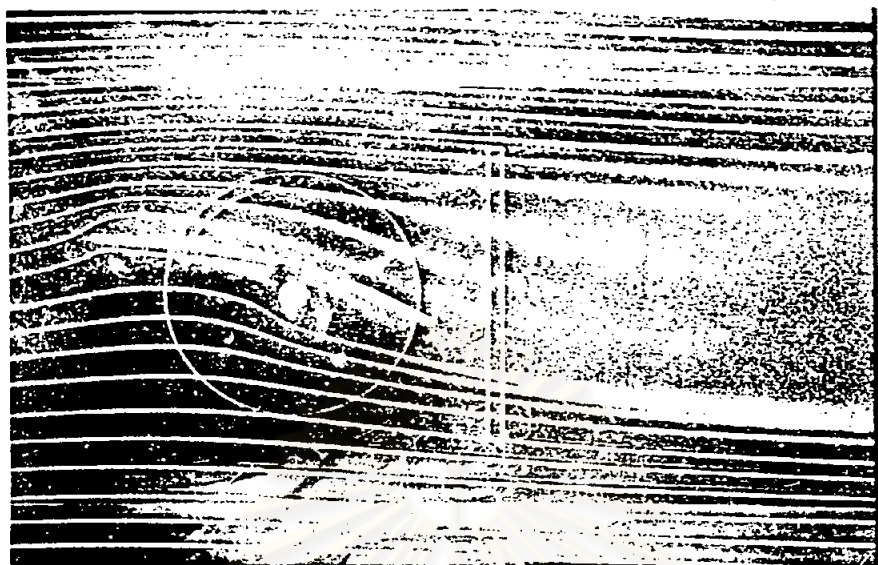


Fig. C.79, Attack angle = 15 degrees

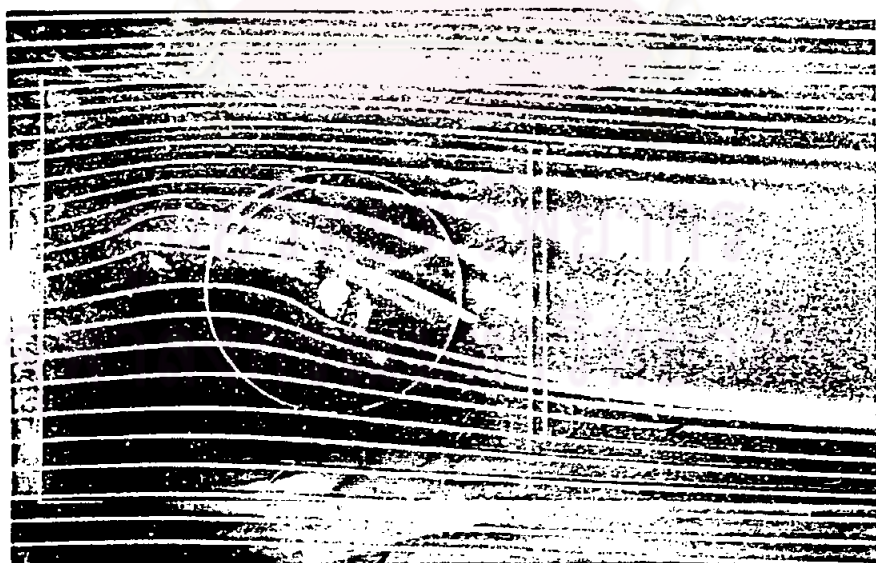


Fig. C.80, Attack angle = 20 degrees



Fig. C.81 Attack angle = 25 degrees

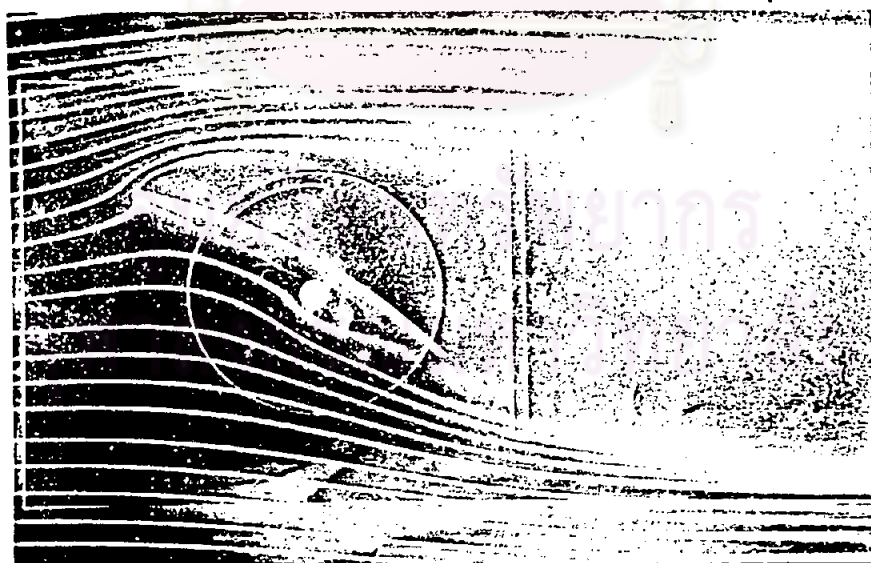


Fig. C.82 Attack angle = 30 degrees

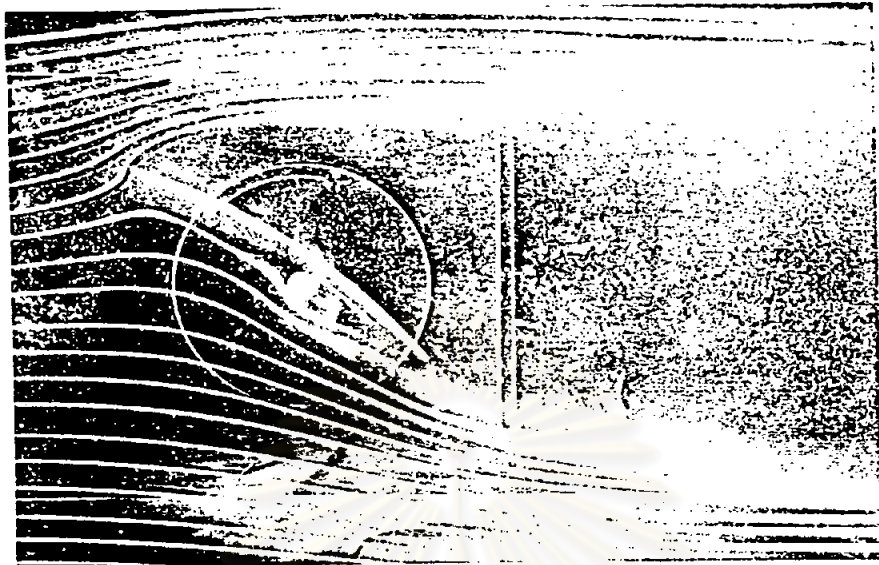


Fig. C.83, Attack angle = 35 degrees

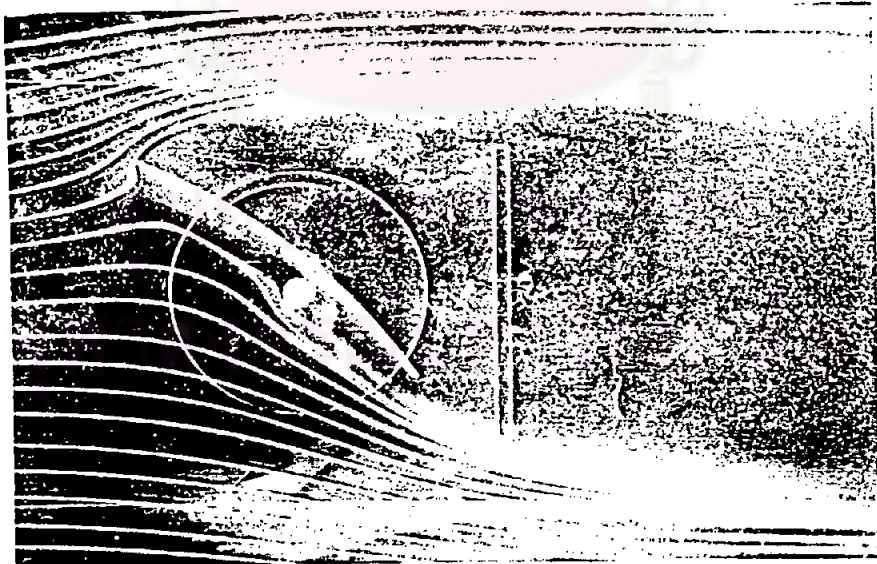


Fig.C.84 Attack angle = 40 degrees

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## Resume

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