CHAPTER 3

PRESENTATION OF ANALYTICAL AIDS

3.1 The Rigidity Ratio

Expressed as the ratio of the flexural rigidity to the torsional rigidity the parameter m plies with the expressions for redundants as derived in Chapter 2. As this research identifies solely with rectangular beam sections of reinforced concrete the rigidity ratio m can be written in terms of the cross-sectional dimensions t and b, the thickness t being always greater than, at least equal to, the width b. The imposition of a Poisson's ratio of 0.15 on the known relation

$$G = \frac{E}{2(1+\mu)}$$

results in $\frac{G}{E}=\frac{1}{2.3}$. The moment of inertia of the beam section with respect to the horizontal axis assumes the familiar expression

$$I = \frac{1}{12} bt^3$$

With reference to Timoshenko and Goodier the expression for the polar moment of inertia of the beam section takes the form

$$J = Cb^3t$$

¹ S. Timoshenko and J.N. Goodier, Theory of Elasticity
(New York; McGraw-Hill Book Co., 1951), pp. 275-278.

wherein

$$C = \frac{1}{3} \left| 1 - \frac{192}{15} \cdot \frac{b}{t} \right|_{n=1,3,5,\dots}^{n=\infty} \frac{1}{n^5} \tanh \frac{n^{1}t}{2b}$$

It follows that

$$m = \frac{2.3}{12C} \cdot \frac{t^2}{b^2}$$



(3.1)

3.2 The S-beam

Evidently the S-beam solution as directed by relations (2.9) to (2.16) exhibits a complex nature as they assimilate compound trigonometric terms. Such trait furnishes justification for development of a graphical presentation enabling a rapid handling of the problem in the design office. The graphical aids represented by Charts 3.1 and 3.2 bring forward values of the redundants M_{\odot} and T for practical ranges of values of \emptyset and $\frac{t}{b}$. Computerised numerical values of M and T forming the basis for the institution of the graphical aids, as tabulated in Appendix B, draw on the following input values of \emptyset and $\frac{t}{b}$:

$$\phi$$
 = 15, 30, 45,, and 120 degrees; and

 $\frac{t}{b}$ = 1.0, 1.1, 1.2, 1.3, 1.4, 1.5, 1.6, 1.7, 2.0, 2.5, 3.0, and 4.0

3.3 The Z-beam

Although expressions (2.23) and (2.24) for the redundant M and T appear relatively simple their graphical presentation, Charts 3.3, and 3.4 has been registered. Computerised numerical values of these redundants, as listed in Appendix B, correspond to identical input values of $\frac{t}{b}$ set forth in Article 3.2, and to the following input values of k:

 $k = 0, 0.1, 0.2, 0.3, \dots, and 2.00$







