CHAPTER II

A HEATED TO HOUVE THE BOUATION OF A VIBRATING

NON - UNIPORM BAR

We shall first start the method by considering a symmetrical non-uniform bur vibrating under its own weight; the load per unit length is equal to the inertial load due to its mass and acceleration⁴. The rate of change of the moment along the bar is equal to the shear. We find, by using these relations, that the Buler equation² for the bar should be

$$\frac{\partial^2}{\partial x^2} \left[S(x) \ x^2(x) \ \frac{\partial^2 \psi}{\partial x^2} \right] = -\rho \frac{S(x)}{Q} \frac{\partial^2 \psi}{\partial x^2} \tag{1}$$

To study the normal modes of the periodic vibration phenomena we can assume that

 $\psi = \mathbf{Y}(\mathbf{x}) e^{\pm \omega \mathbf{t}}$

⁴ WILLIAH 7. THOMSON, <u>Vibration Theory and Amplication</u> (Engle wood Cliffs, N.J.: Prentice-Hall, Inc., 1965), p.275.

² APRINCE HEORMETZ, <u>Advanced Nathematics in Firmics</u> and Hagineering. (New York: McGraw-Hill Company, Inc., 1953), p.151-153. and then the eq. (1) can be reduced to the form

$$\frac{d^2}{dx^2} | S(x) | x^2(x) \frac{d^2y}{dx^2} = \frac{d^2y(S(x))}{q} \cdot x$$
(2)

which is the equation of notion for a non-uniform bar. In this case we have the following boundary conditions:

$$\begin{aligned} y''_{(0)} &= y''_{(0)} &= 0 \\ y'(z_{10}) \neq 0, \ y'(z_{10}) = 0 \\ y''_{(x_{10})} \neq 0 \end{aligned}$$

and

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In the case of a rectangular cross-section with constant base b and variable altitude a(x) we have $\Im R^2 = \frac{n^3 b}{12}$. The next step is to substitute $\Re R^2 = \frac{n^3 b}{12}$ and $\Re = ab$

into equation (2). We have

$$\frac{d^2}{dx^2} \left(\frac{a^3(x)}{12} \right) \frac{d^2}{dx^2} y = a^2 \rho ab y$$

$$\frac{d^2}{dx^2} \left(a^3(x) \frac{d^2y}{dx^2} \right) = ar^2 a(x) y$$

where $c = \frac{1037^2 \rho}{Q}$, and for iron $\rho = 7.8 \text{ gm/cm}^3$

 $Q = 20 \times 10^{n} \text{ dyno/cn}^{2}$. Therefore $c = 0.185 \times 10^{-9} \text{ sec}^{2}/\text{cn}^{2}$

Putting $z = a^3y''$, we have the simultaneous equations as follows:

6

$$y'' = \frac{\pi}{a^3}$$
(4)

(5)

and s" = c 2² a y

Assume, for the symmetrical bar, that the length of the bar is divided into 20 equal parts. If $y_0, y_1, y_2, \dots, y_{20}$ denote the interal displacements at the points x_0, x_1, \dots, x_{20} , where x_0 and x_{20} are the end points. The finite difference approximation³ at x_1 for the equations

(4) and (5) are :

$$y_2 - 2y_1 + y_0 = h^2 - \frac{x_1}{x_2}$$

and.

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Using a step by step calculation we have

$$y_{2+1} = \frac{-1}{(u_1^3)} + 2y_1 - y_{1-1} \tag{6}$$

³ F.B.HILLDERAID, <u>Introduction to Mumerical Analysia</u>. (New York: McGrow-Hill book Company, Inc., 1956), p.91. $z_{1+1} = c 2^2 a_1 y_1 + 2 z_1 - z_{1-1}$

(7)

1 = 1,11 1 710 = 710

J'10 = 0.5 (J11 - J9)

J'10 = J11 - 2J10 + J9

 $y_{10}^{\prime\prime\prime} = 0.5 (y_{12} - 2y_{11} + 2y_9 - y_8)$

At the free end put $y_0 = -1$. This implies

y' = 0.5 (y - y) = 0. y is to be varied.

The boundary conditions, require $s_0 = 0$, $s'_0 = 0$. These imply $s_1 = s_{-1}$.

Therefore $y_1 = -y_{-1}$ (8) and $z_1 = \frac{\alpha x^2 a_0 y_0}{2}$ (9)

Given a(x1) and assuming some trial values for the frequency, the system can be solved by means of the digital computer (IBN 1620) as follows:

 $a(x_4) = a(x_{4+4}) = 1.0$

F = 1000, DF = 1000, $y_1 = -1.0$, $DX_1 = 0.2$ where F denotes frequency: DF denotes the increment of F: w_1 , denotes the displacement at x_1 , DX_1 denotes the increment of X_1 . The results obtained are shown in the tables 3 - 6; x_{10} is the center point. From these tables we can obtain the vibrating frequency and the mode shapes in the next chapter, which is necessary to refer frequently to mathematical concepts such as linear interpolation and inverse interpolation. For convenience these have been collected in the appendix.

Tables 3-6, the results obtained by using electronic computer (IEM 1620).

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F=1000	<i>3</i> 4	V40	710	710	J 310
		-1.7700	-3.10:0	-0.09703	-0.02136
	-0,8	0+5239	0.03765	-0,03480	-0,004964
	-0,6	2.8180	0.39470	0.02742	0.01744
	-0.4	5.1120	0.74580	0.08964	0.03665
	-0.2	7.1:070	1.09900	0,45480	0.05625
	0.0	9.7010	1.4540	0.21410	0.7566

Table 4

F=2000	34	y10	540	¥10	940
	1.0	-4+1700	-1.3450	-0,4430	-0.1206
	-0.8	-0.9762	-0+5109	-0.1799	-0.03199
	-0.6	2.2170	0+3231	0.08311	0.05662
	-0,13	5+4110	1.1570	0.3462	0.1452
	-0+2	8,6060	1+9910	0.6093	0.2338
	0.0	11.8000	2.8250	0.8724	0.3224

Table 5

IPmls000	94 -1.0	y ₁₀ -15.1100	940 -6.6830	710 -2.6880	910
	-0.8	-8,0760	-3.6590	-1-4040	-0.5520
	-0,6	-1.0340	-0+6359	-0.1195	-0.01429
	-0.4	6,0080	2.3870	1.1650	0.5234
	-0.2	13:0500	5.4110	2.4490	1.0610
	0.0	20,0900	8.4350	3.7340	1.5980

Table 6

Mode shapes for F = 4000 Hz.

У ₀	54	y2	¥3	y _{l4}	¥5
-1.00	-1.00	-1.0148000	-1.0888000	-1.2964380	-1.7443806
-1.00	-0.80	-0.6148000	-0.4828800	-0.4609180	-0.6198854
-1.00	-0.60	-0.2148000	0.1230400	0.3746019	0.5046097
-1.00	-0.40	0.1852000	0.7289600	1.2101219	1.6291049
-1.00	-0,20	0.5852999	1.3348800	2.0456420	2.7536003
-1.00	0.00	0.9852000	1.9048000	2.8811620	3.8780955

УG	7 377	38	39	340
-2.577689	-3.9929777	-6.2632808	-9.7797440	-15.1189270
-1.0443966	-1.8374147	-3.1328170	-5.1188682	-8.0765640
0.4888754	0.3181476	-0.0023544	-0.4579942	1.0342051
2.0221478	2.4737107	3.1281094	4-2028816	6.0081570
3.5554202	4.6292736	6.2585729	8.8637570	13.0505190
5.0886925	6.7848370	9.3690380	13-5246350	20.0928830

By varying the inputs we generate another set of data as follows: F = 1000, DF = 100, $X_4 = 1.0$, $DX_4 = 0.1$ The results obtained are shown in the table 7 - 14.

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	εc	3.3			

F=1000	34	y10	340	y10	340
	-1.00	-1.770000	-0.316400	-0.097030	-0.021360
	-0.90	-0.623200	-0.139300	-0.065910	-0.011660
	-0.80	0.523900	0.037650	-0.034800	-0.001961
	-0.70	1.671000	0.214700	-0.003690	+0.007744
	-0,60	2.818000	0.391700	0+027420	0.017140
	-0.50	3.965000	0.568700	0.058530	0.027440

Table 8

F=1100	34	y10	y40	y10	y10
	-1.00	-1.934000	-0.384500	-0.118500	-0.026580
	-0.90	-0.755800	-0.191100	-0.080760	-0.041:750
	-0,80	0.422400	0.002268	-0,042960	-0.002875
	-0.70	1.600000	0.195600	-0.005171	0.008980
		2.779000	0.389000	0.032620	0.020830
	-0.50	3.957000	0.582500	0.070420	0.032690

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12.1	0.0	.	n . 1	G2 .
	60, BA			1

F=1200	34	y10	J40	340	340
1	-1.00	-2-114000	-0.459800	0.142600	-0+032590
	-0.90	-0.901700	-0, 248400	0.097420	-0.018330
	-0.80	0.310600	-0.037000	0.052250	-0.004078
1999 P	-0.07	1.523000	0.174400	0.070760	0.010180
	-0.60	2.735000	0.385800	0.038090	0.024440
	+0.50	3.947000	0.597200	0.083270	0.038700

Table 10

F=1300	34	y40	540	· 310	310
	-1.00	-2.310000	-0.5/12/100	0.169200	-0.039480
	-0.90	-1.061000	-0.311300	0.116000	0.022550
	-0,80	0.1884.00	-0.080310	0.062750	-0.005626
	-0.70	1.438000	0.150700	0,009482	0.011300
	-0.60	2.687000	0.381800	0.0437800	0.028230
	-0.50	3.937000	0.612800	0.097050	0.045160

Table 14

₩=1 400	34	340	¥10	¥10	310
	-1.00	-0.523000	-0.632600	-0.198700	-0.047330
	-0.90	-1.334000	-0.380200	-0.136600	-0.027450
	-0.80	0.055640	-0.127800	-0.074560	-0.00758
	-0.70	1.345000	0.124500	-0.012470	0.012290
	-0,60	2.635000	0.376900	0.0196100	0.032160
	-0,50	3.925000	0.629300	0.111700	0.052040

Table 12

F=1500	¥4	¥40	340	340	340
	-1.00	-2.754000	-0.730500	-0.231100	-0.056230
	-0,90	-1+421000	-0.455000	-0.159400	-0.033120
	-0.80	-0.087990	-0.179600	-0.087810	-0.010000
	-0.70	1.245000	0.095760	-0.016140	0.013000
	-0.60	2+578000	0.371100	0.055510	0.036210
	-0.50	3.911000	0.646600	0.127100	0.059330

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Table 13

₽ =1 600	74	\$10	540	540	¥40
	-1.00	-3.001000	-0.836400	0.266600	-0.066300
	-0.90	-1.622000	-0.536200	04184600	-0.039640
	-0.80	-0.242600	-0.236000	-0.102600	-0.012980
	-0.70	1.113600	0.064140	-0.020590	0.013670
	-0,60	2.516000	0.364300	0.061100	0.040330
	-0.50	3. 896000	0.564500	0. 143400	0.067000

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F=1700	34	340	540	340	J10
	-1.00	-3.266000	0.950500	-0.305300	-0. 077650
	-0.90	-1.837000	0.623800	-0.212200	-0.047110
	-0.80	-0.408500	0.297100	-0.119000	-0.016580
	-0.70	1.020000	0.029540	-0:025930	0.013950
	-0.66	2.14,9000	0.356200	000067200	0.044480
	-0.50	3.878000	0.682900	0.160300	0.075020

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