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นางสาวกฤติกา เลิศสวัสดิ์



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PREDICTION OF NOISE EMISSION FROM POWER PLANT BY A MATHEMATICAL MODEL

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พิมพ์ตันฉบับบทคัดย่อวิทยานิพนธ์ภายในกรอบสีเขียวนี้เพียงแผ่นเดียว

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หลักการแพร่กระจายของเสียงภายนอกอาคารถูกนำมาใช้พัฒนาแบบจำลองคณิตศาสตร์ในการทำนาย ค่าระดับเสียงจากโรงไฟฟ้ากังหันแก๊ส เพื่ออธิบายค่าความไม่แน่นอนของแบบจำลองคณิตศาสตร์ มีการตรวจวัด ระดับความดันเสียง (Sound Pressure Level, SPL) ณ โรงไฟฟ้าระยอง ในช่วงฤดูแล้ง ตามมาตรฐาน ISO1996/1 และ Equals Angle Method คำนวณค่าระดับกำลังเสียง (Sound Power Level, PWL) ของแหล่งกำเนิดเสียงตามมาตรฐาน ISO 3476 การตรวจวัดและการคำนวณเพื่อพิจารณาเลือกแหล่งกำเนิดเสียงที่สำคัญในการใช้แบบจำลองคณิตศาสตร์ ใช้วิธีการหาค่า PWL ของแหล่งกำเนิดเสียงหลักจากการตรวจวัด SPL ภายนอกอาคาร แหล่งกำเนิดเสียงที่สำคัญที่ใช้ คือ อาคารแหล่งกำเนิดเสียงหลัก (Main Building) และหอหล่อเย็น (Cooling Tower) คำนวณ PWL ของแหล่งกำเนิดเสียงหลักส่วนข้าย ขวา และ ตรงกลาง มีค่าเท่ากับ 114.7, 112.9, และ 118.2 เดชิเบล ตามลำดับ ค่า PWL ของอาคาร หอหล่อเย็น มีค่าเท่ากับ 116.7 เดชิเบล ในขณะที่ทำการตรวจวัด SPL ณ จุดรับเสียงใด ๆ ภายนอกอาคาร ได้ทำการ เก็บค่าข้อมูลของค่าแก้ไขระหว่างทางเดินเสียงในแต่ละเส้นทางเดินเสียงในสิ่งในสิ่งแวดล้อมไปด้วย

ผู้ทำการศึกษาได้พัฒนาโปรแกรมคอมพิวเตอร์ด้วยโปรแกรมภาษา Visual Basic เพื่อช่วยการคำนวณใน แบบจำลองนี้ โปรแกรมสามารถนำเข้าค่า SPL จากการตรวจวัด เพื่อคำนวณ PWL จากแหล่งกำเนิดเสียงอุตสาห กรรม หรือค่า PWL จากข้อมูลพื้นฐานของเครื่องจักร และข้อมูลของค่าแก้ไขของเส้นทางเดินเสียงต่างๆ เพื่อใช้ คำนวณค่าระดับเสียง ณ จุดใด ๆ ภายนอกอาคาร เมื่อนำค่า SPL ที่คำนวณได้เปรียบเทียบกับค่า SPL ที่ตรวจวัดได้ จริง ผลการเปรียบเทียบจะนำไปใช้อธิบายระดับความถูกต้องของแบบจำลองคณิตศาสตร์นี้ จากกราฟการกระจาย ตัวของข้อมูลแสดงช่วงของค่าความถูกต้องของแบบจำลองคณิตศาสตร์ที่เบี่ยงเบนไปจากเส้นสมดุล เมื่อมีการ พิจารณาสภาวะการณ์ที่เหมาะสมแล้ว มีค่าอยู่ในช่วง 10 เดซิเบล จากข้อมูลที่ตรวจวัดได้ นอกจากนี้ยังพบว่าที่จุด ตรวจวัดระดับเสียงในเขตอิทธิพลของด้านเหนือลม ค่า SPL ที่จุดตรวจวัดมีค่าต่ำกว่าค่าที่ได้จากการคำนวณของ แบบจำลองคณิตศาสตร์ และค่าแก้ไขทิศทางของแหล่งกำเนิดเสียง (Directivity) ซึ่งเกิดจากตำแหน่งที่ตั้งของแหล่ง กำเนิดเสียงและสภาพแวดล้อมมีผลต่อผลการที่ทำนายได้จากแบบจำลองคณิตศาสตร์ด้วย

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The principles of outdoor sound propagation were used to a develop power plant noise prediction model in order to illustrate the accuracy level of the mathematical model. Sound Pressure Level (SPL) measurements were conducted during dry season at the Rayong Combined Cycle Power Plant (RPP) following the ISO 1996/1 and equal angle methods. Measurement and calculation methods for determining the significant sound source of the prediction model involved the determination of the Sound Power Level (PWL) using SPL measurement in outdoor environment according to ISO 3746. The representative noise sources were the main buildings and the cooling towers. The PWLs of both sound sources were calculated by Colenbrander's method and the area surface method. The PWLs of the left, right, and central parts of the main building were 114.7, 112.9, and 118.2 decibels, respectively. The PWL of the cooling tower was 116.7 decibels. During measurement at any point in the outdoor environment, the transfer function data of each transmission path were collected.

The author developed a computer program using the Visual Basic programming language in order to perform this model calculation. The program can use measured SPLs for calculating the PWL of an industrial sound source, or it can use the PWL from the machine's database and transfer function data to examine the SPL at any immission point in outdoor environment. Those predicted SPLs were compared with on-site measured SPLs. The comparison results were used to investigate the accuracy level of this model. Results showed that the accuracy level of the model is within 10 decibels from the measured data. It was also found that the measured SPL at immission positions under the influence of upwind conditions were lower than predicted levels and the directivity correction caused by source positions and the environment affects the predicted value.

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Contents

		Page
Thai Abs	tract	iv
	bstract	V
Acknowle	edgement	-
	HE	
	gures	
	mbols	
Chapter		All.
1	Introduction	1
	1.1 Background	1
	1.2 Objectives	
	1.3 Scope of Works	
2	Literature Review	
	2.1 Industrial Noise Characteristic	3
	2.2 General Noise Source from Combined Cycle Power Plant	
	2.3 Definitions	
	2.4 Noise Prediction model	7
	2.5 Power Plant Noise Prediction model	17
3	Methodology	
	3.1 Work Plan	
	3.2 Site selection and Description	
	3.3 Instruments	
	3.4 Measurement Method for RPP	34
	3.5 The Development of Power Plant Noise Prediction Model	
4	Results and Discussion	50
	4.1 Sound Pressure Measurement of Rayong Power Plant	50
	4.2 Calculated Sound Power Level of Noise Sources	70
	4.3 Sensitivity Analysis	
	4.4 Predicted Sound Pressure Level from Prediction Model	
5	Conclusion and Recommendation	88
	5.1 Conclusion	88
	5.2 Recommendation	90
	es	
Appendix	A Equipment Apparatus	96
Appendix	B Measured SPL Data	100
Appendix	C Details of Determination Procedure	114
Appendix	D Predicted Sound Pressure Level Data	125
	y	

List of Tables

Tab	le	Page
2-1	The decibel addition value	5
2-2 2-3	The center frequency band	6
	level in this table	6
2-4	Source directivity corrections for sound power determination	10
2-5	Large source position correction	
2-6	The correction term C _h for distance between source to	
	immission, r>= 100 m., if r < 100 m. the values in the table	
0.7	must be multiplied by r/100	13
2-7	Procedure step of the Standard method	13
2-8	The procedure of the specialist method	14
2-9	The near-field correction factors, E ₁ for small and large	
	source method	15
2-10	The near-field correction factors, E ₁ for linear source method	15
	Modal assumption	
	The equation for calculating area source	
	Reflecting obstacle specification	
	Reflecting obstacle coefficient, p	
2-15	The screening obstacles specification	24
2-16	The selecting method for more than two screen	.24
2-17	The calculation of the screening attenuation and more than	
	one effective screen	
2-18	Determination step for screening correction calculation	25
2-19	Definitions of different ground surface parts	28
2-20	Ground surface type characterization and values of	
	ground factors G	
2-21	The equations is used estimating the part of ground	29
	The main procedure step of the study	
3-2	Design Criteria	32
3-3	Plant performance per block, based on natural	
	gas site condtions	32
3-4	-,	32
3-5	Machine specification	33
3-6	Co-ordinates of microphone positions in terms of distances from	
	center of hemisphere along three mutually perpendicular axes (x,y,z).	37
3-7	Effective Microphone Height of Rectangular Measurement Surface	
3-8	Required data for input in each transmission path	
3-9	Criteria for identifying noise source determination	41

List of Tables (Cont.)

Tab	le ,	Page
4-1	Weather condition at RPP during the measurement	50
4-2	Noise sources, located inside plant's enclosure	71
4-3	Noise sourcees, located outside plant's enclosure	72
4-4	Comparison of measured SPL inside and outside enclosure room	72
4-5	(a) to (e) Point source PWL in decibel	73
	(a) Point source PWL in decibel	73
	(b) PWL in decibel by Colenbrander method	73
	(c) PWL in decibel by Solid surface method	73
	(d) PWL in decibel by Linear surface method	73
	(e) PWL in decibel by Area surface method	
4-6	General guidance noise limit at work	
4-7	Selected noise source for testing predicted immission noise	
	levels	76
4-8	Ranking criterial for transfer function	80
4-9	Selected transfer functions for the correction of prediction model	
5-1	The advantage and Limitation of the Sonic Software	

List of Figures

Figu	ire	Page
2-1 2-2	The combined cycle and the heat recovery steam generator Sound decay outdoor in free field and indoors in reverberant	3
	room	6
2-3 2-4	Direction coefficient	10
	point heights and immission height in hilly (a) to (f)	12
2-5	Noise source propagation path	19
2-6	Description of solid surface and Colenbrander surface	
2-7	Plan of transmission paths between source and immission point	
2-8	Main procedure of screening selection	
2-9	Plan view of screen	
	Geometrical parameter in vertical plane of screen correction Example illustrating a building's screen representation in	
	sectional view	26
2-12	Sectional view illustrating the general situation when more	
	than one screen intersect the vertical plane	26
2-13	Sectional view illustrating the selection procedure n = 5,	
	highest elevation of SM _j is found for j=q=1 and highest	
2-14	elevation of IM _j is found for j=k=4	27
2-15	attenuation for two screen, nos. q and k	27
	particularly the horizontal transmission path differences	27
3-1	The photograph of Rayong Power Plant	31
3-2	Measurement Surface of Point Source determination Method according to ISO 3746. (ISO, 1979)	36
3-3	The methodology for development of prediction model	39
3-4	The development of computer software for power plant noise	39
	prediction model	40
3-5	The determination procedure of sound source, applied in RPP's	
	study	
3-6	Determination of the measurement area of the rectangular surface	
3-7	Point source calculation method	43
3-8	Microphone position for Colenbrander's method	44
3-9	Solid surface method microphone position	44
3-10	Linear surface method for non-point source determination	44
3-11	Area surface method for non-point source determination	44
	Diagram of PWL determination using Colenbrander's method	
3-13	Diagram of PWL determination using solid surface method	45
	Diagram of PWL determination using linear surface method	
	Diagram of PWL determination using area surface method	
3-16	All band level and A-weighted level calculation method	47

List of Figures (Cont.)

Figu	re	Page
4-1	Rayong Power Plant (RPP) Plan Layout	49
4-2	Measurement position for grid-system method inside the main building	51
4-3	Measured SPL at node of grid box inside the main building	52
4-4	(a) 63 Hz measured SPL inside the main building	53
4-4	(b) 125 Hz measured SPL inside the main building	54
4-4	(c) 250 Hz measured SPL inside the main building	55
4-4	(d) 500 Hz measured SPL inside the main building	56
4-4	(e) 1000 Hz measured SPL inside the main building	57
4-4	(f) 2000 Hz measured SPL inside the main building	
4-4	(g) 4000 Hz measured SPL inside the main building	
4-4	(h) 8000 Hz measured SPL inside the main building	
4-5	Measurement point of measured SPL for noise source	
4-6	Contour map of measured SPL for noise source determination	
4-7	(a) to (d) 1/1 Octave band measured SPL for noise source	
	determination	63
4-7	(e) to (h) 1/1 Octave band measured SPL for noise source	
	determination	64
4-8	Measurement point of measured SPL at immission point	
4-9	Contour map of measured SPL at immission point	
	(a) to (d) Contour map of measured SPL at immission point	
	(e) to (h) Contour map of measured SPL at immission point	
	Transmission path for noise prediction model	
	Divergence sensitivity by varying "R" distance	
	Relationship of divergence attenuation and air absorption attenuation	
	with the same "R" distance	79
4-14	Wind conditions influent sound wave	
	Noise source directivity correction	
	The comparison between measured SPL and predicted SPL with	
	divergence attenuation	
4-17	The comparison between measured SPL and predicted SPL	
	with divergence attenuation, air absorption attenuation,	
	and ground effect corrections	82
4-18	The comparison between measured SPL and predicted SPL	-
	with divergence attenuation, air absorption attenuation,	
	and ground effect corrections excluding the adjacent position	
	of small sources	83
4-19	The comparison between measured SPL and predicted SPL	
7 10	with divergence attenuation, air absorption attenuation,	
	and ground effect corrections excluding the adjacent position	
	of small sources and the upwind conditions	83
4-20	(a) The contour map of selected SPL measured at immission point	100
	(b) The contour map of predicted SPL considered immission point	
	(c) Overlay map of measured SPL and predicted SPL with the same	
	conditions	0/

List of Symbols

Symbols	Units	Description	Location
p	Pascals	root-mean-square sound pressure	Eq.2.5
p ₀	Pascals	reference root-mean-square sound pressure (2 x 10 -5 Pa)	Eq.2.5
W	watts	sound power of a given source	Eq.2.6, 2.9, 2.10
W ₀	watts	reference sound power (generally 10 -12 W)	Eq.2.6
PWL, L	decibels	sound power level	Eq.2.6, 2.7, 2.8, 2.23,
	decibeis	Sourid power level	
CDL I	desibale		2.31-2.37, 2.39-2.40, 2.42
SPL, Lp	decibels	sound pressure level	Eq.2.4, 2.5, 2.8, 2.15, 2.23
			2.24, 2.34-2.36, 2.40
SPLout	decibels	sound pressure level outside enclosure wall	Eq.2.43, 2.44
SPLin	decibels	sound pressure level inside enclosure wall	Eq.2.43, 2.44
SPL	decibels	Sound pressure level at an ith immission point	Eq. 2.38
		1 TO SECTION OF THE PROPERTY O	
SPL	decibels	Average sound pressure level at the measurement surface	Eq.2.37, 2.38
_p (r)	decibels	sound pressure level at source-receiver distance	Eq.2.15
L _{pi}	decibels	sound pressure level in the measurement position no. i	Eq.2.23, 2.25
$\overline{L_p}$	decibels	The energy average of sound pressure level [re 20 µPa]	Eq.2.31-2.35
K	•	a function of the environment in which the sound source is	Eq.2.7, 2.39
		located (to be zero in outdoor measurement)	
d	meters	distance between source and immission point	Eq.2.8, 2.15, 2.47,
			Table 2-18
	W/m²	sound intensity	Eq.2.9, 2.10
	meters	distance far away from center of source	
	meters		Eq.2.9, 2.16, 2.17, 2.40
4		total room absorption (sabines)	Eq.2.10
u	Hz	upper frequencies of octave band	Eq.2.11, 2.12, 2.13
	Hz	lower frequencies of octave band	Eq.2.11, 2.12, 2.13, 2.14
c	Hz	central frequencies of octave band	Eq.2.12-2.14
Ol _{revr}	decibels	source directivity index in the receiver direction	Eq.2.15
2	degree	solid angle at the source that is available for sound propagation	Eq.2.15
	decibels	combined attenuation from all significant propagation	The control of the co
A _{combined,re}	decibeis		Eq.2.15
ır		mechanisms between source and receiver	
downwind	decibels	effective octave-band sound power level in the direction of	Eq.2.16
		propagation(re 1 picowatt)	
L _{WD}	decibels	sound pressure level at an receiver shall be calculated for each	Eq.2.16, 2.18
		point source and octave band with nominal midband	
		frequencies from 63 Hz to 8 kHz	
A	decibels	octave-band attenuation during propagation from the point	Eq.2. 17
	decibeis		Lq.2. 17
	de elle elle	source to the receiver	- 0.17
div	decibels	attenuation due to geometrical divergence	Eq.2.17
A _{atm}	decibels	attenuation due to air absorption	Eq.2.17
ground	decibels	attenuation due to the ground effect	Eq.2.17
A _{refl}	decibels	attenuation due to reflections by obstacles	Eq.2.17
Screen	decibels	attenuation due to screening	Eq.2.17
misc	decibels	attenuation due to miscellaneous other effects	Eq.2.17
	decibels	directivity correction to the sound power level	
DC			Eq.2.19
DI	decibels	directivity index, indicated the sound pressure level of sound	Eq.2.20, 2.19
		source in the direction of propagation under consideration	
		exceeds that of a non-directional point source of the same	
		power at the same distance	
K ₀	_	correction index for emission into restricted solid angles or large	Eq.2.20, 2.21
		source position correction	
	decibels	Immission sound pressure level	Eq.2.23
5			Eq.2.23
O _s	decibels	Divergence attenuation correction	Eq.2.20
D	decibels	summation of correction for noise propagation or transfer	Eq.2.22
		function or attenuation correction	Takes and the same of the same
D _{BM}	decibels	correction of meteorological effect (ground effects and air	Eq.2.25
		temperature)	
Ω	radius	large source position angle correction (see Table 2-6)	Eq.2.21
D _L	decibels	correction of air absorption (temperature and relative humidity)	Eq.2.22
Company of the contract of the	decibels	correction of reflecting obstacles	
\mathcal{O}_{D}			Eq.2.22
O_{G}	decibels	correction of residential obstacles	Eq.2.22
DE	decibels	correction of sound screening	Eq.2.22
–p(tij)	decibels	sound pressure level contributing via transmission path no. t	Eq.2.23
		from source no. j (dB re 20 μPa) in 1/1 octave band no.i at	
	Market Control of the	immission point	

			(Cont.)
Symbols	Units	Description	Location
$L_{w}(\Phi_{t})_{ij}$	decibels	sound power level (dB re 1 pW) in direction Φ_t of transmission	Eq.2.23
		path no. t in 1/1 octave band no. 1 for source no. j	
∆L _{tij}	decibels	transfer function value (dB) in 1/1 octave band no.i for	Eq.2.23
		transmission path no. t between source no. j and immission	
		point	
$L_w(\Phi)$	decibels	horizontal directive or immission relevant sound power level in Φ	Eq.2.23
		direction [dB re 1pW]	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
ΔL_{Φ}	decibels	correction for directional effects in a horizontal plane	Eq.2.24
E	GOODOIO	a near field correction term, always between 0 and 3 dB.	
		dependent on the ratio between the surface areas of the	Eq.2.24
•		reference box and the measurement box	
A	meter	Width of rectangular surface of solid surface method	Eq.2.40, 2.41
В	meter	Lenght of rectangular surface of solid surface method	Eq.2.40, 2.41
S	meters ²	measurement surface area	Eq.2.28, 2.37, 2.38, 2.39,
			2.43
S ₀	meters ²	reference surface area	Eq.2.43
K _i	decibels	environment correction in the same position	Eq.2.29
N	-	number of measurement position	Eq.2.29
ΔL _d	dB		
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		correction taking into account the effect of divergence	Eq.2.25
ΔLa	dB	correction taking into account the effect of air absorption	Eq.2.25
ΔLr	dB	correction taking into account the effect of reflecting obstacles	Eq.2.25
ΔL_s	dB	correction taking into account the effect of screening	Eq.2.25
AL,	dB	correction taking into account the effect of vegetation	Eq.2.25
ΔLi	dB	correction taking into account the effect of internal scattering	Eq.2.25, 2.33
	dB	correction taking into account the effect of ground	
	The second secon		Eq.2.25
4	dB	sound pressure level at immission point	Eq.2.27, 2.26
-pA	dB	noise level at the reference point	Eq.2.26
C _n	dB	adjustment for the number of measurements	Eq.2.26
Cref		adjustment for the distance different between the reference and	Eq.2.26
		the immission points	_4
ΔCh		height correction term(Table 2.7)	Ea 2 26
	dB		Eq.2.26
-WR	A STATE OF THE STA	immission relevant sound power level of the source	Eq.2.28, 2.27, 2.29
R _r	meters	distance between source and measuring point	Eq.2.28
D _{bodem}	dB	Ground attenuation	Eq.2.28
a _{lu}	dB/m	air absorption important with long distance and high frequencies	Eq.2.28
D _{geo}	dB	attenuation in the noise level due to geometric propagation	Eq.2.30, 2.36
Dair	dB	attenuation in the noise level due to absorption in the air	Eq.2.30, 2.36
D _{refl}	dB	attenuation due to reflections against obstacles (this term is	Eq.2.30, 2.36
- 1011		negative)	Lq.2.50, 2.50
	dB		F-000 000
D _{screen}	UB	attenuation as a result of screening by acoustically well	Eq.2.30, 2.36
		insulating obstacles	
O _{veg}	dB	attenuation due to noise scattering and absorption by vegetation	Eq. 2.30
D _{site}	dB	attenuation due to scattering and absorption by installations on	Eq. 2.30
		the industrial site in so far as this is not included in the other	
		terms (internal scattering)	
Oground	dB	attenuation as a result of reflections against, scattering by and	Eq. 2.30
ground	u.D	absorption from the ground	Lq. 2.50
	dD.		F 000
Duilding	dB	attenuation due to reflections against buildings in the vicinity of	Eq. 2.30
		the receiver (Also the influence of noise propagation through	
		built-up areas is included in this term)	
=2	dB	environmental correction factor is equal to	Eq.2.31, 2.32, 2.37
		10 log ₁₀ (1+ (4S/R))	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,
= _{1Q}	dB	near -field correction (Table 2.10)	Eq.2.32
E _{1R}	dB	The near-field correction (Table 2.11)	
-1R	meters	width of source surface	Eq.2.33
			Table 2-12
)	meters	length of source surface	Eq.2.39, Table 2-12
\L	dB	attenuation correction factors of outdoor sound propagation	Eq.2.45
1		over all numbers of the measurement points at the	Eq.2.38
		measurement surfaces	
Sc	m ²	area within the contour	Eq.2.45
\L _{div}	dB	Divergence attenuation correction	Eq.2.45, 2.46, 2.47
	dB		
Lair	ub .	Air absorption by means of temperature and relative humidity	Eq.2.45, 2.48
	4D	attenuation correction	
L _{ref}	dB	Reflecting obstacles attenuation correction	Eq.2.45, 2.49
Lscr	dB	Screening obstacles attenuation correction	Eq.2.45
L_{grd}	dB	Ground effects correction	Eq.2.45, 2.50
₹,	m ²	Displacement between source and immission point, meters(R _d	Eq.2.45, 2.47, 2.50
		$= d^2 + (H_s - H_i)^2)$	

Company I	11.2		(Cont.)
Symbols	Units	Description	Location
H _s	meters	Height of source	Eq.2.46, 2.47
H _i	meters	Height of immission	Eq.2.46, 2.47
α_a	dB/m	air absorption coefficient	Eq.2.48
ρ		reflection coefficient of the surface of the reflecting obstacle (Table 2.15)	Eq.2.49, 2.50
K _P		intersection between the line SI from the source S to the immission point I and the screen representation	Table 2-18
T _P		intersection between the screen top edge and the vertical plane	Table 2-18
Q _P		intersection between the screen plane and the curved transmission path from S to I as it would have	Table 2-18
		been in the absence of the screen	
d ₁	meters	Horizontal distance from the source to the screen	Table 2-18
d ₂	meters	Horizontal distance from the immission point to the screen	Table 2-18
δν	meters	vertical transmission path difference	Table 2-18
δ_{r}	meters	horizontal transmission path difference on the right vertical edge	Table 2-18
δι	meters	vertical edge vertical transmission path difference on the left vertical edge	Table 2-18
N _v	-	Fresnel number of the vertical transmission path difference	Table 2-18
N _r	-	Fresnel number of the right horizontal transmission path difference	Table 2-18
Nı		Fresnel number of the left horizontal transmission path difference	Table 2-18
f _c	Hz	Octave band center frequency	Table 2-18
Ϋ́t	meters	Height of screen top	Table 2-18
Hg	meters	Height of lowest ground surface	Table 2-18
$\Delta \tilde{L}_{g,s}$	dB	Ground effects correction of source part	Eq.2.50
$\Delta L_{g,i}$	dB	Ground effects correction immission part	Eq.2.50
$\Delta L_{g,c}$	dB	Ground effects correction center part between source and immssion	Eq.2.50
H _{e1}		Effecitive height of screen no. 1	Table 2-16
H _{e2}		Effective height of screen no. 2	Table 2-16
d _{s1}	meters	Distance from source to the nearest screen included in the calculation of δ_{ν}	Table 2-16
d _{i2}	meters	Distance from immission point to the nearest screen included in the calculation of δ_v	Table 2-16
RPP		Rayong Power Plant	
GT		Gas Turbine	
ST		Steam Turbine	
S		South direction	table 4.1
SE		South direction Southeast direction	table 4-1
SW		Southwest direction	table 4-1
W		West direction	table 4-1
		Vest direction Calm	table 4-1
C K			table 4-1
•	-	Environmental Factor	eq.2.37