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TABLE 1
A B C D CONSTANTS FOR 636 MCM ACSR CONDUCTOR A1/S1 = 54/7 STRANDS
BY IBM 1620 DIGITAL COMPUTER

DISTANCE		A = D in p.u.	B in p.u.	C in p.u.
Km.	Mile			
700	433	0.72257970 + j0.06902598	0.22492694 + j1.01291150	-0.01150739 + j0.45398780
620	385	0.78268930 + j0.05406990	0.20886093 + j0.91493591	-0.00797732 + j0.41067593
435	270	0.89312230 + j0.02659265	0.15908455 + j0.66541606	-0.00275080 + j0.29943780
425	264	0.89781970 + j0.02542388	0.15607383 + j0.65161776	-0.00257094 + j0.29325908
275	171	0.95713020 + j0.01066660	0.10538274 + j0.43015682	-0.00069828 + j0.19383883
265	165	0.96008580 + j0.00993120	0.10189136 + j0.41545240	-0.00062686 + j0.18722368
185	115	0.98061100 + j0.00482425	0.07201348 + j0.29143964	-0.00021160 + j0.13139302
160	99	0.98563090 + j0.00357523	0.06220440 + j0.25128775	-0.00013489 + j0.11330386
80	50	0.99633480 + j0.00091195	0.03164272 + j0.12733971	-0.00001587 + j0.05742824

Base KV = 230 KV
 Base MVA = 200 MVA

△ eq spacing = 26 ft.
 Base Z = 264.5 ohms.

TABLE 2
A B C D CONSTANTS FOR 795 MCM ACSR CONDUCTOR Al/st = 54/7 Strands
BY IBM 1620 DIGITAL COMPUTER

DISTANCE		A = D	B	C
KM	MILE	in p.u.	in p.u.	in p.u.
700	435	0.72227470 + j0.05685122	0.18198722 + j0.99426551	-0.00964632 + j0.46197306
620	385	0.78245030 + j0.04453308	0.16899899 + j0.89853965	-0.00668656 + j0.41791000
435	270	0.89300480 + j0.02190225	0.12873576 + j0.65405459	-0.00230644 + j0.30472516
425	264	0.89770730 + j0.02093963	0.12629990 + j0.64051448	-0.00215568 + j0.29843799
275	171	0.95708310 + j0.00878523	0.08528315 + j0.42301156	-0.00058455 + j0.19726675
265	165	0.96004190 + j0.00817954	0.08245787 + j0.40856011	-0.00052636 + j0.19053522
185	115	0.98058970 + j0.00397335	0.05827944 + j0.28664677	-0.00017722 + j0.13371798
160	99	0.98561510 + j0.00294463	0.05034128 + j0.24716401	-0.00011109 + j0.11530878
80	50	0.99633080 + j0.00075110	0.02560828 + j0.12525948	-0.00001323 + j0.05844392

Base KV = 230 KV

Δ eq. spacing = 26 ft.

Base MVA = 200 MVA

Base Z = 264.5 ohms.

TABLE 3
A B C D CONSTANTS FOR 954 MCM ACSR CONDUCTOR A1/st = 54/7 STRANDS
BY IBM 1620 DIGITAL COMPUTER

DISTANCE		A = D	B	C
KM	MILE	in p.u.	in p.u.	in p.u.
700	435	0.72210770 + j0.04747611	0.14980407 + j0.97945183	-0.00817041 + j0.46857762
620	385	0.78231950 + j0.03718930	0.13911753 + j0.88543100	-0.00566559 + j0.42389299
435	270	0.89294040 + j0.01829043	0.10597933 + j0.64486449	-0.00195201 + j0.30909470
425	264	0.89764580 + j0.01748656	0.10397428 + j0.63152877	-0.00170085 + j0.30271761
275	171	0.95705730 + j0.00733649	0.07020977 + j0.41719228	-0.00049462 + j0.20009689
265	165	0.96001790 + j0.00683068	0.06788393 + j0.40294506	-0.00044436 + j0.19327015
185	115	0.98057810 + j0.00331812	0.04797931 + j0.28273353	-0.00015077 + j0.13563825
160	99	0.98560650 + j0.00245904	0.04144420 + j0.24379525	-0.00009522 + j0.11696455
80	50	0.99632860 + j0.00062724	0.02108248 + j0.12355813	-0.00001058 + j0.05928503

Base KV = 230 KV
 Base MVA = 200 MVA

△ eq. spacing = 26 ft.
 Base Z = 264.5 ohms.

TABLE 4
A, B, C, D CONSTANTS FOR 1113 HCM ACSR CONDUCTOR Al/St = 54/19 STRANDS

BY IBM 1620 DIGITAL COMPUTER

DISTANCE		A = D	B	C
Km	MILES	in p.u.	in p.u.	in p.u.
700	435	0.72201130 + j0.04115643	0.12822109 + j0.96672884	-0.00717324 + j0.47452623
620	385	0.78224400 + j0.03223893	0.11907660 + j0.87408722	-0.00497260 + j0.42927557
435	270	0.89290330 + j0.01585575	0.09071513 + j0.63680192	-0.00171396 + j0.31302517
425	264	0.89761030 + j0.01515888	0.08899897 + j0.62364086	-0.00160287 + j0.30656608
275	171	0.95704240 + j0.00635991	0.06009845 + j0.41204661	-0.00043378 + j0.20264403
265	165	0.96000400 + j0.00592143	0.05810760 + j0.39797818	-0.00039146 + j0.19573000
185	115	0.98057130 + j0.00287643	0.04106976 + j0.27926327	-0.00013225 + j0.13736543
160	99	0.98560150 + j0.00213171	0.03547582 + j0.24080603	-0.00008199 + j0.11845368
80	50	0.99632730 + j0.00054375	0.01804644 + j0.12204650	-0.00001058 + j0.06003886

Base kV = 230 kV

Base MVA = 200 MVA

△ eq. spacing = 26 ft.

Base Z = 264.5 ohms.

TABLE 5
A B C D CONSTANTS FOR 1272 MCM ACSR CONDUCTOR Al/st = 54/19 STRANDS
BY IBM 1620 DIGITAL COMPUTER

DISTANCE		A - D	B	C
KM	MILE	in p.u.	in p.u.	in p.u.
700	435	0.72198890 + j0.03652320	0.11254310 + j0.95579822	-0.00643529 + j0.47975539
630	385	0.70222650 + j0.02860960	0.10451721 + j0.86430143	-0.00446212 + j0.43400747
435	270	0.89289470 + j0.01407077	0.07962407 + j0.62979546	-0.01153675 + j0.31647425
425	264	0.89760200 + j0.01345235	0.07811776 + j0.61678412	-0.00143888 + j0.30994639
275	171	0.95703890 + j0.00564394	0.05275086 + j0.40755644	-0.00038882 + j0.20487906
265	165	0.96000080 + j0.00525482	0.05100343 + j0.39364321	-0.00034914 + j0.19788832
185	115	0.98056980 + j0.00255261	0.03604865 + j0.27623055	-0.00011638 + j0.13887837
160	99	0.98560030 + j0.00189173	0.03113863 + j0.23819284	-0.00007406 + j0.11975767
80	50	0.99632700 + j0.00048253	0.01584013 + j0.12072413	-0.00000794 + j0.06070011

Base KV = 230 KV
 Base MVA = 200 MVA

△ eq spacing = 26 ft.
 Base Z = 264.5 ohms.

TABLE 6
A B C D CONSTANTS FOR 1431 MCM ACSR CONDUCTOR A1/st = 54/19 STRANDS
BY IBM 1620 DIGITAL COMPUTER

DISTANCE		A = D in p.u.	B in p.u.	C in p.u.
KN	MILE			
700	435	0.72204290 + j0.03286862	0.10035536 + j0.94653145	-0.00584545 + j0.48421486
620	385	0.78226880 + j0.02574687	0.09319759 + j0.85598461	-0.00405214 + j0.43804110
435	270	0.89291550 + j0.01266282	0.07099919 + j0.62381440	-0.00139656 + j0.31941285
425	264	0.89762190 + j0.01210628	0.06965600 + j0.61092979	-0.00130663 + j0.31282415
275	171	0.95704720 + j0.00507919	0.04703645 + j0.40371387	-0.00035443 + j0.20677817
265	165	0.96000860 + j0.00472901	0.04547830 + j0.38993311	-0.00031740 + j0.19972395
185	115	0.98057350 + j0.00229719	0.03214346 + j0.27363294	-0.00010580 + j0.14016913
160	99	0.98560310 + j0.00170244	0.02776533 + j0.23595419	-0.00006877 + j0.12087121
80	50	0.99632770 + j0.00043425	0.01412412 + j0.11959083	-0.00000794 + j0.06126349

Base KV = 230 KV

△ eq Spacing = 26 ft.

Base MVA = 200 MVA

Base Z = 264.5 ohms

TABLE 2

A B C D CONSTANTS FOR 1590 MCM ACSR CONDUCTOR Al/St = 54/19 STRANDS
 BY IBM 1620 DIGITAL COMPUTER

DISTANCE		A = D	B	C
KM	MILE	in p.u.	in p.u.	in p.u.
700	435	0.72178530 + j0.02988462	0.09042134 + j0.93873776	-0.00536142 + j0.48847331
620	385	0.78206700 + j0.02340942	0.08397659 + j0.84900438	-0.00371623 + j0.44190279
435	270	0.89281620 + j0.01151321	0.06398003 + j0.61881308	-0.00128018 + j0.32224299
425	264	0.89752700 + j0.01100720	0.06276983 + j0.60603523	-0.00119819 + j0.31559347
275	171	0.95700740 + j0.00461808	0.04238817 + j0.40050748	-0.00032534 + j0.20861379
265	165	0.95997150 + j0.00429968	0.04098407 + j0.38683742	-0.00029095 + j0.20149610
185	115	0.98055550 + j0.00208864	0.02896739 + j0.27146696	-0.00009787 + j0.14141228
160	99	0.98558980 + j0.00154788	0.02502193 + j0.23408779	-0.00006084 + j0.12194508
80	50	0.99632430 + j0.00039482	0.01272865 + j0.11864630	-0.00000794 + j0.06180836

Base KV = 230 KV

eq Spacing = 26 ft.

Base MVA = 200 MVA

Base Z = 264.5 ohms

TABLE 8

LOADING CONDITIONS OF 7 CONDUCTOR SIZES AT VARIOUS PERCENTAGE
OF COMPENSATION AT RECEIVING END

ACSR MCM	E_R /0.0	$S_R = P_R + jQ_R$	Q_X %	I_R	E_S	I_S	$S_S = P_S + jQ_S$	
636	1.0	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.722+j0.069	0.725/5.5°	-0.0115+j0.4539	0.0230-j0.3288
	1.0	0.0000+j0.0000	0.1000	0.0000-j0.1000	0.823+j0.046	0.825/3.2°	-0.0046+j0.3817	0.0139-j0.3147
	1.0	0.0000+j0.0000	0.2000	0.0000-j0.2000	0.925+j0.024	0.925/1.5°	0.0022+j0.3094	0.0095-j0.2862
	1.0	0.0000+j0.0000	0.3000	0.0000-j0.3000	1.026+j0.001	1.026/0.1°	0.0092+j0.2372	0.0098-j0.2434
	1.0	0.0000+j0.0000	0.4000	0.0000-j0.4000	1.127-j0.020	1.127/-0.1°	0.0161+j0.1649	0.0147-j0.1863
	1.0	0.4000+j0.3000	0.0000	0.4000-j0.3000	1.116+j0.406	1.188/20.0°	0.2982+j0.2648	0.4406-j0.1743
	1.0	0.4000+j0.3000	-0.1000	0.4000-j0.2000	1.015+j0.429	1.102/22.9°	0.2913+j0.3370	0.4404-j0.2171
	1.0	0.4000+j0.3000	-0.2000	0.4000-j0.1000	0.913+j0.451	1.019/26.3°	0.2844+j0.4093	0.4448-j0.2455
	1.0	0.4000+j0.3000	-0.3000	0.4000-j0.0000	0.812+j0.474	0.940/30.2°	0.2775+j0.4815	0.4538-j0.2597
	1.0	0.4000+j0.3000	-0.4000	0.4000+j0.1000	0.711+j0.496	0.867/34.9°	0.2706+j0.5538	0.4675-j0.2595
795	1.0	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.722+j0.056	0.724/4.5°	-0.0096+j0.4619	0.0192-j0.3342
	1.0	0.0000+j0.0000	0.1000	0.0000-j0.1000	0.821+j0.038	0.822/2.6°	-0.0039+j0.3897	0.0118-j0.3204
	1.0	0.0000+j0.0000	0.2000	0.0000-j0.2000	0.921+j0.020	0.921/1.3°	0.0017+j0.3175	0.0080-j0.2924
	1.0	0.0000+j0.0000	0.3000	0.0000-j0.3000	1.020+j0.002	1.020/0.1°	0.0074+j0.2452	0.0081-j0.2503
	1.0	0.0000+j0.0000	0.4000	0.0000-j0.4000	1.119-j0.015	1.120/-0.8°	0.0130+j0.1730	0.0119-j0.1940
	1.0	0.4000+j0.3000	-0.0000	0.4000-j0.3000	1.093+j0.399	1.164/20.1°	0.2963+j0.2680	0.4311-j0.1745
	1.0	0.4000+j0.3000	-0.1000	0.4000-j0.2000	0.993+j0.418	1.078/22.8°	0.2906+j0.3402	0.4311-j0.2166
	1.0	0.4000+j0.3000	-0.2000	0.4000-j0.1000	0.894+j0.436	0.995/26.0°	0.2849+j0.4124	0.4348-j0.2446
	1.0	0.4000+j0.3000	-0.3000	0.4000-j0.0000	0.795+j0.454	0.915/29.7°	0.2792+j0.4847	0.4423-j0.2584
	1.0	0.4000+j0.3000	-0.4000	0.4000+j0.1000	0.695+j0.472	0.841/34.2°	0.2735+j0.5569	0.4536-j0.2580

(TO BE CONTINUED)

TABLE 8 (CONT'D)

ACSR MCK	$\frac{E_R}{/0.0}$	$S_R = P_R + jQ_R$	$\frac{Q_X}{\%}$	I_R	E_S	I_S	$S_S = P_S + jQ_S$	
954	1.0	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.722+j0.047	0.723/3.7°	-0.0081+j0.4685	0.0163-j0.3387
	1.0	0.0000+j0.0000	0.1000	0.0000-j0.1000	0.820+j0.032	0.820/2.3°	-0.0034+j0.3963	0.0100-j0.3251
	1.0	0.0000+j0.0000	0.2000	0.0000-j0.2000	0.917+j0.017	0.918/1.1°	0.0013+j0.3241	0.0068-j0.2975
	1.0	0.0000+j0.0000	0.3000	0.0000-j0.3000	1.015+j0.002	1.015/0.1°	0.0060+j0.2519	0.0068-j0.2559
	1.0	0.0000+j0.0000	0.4000	0.0000-j0.4000	1.11+j0.012	1.113/-0.6°	0.0108+j0.1797	0.0098-j0.2003
	1.0	0.4000+j0.3000	0.0000	0.4000-j0.3000	1.075+j0.394	1.145/20.2°	0.2949+j0.2709	0.4241-j0.1752
	1.0	0.4000+j0.3000	-0.1000	0.4000-j0.2000	0.977+j0.409	1.060/22.7°	0.2901+j0.3431	0.4242-j0.2168
	1.0	0.4000+j0.3000	-0.2000	0.4000-j0.1000	0.879+j0.424	0.976/25.7°	0.2854+j0.4153	0.4273-j0.2444
	1.0	0.4000+j0.3000	-0.3000	0.4000-j0.0000	0.782+j0.439	0.896/29.3°	0.2806+j0.4875	0.4336-j0.2580
	1.0	0.4000+j0.3000	-0.4000	0.4000+j0.1000	0.684+j0.454	0.821/33.6°	0.2759+j0.5597	0.4430-j0.2576
1113	1.0	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.722+j0.041	0.723/3.3°	-0.0071+j0.4745	0.0143-j0.3429
	1.0	0.0000+j0.0000	0.1000	0.0000-j0.1000	0.818+j0.028	0.819/2.0°	-0.0030+j0.4023	0.0088-j0.3294
	1.0	0.0000+j0.0000	0.2000	0.0000-j0.2000	0.915+j0.015	0.915/1.0°	0.0010+j0.3301	0.0060-j0.3021
	1.0	0.0000+j0.0000	0.3000	0.0000-j0.3000	1.012+j0.002	1.012/0.1°	0.0051+j0.2579	0.0059-j0.2610
	1.0	0.0000+j0.0000	0.4000	0.0000-j0.4000	1.108-j0.010	1.108/-0.5°	0.0092+j0.1857	0.0084-j0.2060
	1.0	0.4000+j0.3000	0.0000	0.4000-j0.3000	1.063+j0.389	1.132/20.1°	0.2939+j0.2743	0.4194-j0.1772
	1.0	0.4000+j0.3000	-0.1000	0.4000-j0.2000	0.966+j0.402	1.046/22.6°	0.2898+j0.3465	0.4195-j0.2184
	1.0	0.4000+j0.3000	-0.2000	0.4000-j0.1000	0.869+j0.415	0.963/25.5°	0.2857+j0.4187	0.4223-j0.2457
	1.0	0.4000+j0.3000	-0.3000	0.4000-j0.0000	0.773+j0.427	0.883/28.9°	0.2816+j0.4909	0.4278-j0.2591
	1.0	0.4000+j0.3000	-0.4000	0.4000+j0.1000	0.676+j0.440	0.807/33.0°	0.2775+j0.5631	0.4359-j0.2587

(TO BE CONTINUED)

TABLE 8 (CONT'D)

ACSR MCM	$\frac{E}{0.0}$	$S_R = P_R + jQ_R$	$\frac{Q_X}{\%}$	I_R	E_S		I_S	$S_S = P_S + jQ_S$
1272	1.0	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.721+j0.036	0.722/2.9°	-0.0064+j0.4797	0.0128-j0.3466
	1.0	0.0000+j0.0000	0.1000	0.0000-j0.1000	0.817+j0.025	0.817/1.7°	-0.0027+j0.4075	0.0080-j0.3332
	1.0	0.0000+j0.0000	0.2000	0.0000-j0.2000	0.913+j0.014	0.913/0.9°	0.0008+j0.3353	0.0054-j0.3062
	1.0	0.0000+j0.0000	0.3000	0.0000-j0.3000	1.008+j0.002	1.008/0.1°	0.0045+j0.2631	0.0052-j0.2654
	1.0	0.0000+j0.0000	0.4000	0.0000-j0.4000	1.104-j0.008	1.104/-0.4°	0.0081+j0.1909	0.0074-j0.2109
	1.0	0.4000+j0.3000	0.0000	0.4000-j0.3000	1.053+j0.385	1.121/20.1°	0.2933+j0.2777	0.4160-j0.1797
	1.0	0.4000+j0.3000	-0.1000	0.4000-j0.2000	0.958+j0.396	1.036/22.4°	0.2896+j0.3499	0.4162-j0.2205
	1.0	0.4000+j0.3000	-0.2000	0.4000-j0.1000	0.862+j0.407	0.954/25.3°	0.2860+j0.4221	0.4187-j0.2475
	1.0	0.4000+j0.3000	-0.3000	0.4000-j0.0000	0.767+j0.418	0.873/28.5°	0.2823+j0.4943	0.4236-j0.2609
	1.0	0.4000+j0.3000	-0.4000	0.4000+j0.1000	0.671+j0.430	0.797/32.6°	0.2787+j0.5665	0.4308-j0.2605
1431	1.0	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.722+j0.032	0.722/2.6°	-0.0058+j0.4842	0.0116-j0.3498
	1.0	0.0000+j0.0000	0.1000	0.0000-j0.1000	0.816+j0.022	0.817/1.5°	-0.0025+j0.4120	0.0073-j0.3365
	1.0	0.0000+j0.0000	0.2000	0.0000-j0.2000	0.911+j0.012	0.911/0.8°	0.0007+j0.3398	0.0050-j0.3096
	1.0	0.0000+j0.0000	0.3000	0.0000-j0.3000	1.006+j0.002	1.006/0.1°	0.0040+j0.2676	0.0047-j0.2691
	1.0	0.0000+j0.0000	0.4000	0.0000-j0.4000	1.100-j0.007	1.100/-0.4°	0.0073+j0.1953	0.0066-j0.2151
	1.0	0.4000+j0.3000	0.0000	0.4000-j0.3000	1.046+j0.381	1.113/20.0°	0.2928+j0.2807	0.4134-j0.1820
	1.0	0.4000+j0.3000	-0.1000	0.4000-j0.2000	0.951+j0.391	1.028/22.3°	0.2895+j0.3529	0.4136-j0.2225
	1.0	0.4000+j0.3000	-0.2000	0.4000-j0.1000	0.856+j0.401	0.946/25.1°	0.2862+j0.4251	0.4159-j0.2493
	1.0	0.4000+j0.3000	-0.3000	0.4000-j0.0000	0.762+j0.411	0.866/28.3°	0.2829+j0.4973	0.4203-j0.2626
	1.0	0.4000+j0.3000	-0.4000	0.4000+j0.1000	0.667+j0.421	0.789/32.3°	0.2796+j0.5695	0.4267-j0.2623

(TO BE CONTINUED)

TABLE 8 (CONT'D)

ACSR MCM	E_R /o.o°	$S_R = P_R + jQ_R$	α_{RX} %	I_R	E_S	I_S	$S_S = P_S + jQ_S$	
1590	1.0	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.721+j0.029	0.722/2.3°	-0.0053+j0.4884	0.0107-j0.3527
	1.0	0.0000+j0.0000	0.1000	0.0000-j0.1000	0.815+j0.020	0.815/1.4°	-0.0023+j0.4162	0.0067-j0.3396
	1.0	0.0000+j0.0000	0.2000	0.0000-j0.2000	0.909+j0.011	0.909/0.7°	0.0006+j0.3441	0.0046-j0.3129
	1.0	0.0000+j0.0000	0.3000	0.0000-j0.3000	1.003+j0.002	1.003/0.1°	0.0036+j0.2719	0.0043-j0.2728
	1.0	0.0000+j0.0000	0.4000	0.0000-j0.4000	1.097-j0.006	1.097/-0.3°	0.0065+j0.1997	0.0059-j0.2192
	1.0	0.4000+j0.3000	0.0000	0.4000-j0.3000	1.039+j0.378	1.106/20.0°	0.2923+j0.2838	0.4112-j0.1845
	1.0	0.4000+j0.3000	-0.1000	0.4000-j0.2000	0.945+j0.387	1.021/22.2°	0.2893+j0.3560	0.4115-j0.2246
	1.0	0.4000+j0.3000	-0.2000	0.4000-j0.1000	0.851+j0.396	0.939/24.9°	0.2863+j0.4282	0.4136-j0.2513
	1.0	0.4000+j0.3000	-0.3000	0.4000-j0.0000	0.757+j0.405	0.859/28.1°	0.2833+j0.5004	0.4176-j0.2644
	1.0	0.4000+j0.3000	-0.4000	0.4000+j0.1000	0.664+j0.414	0.782/31.9°	0.2803+j0.5726	0.4234-j0.2640

(RESULTS FROM IBM 1620 DIGITAL COMPUTER)

All in p.u.

Full Load = 100 MVA 0.8 p.f. lagging

Base kV = 230 KV

Base MVA = 200 MVA

Distance = 700 KM

TABLE 9

LOADING CONDITIONS OF 7 CONDUCTOR SIZES FOR TRANSMISSION LINE ALONE

AT $E_S = 0.98 - 1.02$ p.u.

ACSR MCM	E_R /p.u.	$S_R = P_R + jQ_R$	e_x %	I_R	E_S	I_S	$S_S = P_S + jQ_S$	
636	1.36	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.982 +j0.093	0.987/5.4°	-0.0156+j0.6174	0.0425-j0.6082
	1.37	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.989 +j0.094	0.994/5.4°	-0.0157+j0.6219	0.0432-j0.6171
	1.38	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.997 +j0.095	1.001/5.4°	-0.0158+j0.6265	0.0438-j0.6262
	1.383	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.999 +j0.095	1.003/5.4°	-0.0159+j0.6278	0.0440-j0.6289
	1.39	0.0000+j0.0000	0.0000	0.0000-j0.0000	1.004 +j0.095	1.008/5.4°	-0.0159+j0.6310	0.0444-j0.6353
	1.40	0.0000+j0.0000	0.0000	0.0000-j0.0000	1.011 +j0.096	1.016/5.4°	-0.0161+j0.6355	0.0451-j0.6445
795	1.36	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.982 +j0.077	0.985/4.5°	-0.0131+j0.6282	0.0356-j0.6181
	1.37	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.989 +j0.077	0.992/4.5°	-0.0132+j0.6329	0.0362-j0.6272
	1.38	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.996 +j0.078	0.999/4.5°	-0.0133+j0.6375	0.0367-j0.6364
	1.383	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.998 +j0.078	1.001/4.5°	-0.0133+j0.6389	0.0369-j0.6392
	1.39	0.0000+j0.0000	0.0000	0.0000-j0.0000	1.003 +j0.079	1.007/4.5°	-0.0134+j0.6421	0.0372-j0.6457
	1.40	0.0000+j0.0000	0.0000	0.0000-j0.0000	1.011 +j0.079	1.014/4.5°	-0.0135+j0.6467	0.0378-j0.6550
954	1.36	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.982 +j0.064	0.984/3.7°	-0.0111+j0.6372	0.0302-j0.6265
	1.37	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.989 +j0.065	0.991/3.7°	-0.0111+j0.6419	0.0306-j0.6358
	1.38	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.996 +j0.065	0.998/3.7°	-0.0112+j0.6466	0.0311-j0.6451
	1.383	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.998 +j0.065	1.000/3.7°	-0.0112+j0.6480	0.0312-j0.6479
	1.39	0.0000+j0.0000	0.0000	0.0000-j0.0000	1.003 +j0.065	1.005/3.7°	-0.0113+j0.6513	0.0315-j0.6545
	1.40	0.0000+j0.0000	0.0000	0.0000-j0.0000	1.010 +j0.066	1.013/3.7°	-0.0114+j0.6560	0.0320-j0.6639
1113	1.36	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.981 +j0.055	0.983/3.2°	-0.0097+j0.6453	0.0265-j0.6342
	1.37	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.989 +j0.056	0.990/3.2°	-0.0098+j0.6501	0.0269-j0.6436
	1.38	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.996 +j0.056	0.997/3.2°	-0.0098+j0.6548	0.0273-j0.6530
	1.383	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.998 +j0.056	1.000/3.2°	-0.0099+j0.6562	0.0274-j0.6558

(TO BE CONTINUED)

TABLE 9 (CONT'D)

ACSR MCM	E_R /0.0°	$S_R = P_R + jQ_R$	Q_X %	I_R	E_S	I_S	$S_S = P_S + jQ_S$	
1113	1.39	0.0000+j0.0000	0.0000	0.0000-j0.0000	1.003+j0.057	1.005/3.2°	-0.0099+j0.6595	0.0277-j0.6625
	1.40	0.0000+j0.0000	0.0000	0.0000-j0.0000	1.010+j0.057	1.012/3.2°	-0.0100+j0.6643	0.0281-j0.6721
1272	1.36	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.981+j0.049	0.983/2.9°	-0.0087+j0.6524	0.0238-j0.6410
	1.37	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.989+j0.050	0.990/2.9°	-0.0088+j0.6572	0.0241-j0.6505
	1.38	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.996+j0.050	0.997/2.9°	-0.0088+j0.6620	0.0245-j0.6600
	1.383	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.998+j0.050	0.999/2.9°	-0.0089+j0.6635	0.0246-j0.6629
	1.39	0.0000+j0.0000	0.0000	0.0000-j0.0000	1.003+j0.050	1.004/2.9°	-0.0089+j0.6668	0.0248-j0.6696
	1.40	0.0000+j0.0000	0.0000	0.0000-j0.0000	1.010+j0.051	1.012/2.9°	-0.0090+j0.6716	0.0252-j0.6793
1431	1.36	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.981+j0.044	0.982/2.6°	-0.0079+j0.6585	0.0216-j0.6470
	1.37	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.989+j0.045	0.990/2.6°	-0.0080+j0.6633	0.0219-j0.6565
	1.38	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.996+j0.045	0.997/2.6°	-0.0080+j0.6682	0.0222-j0.6661
	1.383	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.998+j0.045	0.999/2.6°	-0.0080+j0.6696	0.0223-j0.6690
	1.39	0.0000+j0.0000	0.0000	0.0000-j0.0000	1.003+j0.045	1.004/2.6°	-0.0081+j0.6730	0.0225-j0.6758
	1.40	0.0000+j0.0000	0.0000	0.0000-j0.0000	1.010+j0.046	1.011/2.6°	-0.0081+j0.6779	0.0229-j0.6856
1590	1.36	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.981+j0.040	0.982/2.3°	-0.0072+j0.6643	0.0198-j0.6524
	1.37	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.988+j0.040	0.989/2.3°	-0.0073+j0.6692	0.0201-j0.6620
	1.38	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.996+j0.041	0.996/2.3°	-0.0073+j0.6740	0.0204-j0.6717
	1.383	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.998+j0.041	0.999/2.3°	-0.0074+j0.6755	0.0205-j0.6746
	1.39	0.0000+j0.0000	0.0000	0.0000-j0.0000	1.003+j0.041	1.004/2.3°	-0.0074+j0.6789	0.0207-j0.6815
	1.40	0.0000+j0.0000	0.0000	0.0000-j0.0000	1.010+j0.041	1.011/2.3°	-0.0075+j0.6838	0.0210-j0.6913

RESULTS FROM TBM 1620 DIGITAL COMPUTER

All in p.u.

Base KV = 230 KV

Distance 700 KM

Base MVA = 200 MVA

TABLE 10

LOADING CONDITIONS AT NO LOAD AND FULL LOAD OF 7 CONDUCTOR SIZES

FOR $E_R = 0.9 - 1.0$ p.u.

ACSR MCM	E_R /0.0	$S_R = P_R + jQ_R$	Q_X %	I_R	E_S	I_S	$S_S = P_S + jQ_S$	
636	0.90	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.650+j0.062	0.653/5.4	-0.0103+j0.4085	0.0186-j0.2663
	0.91	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.657+j0.062	0.660/5.4	-0.0104+j0.4131	0.0190-j0.2723
	0.92	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.664+j0.063	0.667/5.4	-0.0105+j0.4176	0.0194-j0.2783
	0.93	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.671+j0.064	0.675/5.4	-0.0107+j0.4222	0.0199-j0.2844
	0.94	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.679+j0.064	0.682/5.4	-0.0108+j0.4267	0.0203-j0.2905
	0.95	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.686+j0.065	0.689/5.4	-0.0109+j0.4312	0.0207-j0.2967
	0.96	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.693+j0.066	0.696/5.4	-0.0110+j0.4358	0.0212-j0.3030
	0.97	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.700+j0.066	0.704/5.4	-0.0111+j0.4403	0.0216-j0.3094
	0.98	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.708+j0.067	0.711/5.4	-0.0112+j0.4449	0.0221-j0.3158
	0.99	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.715+j0.068	0.718/5.4	-0.0113+j0.4494	0.0225-j0.3222
	1.00	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.722+j0.069	0.725/5.4	-0.0115+j0.4539	0.0230-j0.3288
	0.90	0.0000+j0.0000	0.2000	0.0000-j0.2222	0.875+j0.012	0.875/0.8	0.0049+j0.2480	0.0073-j0.2170
	0.91	0.0000+j0.0000	0.2000	0.0000-j0.2197	0.880+j0.013	0.880/0.8	0.0046+j0.2543	0.0075-j0.2237
	0.92	0.0000+j0.0000	0.2000	0.0000-j0.2173	0.884+j0.014	0.885/0.9	0.0044+j0.2605	0.0077-j0.2305
	0.93	0.0000+j0.0000	0.2000	0.0000-j0.2150	0.889+j0.015	0.889/1.0	0.0041+j0.2668	0.0079-j0.2373
	0.94	0.0000+j0.0000	0.2000	0.0000-j0.2127	0.894+j0.017	0.894/1.1	0.0038+j0.2730	0.0081-j0.2442
	0.95	0.0000+j0.0000	0.2000	0.0000-j0.2105	0.899+j0.018	0.899/1.2	0.0035+j0.2791	0.0083-j0.2510
	0.96	0.0000+j0.0000	0.2000	0.0000-j0.2083	0.904+j0.019	0.904/1.2	0.0033+j0.2852	0.0085-j0.2580
	0.97	0.0000+j0.0000	0.2000	0.0000-j0.2061	0.909+j0.020	0.909/1.3	0.0030+j0.2913	0.0087-j0.2650
	0.98	0.0000+j0.0000	0.2000	0.0000-j0.2040	0.914+j0.021	0.915/1.3	0.0028+j0.2974	0.0090-j0.2720
	0.99	0.0000+j0.0000	0.2000	0.0000-j0.2020	0.919+j0.022	0.920/1.4	0.0025+j0.3034	0.0092-j0.2791
	1.00	0.0000+j0.0000	0.2000	0.0000-j0.2000	0.925+j0.024	0.925/1.5	0.0022+j0.3094	0.0092-j0.2862

(TO BE CONTINUED)

TABLE 10 (CONT'D)

ACSR MCM	$\frac{E_R}{G.C.}$	$S_R = P_R + jQ_R$	Q_X %	I_R	E_S	I_S	$S_S = P_S + jQ_S$	
636	0.90	0.0000+j0.0000	0.3000	0.0000-j0.3333	0.987-j0.012	0.988/0.7°	0.0126+j0.1677	0.0103-j0.1658
	0.91	0.0000+j0.0000	0.3000	0.0000-j0.3296	0.991-j0.011	0.991/0.6°	0.0122+j0.1749	0.0101-j0.1735
	0.92	0.0000+j0.0000	0.3000	0.0000-j0.3260	0.995-j0.009	0.995/0.6°	0.0119+j0.1820	0.0100-j0.1812
	0.93	0.0000+j0.0000	0.3000	0.0000-j0.3225	0.998-j0.008	0.998/0.5°	0.0115+j0.1891	0.0099-j0.1889
	0.94	0.0000+j0.0000	0.3000	0.0000-j0.3191	1.002-j0.006	1.002/0.5°	0.0112+j0.1961	0.0098-j0.1967
	0.95	0.0000+j0.0000	0.3000	0.0000-j0.3157	1.006-j0.005	1.006/0.5°	0.0108+j0.2031	0.0098-j0.2044
	0.96	0.0000+j0.0000	0.3000	0.0000-j0.3123	1.010-j0.004	1.010/0.2°	0.0105+j0.2100	0.0097-j0.2122
	0.97	0.0000+j0.0000	0.3000	0.0000-j0.3092	1.014-j0.002	1.014/0.1°	0.0101+j0.2168	0.0097-j0.2199
	0.98	0.0000+j0.0000	0.3000	0.0000-j0.3061	1.018-j0.001	1.018/0.1°	0.0098+j0.2237	0.0097-j0.2277
	0.99	0.0000+j0.0000	0.3000	0.0000-j0.3030	1.022+j0.000	1.022/0.0°	0.0095+j0.2304	0.0097-j0.2356
	1.00	0.0000+j0.0000	0.3000	0.0000-j0.3000	1.026+j0.001	1.026/0.1°	0.0092+j0.2372	0.0098-j0.2434
	0.90	0.4000+j0.3000	0.0000	0.4444-j0.3333	1.037+j0.437	1.172/21.9°	0.3337+j0.1984	0.4499-j0.0698
	0.91	0.4000+j0.3000	0.0000	0.4395-j0.3296	1.090+j0.433	1.173/21.7°	0.3299+j0.2052	0.4487-j0.0806
	0.92	0.4000+j0.3000	0.0000	0.4347-j0.3260	1.092+j0.430	1.174/21.5°	0.3260+j0.2120	0.4476-j0.0913
	0.93	0.4000+j0.3000	0.0000	0.4301-j0.3225	1.095+j0.427	1.175/21.3°	0.3223+j0.2188	0.4466-j0.1019
	0.94	0.4000+j0.3000	0.0000	0.4255-j0.3191	1.098+j0.424	1.177/21.1°	0.3186+j0.2255	0.4456-j0.1124
	0.95	0.4000+j0.3000	0.0000	0.4210-j0.3157	1.101+j0.421	1.178/20.9°	0.3151+j0.2321	0.4446-j0.1229
	0.96	0.4000+j0.3000	0.0000	0.4166-j0.3125	1.103+j0.418	1.180/20.8°	0.3115+j0.2387	0.4437-j0.1333
	0.97	0.4000+j0.3000	0.0000	0.4123-j0.3092	1.106+j0.415	1.182/20.6°	0.3081+j0.2453	0.4429-j0.1436
	0.98	0.4000+j0.3000	0.0000	0.4081-j0.3061	1.110+j0.412	1.184/20.4°	0.3047+j0.2518	0.4421-j0.1539
	0.99	0.4000+j0.3000	0.0000	0.4040-j0.3030	1.113+j0.409	1.186/20.2°	0.3014+j0.2583	0.4413-j0.1641
	1.00	0.4000+j0.3000	0.0000	0.4000-j0.3000	1.116+j0.406	1.188/20.0°	0.2982+j0.2648	0.4406-j0.1743

(TO BE CONTINUED)

TABLE 10 (CONT'D)

ACSR MCM	E_R /p.u.	$S_R = P_R + jQ_R$	G_X %	I_R	E_S	I_S	$S_S = P_S + jQ_S$	
636	0.90	0.4000+j0.3000	-0.2000	0.4444-j0.1111	0.862 +j0.487	0.990/29.4°	0.3184+j0.3589	0.4497-j0.1545
	0.91	0.4000+j0.3000	-0.2000	0.4395-j0.1098	0.867 +j0.483	0.993/28.9°	0.3147+j0.3640	0.4490-j0.1637
	0.92	0.4000+j0.3000	-0.2000	0.4347-j0.1086	0.872 +j0.479	0.995/28.8°	0.3110+j0.3691	0.4484-j0.1729
	0.93	0.4000+j0.3000	-0.2000	0.4301-j0.1075	0.877 +j0.475	0.998/28.6°	0.3075+j0.3742	0.4478-j0.1821
	0.94	0.4000+j0.3000	-0.2000	0.4255-j0.1063	0.882 +j0.471	1.000/28.1°	0.3040+j0.3792	0.4473-j0.1912
	0.95	0.4000+j0.3000	-0.2000	0.4210-j0.1052	0.887 +j0.468	1.003/27.8°	0.3005+j0.3842	0.4468-j0.2003
	0.96	0.4000+j0.3000	-0.2000	0.4165-j0.1041	0.892 +j0.464	1.006/27.5°	0.2972+j0.3893	0.4463-j0.2094
	0.97	0.4000+j0.3000	-0.2000	0.4123-j0.1030	0.898 +j0.461	1.009/27.2°	0.2939+j0.3943	0.4459-j0.2185
	0.98	0.4000+j0.3000	-0.2000	0.4081-j0.1020	0.903 +j0.458	1.012/26.9°	0.2906+j0.3993	0.4455-j0.2275
	0.99	0.4000+j0.3000	-0.2000	0.4040-j0.1010	0.908 +j0.454	1.016/26.6°	0.2875+j0.4043	0.4451-j0.2365
	1.00	0.4000+j0.3000	-0.2000	0.4000-j0.1000	0.913 +j0.451	1.019/26.3°	0.2844+j0.4093	0.4448-j0.2455
795	0.90	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.650 +j0.051	0.652/4.5°	-0.0086+j0.4157	0.0155-j0.2707
	0.91	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.657 +j0.051	0.659/4.5°	-0.0087+j0.4203	0.0159-j0.2767
	0.92	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.664 +j0.052	0.666/4.5°	-0.0088+j0.4250	0.0163-j0.2828
	0.93	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.671 +j0.052	0.673/4.5°	-0.0089+j0.4296	0.0166-j0.2890
	0.94	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.678 +j0.053	0.681/4.5°	-0.0090+j0.4342	0.0170-j0.2953
	0.95	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.685 +j0.054	0.688/4.5°	-0.0091+j0.4388	0.0174-j0.3016
	0.96	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.693 +j0.054	0.695/4.5°	-0.0092+j0.4434	0.0177-j0.3080
	0.97	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.700 +j0.055	0.702/4.5°	-0.0093+j0.4481	0.0181-j0.3144
	0.98	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.707 +j0.055	0.710/4.5°	-0.0094+j0.4527	0.0185-j0.3209
	0.99	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.715 +j0.056	0.717/4.5°	-0.0095+j0.4573	0.0189-j0.3275
	1.00	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.722 +j0.056	0.724/4.5°	-0.0096+j0.4619	0.0192-j0.3342

(TO BE CONTINUED)

TABLE 10 (CONT'D)

ACCR MCM	$\frac{E_R}{V.O.}$	$S_R = P_R + jQ_R$	$\frac{Q_X}{\%}$	I_R	E_S	I_S	$S_S = P_S + jQ_S$	
795	0.90	0.0000+j0.0000	0.2000	0.0000-j0.2222	0.870+j0.010	0.871/0.6°	0.0039+j0.2552	0.0061-j0.2222
	0.91	0.0000+j0.0000	0.2000	0.0000-j0.2197	0.875+j0.011	0.875/0.7°	0.0037+j0.2616	0.0063-j0.2291
	0.92	0.0000+j0.0000	0.2000	0.0000-j0.2173	0.880+j0.012	0.880/0.8°	0.0034+j0.2679	0.0064-j0.2359
	0.93	0.0000+j0.0000	0.2000	0.0000-j0.2150	0.885+j0.013	0.885/0.9°	0.0032+j0.2743	0.0066-j0.2428
	0.94	0.0000+j0.0000	0.2000	0.0000-j0.2127	0.890+j0.014	0.890/0.9°	0.0030+j0.2805	0.0068-j0.2498
	0.95	0.0000+j0.0000	0.2000	0.0000-j0.2105	0.895+j0.015	0.895/1.0°	0.0028+j0.2868	0.0070-j0.2567
	0.96	0.0000+j0.0000	0.2000	0.0000-j0.2083	0.900+j0.016	0.900/1.0°	0.0025+j0.2930	0.0072-j0.2638
	0.97	0.0000+j0.0000	0.2000	0.0000-j0.2061	0.905+j0.017	0.905/1.1°	0.0023+j0.2991	0.0074-j0.2709
	0.98	0.0000+j0.0000	0.2000	0.0000-j0.2040	0.910+j0.018	0.910/1.1°	0.0021+j0.3053	0.0076-j0.2780
	0.99	0.0000+j0.0000	0.2000	0.0000-j0.2020	0.915+j0.019	0.916/1.2°	0.0019+j0.3114	0.0078-j0.2852
	1.00	0.0000+j0.0000	0.2000	0.0000-j0.2000	0.921+j0.020	0.921/1.3°	0.0017+j0.3175	0.0080-j0.2924
	0.90	0.0000+j0.0000	0.3000	0.0000-j0.3333	0.981-j0.009	0.981/-0.5°	0.0102+j0.1750	0.0084-j0.1718
	0.91	0.0000+j0.0000	0.3000	0.0000-j0.3298	0.985-j0.008	0.985/-0.5°	0.0099+j0.1822	0.0083-j0.1796
	0.92	0.0000+j0.0000	0.3000	0.0000-j0.3260	0.988-j0.007	0.988/-0.4°	0.0096+j0.1894	0.0082-j0.1874
	0.93	0.0000+j0.0000	0.3000	0.0000-j0.3225	0.992-j0.005	0.992/-0.3°	0.0093+j0.1966	0.0081-j0.1952
	0.94	0.0000+j0.0000	0.3000	0.0000-j0.3191	0.996-j0.004	0.996/-0.2°	0.0090+j0.2037	0.0080-j0.2030
	0.95	0.0000+j0.0000	0.3000	0.0000-j0.3157	1.000-j0.003	1.000/-0.2°	0.0087+j0.2107	0.0080-j0.2108
	0.96	0.0000+j0.0000	0.3000	0.0000-j0.3125	1.004-j0.002	1.004/-0.1°	0.0085+j0.2177	0.0080-j0.2186
	0.97	0.0000+j0.0000	0.3000	0.0000-j0.3092	1.008-j0.001	1.008/0.0°	0.0082+j0.2247	0.0080-j0.2265
	0.98	0.0000+j0.0000	0.3000	0.0000-j0.3061	1.012+j0.000	1.012/0.0°	0.0079+j0.2316	0.0080-j0.2344
	0.99	0.0000+j0.0000	0.3000	0.0000-j0.3030	1.016+j0.001	1.016/0.0°	0.0076+j0.2384	0.0080-j0.2423
	1.00	0.0000+j0.0000	0.3000	0.0000-j0.3000	1.020+j0.002	1.020/0.1°	0.0074+j0.2452	0.0081-j0.2503

(TO BE CONTINUED)

TABLE 10 (CONT'D)

ACSR MCM	E_R / 3.0°	$S_R = P_R + jQ_R$	Q_X %	I_R	E_S	I_S	$S_S = P_S + jQ_S$	
795	0.90	0.4000+j0.3000	0.0000	0.4444-j0.3333	1.062+j0.432	1.146/22.1°	0.3312+j0.2002	0.4385-j0.0695
	0.91	0.4000+j0.3000	0.0000	0.4395-j0.3296	1.065+j0.428	1.148/21.9°	0.3274+j0.2072	0.4376-j0.0803
	0.92	0.4000+j0.3000	0.0000	0.4347-j0.3260	1.067+j0.425	1.149/21.2°	0.3236+j0.2142	0.4367-j0.0910
	0.93	0.4000+j0.3000	0.0000	0.4301-j0.3225	1.070+j0.421	1.150/21.5°	0.3200+j0.2210	0.4359-j0.1017
	0.94	0.4000+j0.3000	0.0000	0.4255-j0.3191	1.073+j0.418	1.152/21.3°	0.3164+j0.2279	0.4351-j0.1123
	0.95	0.4000+j0.3000	0.0000	0.4210-j0.3157	1.076+j0.415	1.154/21.1°	0.3129+j0.2347	0.4343-j0.1228
	0.96	0.4000+j0.3000	0.0000	0.4166-j0.3125	1.079+j0.411	1.155/20.9°	0.3094+j0.2414	0.4335-j0.1332
	0.97	0.4000+j0.3000	0.0000	0.4123-j0.3092	1.083+j0.408	1.157/20.7°	0.3060+j0.2481	0.4329-j0.1435
	0.98	0.4000+j0.3000	0.0000	0.4081-j0.3061	1.086+j0.405	1.159/20.5°	0.3027+j0.2548	0.4323-j0.1540
	0.99	0.4000+j0.3000	0.0000	0.4040-j0.3030	1.089+j0.401	1.161/20.3°	0.2995+j0.2614	0.4317-j0.1642
	1.00	0.4000+j0.3000	0.0000	0.4000-j0.3000	1.093+j0.399	1.164/20.1°	0.2963+j0.2680	0.4311-j0.1745
	0.90	0.4000+j0.3000	-0.1000	0.4444-j0.2222	0.951+j0.452	1.054/25.4°	0.3249+j0.2805	0.4363-j0.1199
	0.91	0.4000+j0.3000	-0.1000	0.4395-j0.2197	0.955+j0.448	1.055/25.2°	0.3212+j0.2866	0.4356-j0.1298
	0.92	0.4000+j0.3000	-0.1000	0.4347-j0.2173	0.959+j0.445	1.057/24.9°	0.3175+j0.2927	0.4350-j0.1396
	0.93	0.4000+j0.3000	-0.1000	0.4301-j0.2150	0.963+j0.441	1.060/24.6°	0.3139+j0.2987	0.4344-j0.1493
	0.94	0.4000+j0.3000	-0.1000	0.4255-j0.2127	0.967+j0.437	1.062/24.3°	0.3103+j0.3047	0.4338-j0.1591
	0.95	0.4000+j0.3000	-0.1000	0.4210-j0.2105	0.972+j0.434	1.064/24.1°	0.3069+j0.3107	0.4333-j0.1687
	0.96	0.4000+j0.3000	-0.1000	0.4166-j0.2083	0.976+j0.430	1.067/23.8°	0.3035+j0.3167	0.4328-j0.1784
	0.97	0.4000+j0.3000	-0.1000	0.4123-j0.2061	0.980+j0.427	1.069/23.6°	0.3002+j0.3226	0.4323-j0.1880
	0.98	0.4000+j0.3000	-0.1000	0.4081-j0.2040	0.985+j0.424	1.072/23.3°	0.2969+j0.3285	0.4319-j0.1975
	0.99	0.4000+j0.3000	-0.1000	0.4040-j0.2020	0.989+j0.421	1.075/23.0°	0.2937+j0.3344	0.4315-j0.2071
	1.00	0.4000+j0.3000	-0.1000	0.4000-j0.2000	0.993+j0.418	1.078/22.8°	0.2906+j0.3402	0.4311-j0.2166

(TO BE CONTINUED)

TABLE 10 (CONT'D)

ACSR MCM	\bar{z}_R /0.0°	$S_R = P_R + jQ_R$	Q_X %	I_R	E_S	I_S	$S_S = P_S + jQ_S$	
795	0.90	0.4000+j0.3000	-0.2000	0.4444-j0.1111	0.841+j0.472	0.965/29.3	0.3186+j0.3607	0.4387-j0.1529
	0.91	0.4000+j0.3000	-0.2000	0.4395-j0.1098	0.846+j0.468	0.967/29.0	0.3149+j0.3660	0.4381-j0.1621
	0.92	0.4000+j0.3000	-0.2000	0.4347-j0.1086	0.851+j0.464	0.970/28.6	0.3113+j0.3712	0.4377-j0.1714
	0.93	0.4000+j0.3000	-0.2000	0.4301-j0.1075	0.856+j0.460	0.973/28.2	0.3077+j0.3764	0.4372-j0.1806
	0.94	0.4000+j0.3000	-0.2000	0.4255-j0.1063	0.862+j0.457	0.975/27.9	0.3043+j0.3816	0.4368-j0.1898
	0.95	0.4000+j0.3000	-0.2000	0.4210-j0.1052	0.867+j0.453	0.978/27.6	0.3009+j0.3867	0.4364-j0.1990
	0.96	0.4000+j0.3000	-0.2000	0.4166-j0.1041	0.872+j0.449	0.981/27.2	0.2976+j0.3919	0.4360-j0.2081
	0.97	0.4000+j0.3000	-0.2000	0.4023-j0.1030	0.878+j0.446	0.985/26.9	0.2943+j0.3970	0.4357-j0.2173
	0.98	0.4000+j0.3000	-0.2000	0.4081-j0.1020	0.883+j0.442	0.988/26.6	0.2911+j0.4022	0.4354-j0.2264
	0.99	0.4000+j0.3000	-0.2000	0.4040-j0.1010	0.889+j0.439	0.991/26.3	0.2880+j0.4073	0.4351-j0.2355
1.00	0.4000+j0.3000	-0.2000	0.4000-j0.1000	0.894+j0.436	0.995/26.0	0.2849+j0.4124	0.4348-j0.2446	
954	0.90	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.649+j0.042	0.651/3.7°	-0.0073+j0.4217	0.0132-j0.2743
	0.91	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.657+j0.043	0.658/3.7°	-0.0073+j0.4264	0.0135-j0.2805
	0.92	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.664+j0.043	0.665/3.7°	-0.0075+j0.4310	0.0138-j0.2867
	0.93	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.671+j0.044	0.673/3.7°	-0.0075+j0.4357	0.0141-j0.2929
	0.94	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.678+j0.044	0.680/3.7°	-0.0076+j0.4404	0.0144-j0.2993
	0.95	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.686+j0.045	0.687/3.7°	-0.0077+j0.4451	0.0147-j0.3057
	0.96	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.693+j0.045	0.694/3.7°	-0.0078+j0.4498	0.0150-j0.3121
	0.97	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.700+j0.046	0.701/3.7°	-0.0079+j0.4545	0.0153-j0.3187
	0.98	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.707+j0.046	0.709/3.7°	-0.0080+j0.4592	0.0156-j0.3253
	0.99	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.714+j0.047	0.716/3.7°	-0.0080+j0.4638	0.0160-j0.3320
1.00	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.722+j0.047	0.723/3.7°	-0.0081+j0.4685	0.0163-j0.3387	

(TO BE CONTINUED)

TABLE 10 (CONT'D)

ACSR hCh	$\frac{E}{V.O.}$	$S_R = P_R + jQ_R$	Q_X %	I_R	S_S	I_S	$S_S = P_S + jQ_S$	
954	0.90	0.0000+j0.0000	0.2000	0.0000-j0.2222	0.867+j0.009	0.867/0.6°	0.0031+j0.2612	0.0052-j0.2266
	0.91	0.0000+j0.0000	0.2000	0.0000-j0.2197	0.872+j0.010	0.872/0.6°	0.0029+j0.2677	0.0053-j0.2335
	0.92	0.0000+j0.0000	0.2000	0.0000-j0.2173	0.877+j0.011	0.877/0.7°	0.0028+j0.2741	0.0055-j0.2404
	0.93	0.0000+j0.0000	0.2000	0.0000-j0.2150	0.882+j0.011	0.882/0.7°	0.0026+j0.2804	0.0056-j0.2474
	0.94	0.0000+j0.0000	0.2000	0.0000-j0.2127	0.887+j0.012	0.887/0.8°	0.0024+j0.2868	0.0058-j0.2544
	0.95	0.0000+j0.0000	0.2000	0.0000-j0.2105	0.892+j0.013	0.892/0.8°	0.0022+j0.2931	0.0059-j0.2614
	0.96	0.0000+j0.0000	0.2000	0.0000-j0.2083	0.897+j0.014	0.897/0.9°	0.0020+j0.2993	0.0061-j0.2686
	0.97	0.0000+j0.0000	0.2000	0.0000-j0.2061	0.902+j0.015	0.902/0.9°	0.0018+j0.3056	0.0063-j0.2757
	0.98	0.0000+j0.0000	0.2000	0.0000-j0.2040	0.907+j0.015	0.907/1.0°	0.0016+j0.3118	0.0065-j0.2829
	0.99	0.0000+j0.0000	0.2000	0.0000-j0.2020	0.912+j0.016	0.912/1.0°	0.0015+j0.3180	0.0066-j0.2902
	1.00	0.0000+j0.0000	0.2000	0.0000-j0.2000	0.917+j0.017	0.918/1.1°	0.0013+j0.3241	0.0068-j0.2975
	0.90	0.0000+j0.0000	0.3000	0.0000-j0.3333	0.976-j0.007	0.976/-0.4°	0.0084+j0.1810	0.0069-j0.1768
	0.91	0.0000+j0.0000	0.3000	0.0000-j0.3296	0.980-j0.006	0.980/-0.4°	0.0082+j0.1883	0.0068-j0.1846
	0.92	0.0000+j0.0000	0.3000	0.0000-j0.3260	0.983-j0.005	0.983/-0.3°	0.0079+j0.1956	0.0068-j0.1924
	0.93	0.0000+j0.0000	0.3000	0.0000-j0.3225	0.987-j0.004	0.987/-0.2°	0.0077+j0.2028	0.0067-j0.2003
	0.94	0.0000+j0.0000	0.3000	0.0000-j0.3191	0.991-j0.003	0.991/-0.2°	0.0074+j0.2100	0.0067-j0.2082
	0.95	0.0000+j0.0000	0.3000	0.0000-j0.3157	0.995-j0.002	0.995/-0.1°	0.0072+j0.2171	0.0067-j0.2161
	0.96	0.0000+j0.0000	0.3000	0.0000-j0.3125	0.999-j0.001	0.999/-0.1°	0.0069+j0.2241	0.0067-j0.2240
	0.97	0.0000+j0.0000	0.3000	0.0000-j0.3092	1.003-j0.000	1.003/-0.0°	0.0067+j0.2311	0.0067-j0.2319
	0.98	0.0000+j0.0000	0.3000	0.0000-j0.3061	1.007+j0.000	1.007/0.0°	0.0065+j0.2381	0.0067-j0.2399
	0.99	0.0000+j0.0000	0.3000	0.0000-j0.3030	1.011+j0.001	1.011/0.0°	0.0062+j0.2450	0.0067-j0.2479
	1.00	0.0000+j0.0000	0.3000	0.0000-j0.3000	1.015+j0.002	1.015/0.1°	0.0060+j0.2519	0.0068-j0.2559

(TO BE CONTINUED)

TABLE 10 (CONT'D)

ACBR P.C.H	$\frac{E_R}{V_0}$	$S_R = P_R + jQ_R$	e_X %	I_R	E_S	I_S	$S_S = P_S + jQ_S$	
954	0.90	0.4000+j0.3000	0.0000	0.4444-j0.3333	1.042+j0.428	1.127/22.3	0.3294+j0.2021	0.4300-j0.0697
	0.91	0.4000+j0.3000	0.0000	0.4395-j0.3296	1.045+j0.424	1.128/22.1	0.3256+j0.2092	0.4293-j0.0806
	0.92	0.4000+j0.3000	0.0000	0.4347-j0.3260	1.048+j0.420	1.130/21.8	0.3219+j0.2162	0.4286-j0.0914
	0.93	0.4000+j0.3000	0.0000	0.4301-j0.3225	1.051+j0.417	1.131/21.7	0.3183+j0.2232	0.4279-j0.1020
	0.94	0.4000+j0.3000	0.0000	0.4255-j0.3191	1.055+j0.413	1.133/21.4	0.3147+j0.2302	0.4273-j0.1127
	0.95	0.4000+j0.3000	0.0000	0.4210-j0.3157	1.058+j0.410	1.135/21.2	0.3112+j0.2371	0.4267-j0.1232
	0.96	0.4000+j0.3000	0.0000	0.4166-j0.3125	1.061+j0.406	1.137/21.0	0.3078+j0.2439	0.4261-j0.1337
	0.97	0.4000+j0.3000	0.0000	0.4123-j0.3092	1.065+j0.403	1.139/20.8	0.3043+j0.2507	0.4255-j0.1441
	0.98	0.4000+j0.3000	0.0000	0.4081-j0.3061	1.068+j0.400	1.141/20.6	0.3012+j0.2575	0.4250-j0.1545
	0.99	0.4000+j0.3000	0.0000	0.4040-j0.3030	1.072+j0.397	1.143/20.3	0.2980+j0.2642	0.4245-j0.1649
	1.00	0.4000+j0.3000	0.0000	0.4000-j0.3000	1.075+j0.394	1.145/20.1	0.2949+j0.2709	0.4241-j0.1752
	0.90	0.4000+j0.3000	-0.2000	0.4444-j0.1111	0.825+j0.461	0.945/29.2	0.3188+j0.3625	0.4304-j0.1521
	0.91	0.4000+j0.3000	-0.2000	0.4395-j0.1098	0.830+j0.457	0.948/28.8	0.3151+j0.3679	0.4300-j0.1614
	0.92	0.4000+j0.3000	-0.2000	0.4347-j0.1086	0.835+j0.453	0.950/28.5	0.3116+j0.3732	0.4296-j0.1707
	0.93	0.4000+j0.3000	-0.2000	0.4301-j0.1075	0.841+j0.449	0.953/28.1	0.3080+j0.3785	0.4292-j0.1800
	0.94	0.4000+j0.3000	-0.2000	0.4255-j0.1063	0.846+j0.445	0.956/27.8	0.3046+j0.3838	0.4289-j0.1892
	0.95	0.4000+j0.3000	-0.2000	0.4210-j0.1052	0.852+j0.441	0.959/27.4	0.3012+j0.3891	0.4286-j0.1985
	0.96	0.4000+j0.3000	-0.2000	0.4166-j0.1041	0.857+j0.438	0.963/27.1	0.2979+j0.3943	0.4283-j0.2077
	0.97	0.4000+j0.3000	-0.2000	0.4123-j0.1030	0.863+j0.434	0.966/26.7	0.2947+j0.3996	0.4280-j0.2169
	0.98	0.4000+j0.3000	-0.2000	0.4081-j0.1020	0.868+j0.431	0.969/26.4	0.2915+j0.4048	0.4278-j0.2260
	0.99	0.4000+j0.3000	-0.2000	0.4040-j0.1010	0.874+j0.427	0.973/26.1	0.2884+j0.4101	0.4275-j0.2352
	1.00	0.4000+j0.3000	-0.2000	0.4000-j0.2444	0.879+j0.424	0.976/25.8	0.2854+j0.4153	0.4273-j0.2444

(TO BE CONTINUED)

TABLE 10 (CONT'D)

μ CSR 1.00	$\frac{E_k}{V_0 \cdot C}$	$S_R = P_R + jQ_R$	$\frac{Q}{\%X}$	I_R	E_S		I_S	$S_S = P_S + jQ_S$
1113	0.90	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.649+j0.037	0.650/3.3	-0.0064+j0.4270	0.0116-j0.2777
	0.91	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.657+j0.037	0.658/3.3	-0.0065+j0.4318	0.0118-j0.2839
	0.92	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.664+j0.037	0.665/3.3	-0.0065+j0.4365	0.0121-j0.2902
	0.93	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.671+j0.038	0.672/3.3	-0.0066+j0.4413	0.0124-j0.2965
	0.94	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.678+j0.038	0.679/3.3	-0.0067+j0.4460	0.0126-j0.3029
	0.95	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.685+j0.039	0.687/3.3	-0.0068+j0.4507	0.0129-j0.3094
	0.96	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.693+j0.039	0.694/3.3	-0.0068+j0.4555	0.0132-j0.3160
	0.97	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.700+j0.039	0.701/3.3	-0.0069+j0.4602	0.0135-j0.3226
	0.98	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.707+j0.040	0.708/3.3	-0.0070+j0.4650	0.0137-j0.3293
	0.99	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.714+j0.040	0.716/3.3	-0.0070+j0.4697	0.0141-j0.3360
	1.00	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.722+j0.041	0.723/3.3	-0.0071+j0.4745	0.0143-j0.3429
	0.90	0.0000+j0.0000	0.3000	0.0000-j0.3333	0.972-j0.005	0.972/-0.3	0.0072+j0.1864	0.0059-j0.1812
	0.91	0.0000+j0.0000	0.3000	0.0000-j0.3296	0.975-j0.004	0.975/-0.2	0.0070+j0.1937	0.0059-j0.1891
	0.92	0.0000+j0.0000	0.3000	0.0000-j0.3260	0.979-j0.003	0.979/-0.2	0.0068+j0.2011	0.0058-j0.1970
	0.93	0.0000+j0.0000	0.3000	0.0000-j0.3225	0.983-j0.003	0.983/-0.2	0.0066+j0.2084	0.0058-j0.2049
	0.94	0.0000+j0.0000	0.3000	0.0000-j0.3191	0.987-j0.002	0.987/-0.1	0.0063+j0.2156	0.0058-j0.2128
	0.95	0.0000+j0.0000	0.3000	0.0000-j0.3157	0.991-j0.001	0.991/-0.1	0.0061+j0.2227	0.0058-j0.2208
	0.96	0.0000+j0.0000	0.3000	0.0000-j0.3125	0.995-j0.000	0.995/-0.0	0.0059+j0.2299	0.0058-j0.2288
	0.97	0.0000+j0.0000	0.3000	0.0000-j0.3092	0.999+j0.000	0.999/0.0	0.0057+j0.2369	0.0058-j0.2368
	0.98	0.0000+j0.0000	0.3000	0.0000-j0.3061	1.003+j0.001	1.003/0.1	0.0055+j0.2440	0.0058-j0.2448
	0.99	0.0000+j0.0000	0.3000	0.0000-j0.3030	1.007+j0.001	1.007/0.1	0.0053+j0.2509	0.0058-j0.2529
	1.00	0.0000+j0.0000	0.3000	0.0000-j0.3000	1.012+j0.002	1.012/0.1	0.0051+j0.2579	0.0059-j0.2610

(TO BE CONTINUED)

TABLE 10 (CONT'D)

ACSR F.C.B.	E_R /0.0	$S_R = P_R + jQ_R$	Q_X %	I_R	E_S	I_S	$S_S = P_S + jQ_S$	
1113	0.90	0.0000+j0.0000	0.2000	0.0000-j0.2222	0.864+j0.008	0.864/0.5°	0.0026+j0.2666	0.0046-j0.2305
	0.91	0.0000+j0.0000	0.2000	0.0000-j0.2197	0.869+j0.009	0.869/0.6°	0.0025+j0.2731	0.0047-j0.2374
	0.92	0.0000+j0.0000	0.2000	0.0000-j0.2173	0.874+j0.009	0.874/0.6°	0.0023+j0.2796	0.0048-j0.2444
	0.93	0.0000+j0.0000	0.2000	0.0000-j0.2150	0.879+j0.010	0.879/0.6°	0.0021+j0.2860	0.0049-j0.2515
	0.94	0.0000+j0.0000	0.2000	0.0000-j0.2127	0.884+j0.011	0.884/0.7°	0.0020+j0.2924	0.0051-j0.2586
	0.95	0.0000+j0.0000	0.2000	0.0000-j0.2105	0.889+j0.012	0.889/0.7°	0.0018+j0.2987	0.0052-j0.2657
	0.96	0.0000+j0.0000	0.2000	0.0000-j0.2083	0.894+j0.012	0.894/0.7°	0.0016+j0.3051	0.0054-j0.2729
	0.97	0.0000+j0.0000	0.2000	0.0000-j0.2061	0.899+j0.013	0.899/0.8°	0.0015+j0.3114	0.0055-j0.2801
	0.98	0.0000+j0.0000	0.2000	0.0000-j0.2040	0.904+j0.014	0.904/0.9°	0.0013+j0.3176	0.0057-j0.2874
	0.99	0.0000+j0.0000	0.2000	0.0000-j0.2020	0.910+j0.014	0.910/0.9°	0.0012+j0.3239	0.0059-j0.2947
	1.00	0.0000+j0.0000	0.2000	0.0000-j0.2000	0.915+j0.015	0.915/0.9°	0.0010+j0.3301	0.0060-j0.3021

(TO BE CONTINUED)

TABLE 10 (CONT'D)

ACSR No.	$\frac{E_p}{10.0}$	$S_R = P_R + jQ_R$	$\frac{G}{\%X}$	I_R	E_S		I_S	$S_S = P_S + jQ_S$
1113	0.90	0.4000+j0.3000	0.0000	0.4444-j0.3333	1.029+j0.423	1.112/22.3	0.3281+j0.2046	0.4244-j0.0715
	0.91	0.4000+j0.3000	0.0000	0.4395-j0.3296	1.032+j0.420	1.114/22.1	0.3244+j0.2118	0.4238-j0.0823
	0.92	0.4000+j0.3000	0.0000	0.4347-j0.3260	1.035+j0.416	1.115/21.9	0.3207+j0.2190	0.4232-j0.0931
	0.93	0.4000+j0.3000	0.0000	0.4301-j0.3225	1.038+j0.412	1.117/21.7	0.3171+j0.2261	0.4226-j0.1039
	0.94	0.4000+j0.3000	0.0000	0.4255-j0.3191	1.041+j0.409	1.119/21.4	0.3136+j0.2331	0.4221-j0.1145
	0.95	0.4000+j0.3000	0.0000	0.4210-j0.3157	1.045+j0.405	1.121/21.2	0.3101+j0.2401	0.4216-j0.1251
	0.96	0.4000+j0.3000	0.0000	0.4166-j0.3125	1.048+j0.402	1.123/21.0	0.3068+j0.2470	0.4211-j0.1356
	0.97	0.4000+j0.3000	0.0000	0.4123-j0.3092	1.052+j0.398	1.125/20.7	0.3035+j0.2539	0.4206-j0.1461
	0.98	0.4000+j0.3000	0.0000	0.4081-j0.3061	1.055+j0.395	1.127/20.5	0.3002+j0.2608	0.4202-j0.1565
	0.99	0.4000+j0.3000	0.0000	0.4040-j0.3030	1.059+j0.392	1.129/20.3	0.2970+j0.2676	0.4198-j0.1669
	1.00	0.4000+j0.3000	0.0000	0.4000-j0.3000	1.063+j0.389	1.132/20.0	0.2939+j0.2743	0.4194-j0.1772
	0.90	0.4000+j0.3000	-0.2000	0.4444-j0.1111	0.814+j0.452	0.931/29.0	0.3190+j0.3651	0.4249-j0.1529
	0.91	0.4000+j0.3000	-0.2000	0.4395-j0.1098	0.819+j0.448	0.934/28.6	0.3153+j0.3705	0.4246-j0.1623
	0.92	0.4000+j0.3000	-0.2000	0.4347-j0.1086	0.825+j0.444	0.937/28.3	0.3117+j0.3759	0.4242-j0.1717
	0.93	0.4000+j0.3000	-0.2000	0.4301-j0.1075	0.830+j0.440	0.940/27.9	0.3082+j0.3813	0.4239-j0.1810
	0.94	0.4000+j0.3000	-0.2000	0.4255-j0.1063	0.836+j0.436	0.943/27.5	0.3048+j0.3867	0.4236-j0.1903
	0.95	0.4000+j0.3000	-0.2000	0.4210-j0.1052	0.841+j0.432	0.946/27.2	0.3015+j0.3921	0.4234-j0.1995
	0.96	0.4000+j0.3000	-0.2000	0.4166-j0.1041	0.847+j0.428	0.949/26.8	0.2982+j0.3974	0.4231-j0.2088
	0.97	0.4000+j0.3000	-0.2000	0.4123-j0.1030	0.852+j0.425	0.953/26.5	0.2950+j0.4028	0.4229-j0.2180
	0.98	0.4000+j0.3000	-0.2000	0.4081-j0.1020	0.858+j0.421	0.956/26.1	0.2918+j0.4081	0.4227-j0.2273
	0.99	0.4000+j0.3000	-0.2000	0.4040-j0.1010	0.864+j0.418	0.960/25.8	0.2887+j0.4134	0.4225-j0.2365
	1.00	0.4000+j0.3000	-0.2000	0.4000-j0.1000	0.869+j0.415	0.963/25.5	0.2857+j0.4187	0.4223-j0.2457

(TO BE CONTINUED)

TABLE 10 (CONT'D)

ACSR MCM	$\frac{E_R}{0.0}$	$S_R = P_R + jQ_R$	$\frac{Q}{\%X}$	I_R	E_S	I_S	$S_S = P_S + jQ_S$	
1272	0.90	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.649+j0.032	0.650/2.9	-0.0057+j0.4317	0.0104-j0.2807
	0.91	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.657+j0.033	0.657/2.9	-0.0058+j0.4365	0.0106-j0.2870
	0.92	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.664+j0.033	0.665/2.9	-0.0059+j0.4413	0.0108-j0.2933
	0.93	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.671+j0.033	0.672/2.9	-0.0059+j0.4461	0.0111-j0.2997
	0.94	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.678+j0.034	0.679/2.9	-0.0060+j0.4509	0.0113-j0.3062
	0.95	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.685+j0.034	0.686/2.9	-0.0061+j0.4557	0.0116-j0.3128
	0.96	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.693+j0.035	0.693/2.9	-0.0061+j0.4605	0.0118-j0.3194
	0.97	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.700+j0.035	0.701/2.9	-0.0061+j0.4653	0.0121-j0.3261
	0.98	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.707+j0.035	0.708/2.9	-0.0063+j0.4701	0.0123-j0.3328
	0.99	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.714+j0.036	0.715/2.9	-0.0063+j0.4749	0.0126-j0.3397
	1.00	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.721+j0.036	0.722/2.9	-0.0063+j0.4797	0.0128-j0.3466
	0.90	0.0000+j0.0000	0.2000	0.0000-j0.2222	0.862+j0.007	0.862/0.5	0.0023+j0.2713	0.0041-j0.2339
	0.91	0.0000+j0.0000	0.2000	0.0000-j0.2197	0.867+j0.008	0.867/0.5	0.0021+j0.2778	0.0042-j0.2409
	0.92	0.0000+j0.0000	0.2000	0.0000-j0.2173	0.872+j0.009	0.872/0.6	0.0020+j0.2844	0.0043-j0.2479
	0.93	0.0000+j0.0000	0.2000	0.0000-j0.2150	0.876+j0.009	0.877/0.6	0.0018+j0.2909	0.0044-j0.2551
	0.94	0.0000+j0.0000	0.2000	0.0000-j0.2127	0.882+j0.010	0.882/0.6	0.0017+j0.2973	0.0046-j0.2622
	0.95	0.0000+j0.0000	0.2000	0.0000-j0.2105	0.887+j0.011	0.887/0.7	0.0015+j0.3037	0.0047-j0.2694
	0.96	0.0000+j0.0000	0.2000	0.0000-j0.2083	0.892+j0.011	0.892/0.7	0.0014+j0.3101	0.0048-j0.2767
	0.97	0.0000+j0.0000	0.2000	0.0000-j0.2061	0.897+j0.012	0.897/0.7	0.0012+j0.3164	0.0050-j0.2840
	0.98	0.0000+j0.0000	0.2000	0.0000-j0.2040	0.902+j0.012	0.902/0.7	0.0011+j0.3228	0.0051-j0.2913
	0.99	0.0000+j0.0000	0.2000	0.0000-j0.2020	0.907+j0.013	0.907/0.8	0.0010+j0.3291	0.0053-j0.2987
	1.00	0.0000+j0.0000	0.2000	0.0000-j0.2000	0.913+j0.014	0.913/0.9	0.0008+j0.3353	0.0054-j0.3062

(TO BE CONTINUED)

TABLE 10 (CONT'D)

CSR OCR	$\frac{E_R}{C_{R0}}$	$S_R = F_R + jC_R$	$\frac{C_R}{\%X}$	I_R	E_S	I_S	$S_S = P_S + jQ_S$	
1272	0.90	0.0000+j0.0000	0.3000	0.0000-j0.3333	0.968-j0.004	0.968/-0.3°	0.0063+j0.1911	0.0052-j0.1851
	0.91	0.0000+j0.0000	0.3000	0.0000-j0.3296	0.972-j0.003	0.972/-0.2°	0.0061+j0.1985	0.0052-j0.1930
	0.92	0.0000+j0.0000	0.3000	0.0000-j0.3260	0.975-j0.003	0.975/-0.2°	0.0059+j0.2059	0.0052-j0.2009
	0.93	0.0000+j0.0000	0.3000	0.0000-j0.3225	0.979-j0.002	0.979/-0.2°	0.0057+j0.2132	0.0051-j0.2089
	0.94	0.0000+j0.0000	0.3000	0.0000-j0.3191	0.983-j0.001	0.983/-0.1°	0.0056+j0.2205	0.0051-j0.2169
	0.95	0.0000+j0.0000	0.3000	0.0000-j0.3157	0.987-j0.000	0.987/0.0°	0.0054+j0.2277	0.0051-j0.2249
	0.96	0.0000+j0.0000	0.3000	0.0000-j0.3125	0.991-j0.000	0.991/0.0°	0.0052+j0.2349	0.0051-j0.2330
	0.97	0.0000+j0.0000	0.3000	0.0000-j0.3092	0.995+j0.000	0.995/0.0°	0.0050+j0.2420	0.0051-j0.2410
	0.98	0.0000+j0.0000	0.3000	0.0000-j0.3061	1.000+j0.001	1.000/0.1°	0.0048+j0.2491	0.0052-j0.2491
	0.99	0.0000+j0.0000	0.3000	0.0000-j0.3030	1.004+j0.002	1.004/0.1°	0.0046+j0.2561	0.0052-j0.2572
	1.00	0.0000+j0.0000	0.3000	0.0000-j0.3000	1.008+j0.002	1.008/0.1°	0.0045+j0.2631	0.0052-j0.2654
	0.90	0.4000+j0.3000	0.0000	0.4444-j0.3333	1.018+j0.420	1.101/22.3°	0.3272+j0.2073	0.4204-j0.0736
	0.91	0.4000+j0.3000	0.0000	0.4395-j0.3296	1.021+j0.416	1.103/22.1°	0.3235+j0.2146	0.4198-j0.0845
	0.92	0.4000+j0.3000	0.0000	0.4347-j0.3260	1.024+j0.412	1.104/21.9°	0.3198+j0.2218	0.4193-j0.0953
	0.93	0.4000+j0.3000	0.0000	0.4301-j0.3225	1.028+j0.408	1.106/21.7°	0.3163+j0.2289	0.4188-j0.1061
	0.94	0.4000+j0.3000	0.0000	0.4255-j0.3191	1.031+j0.405	1.108/21.4°	0.3128+j0.2360	0.4183-j0.1168
	0.95	0.4000+j0.3000	0.0000	0.4210-j0.3157	1.035+j0.401	1.110/21.2°	0.3094+j0.2431	0.4179-j0.1274
	0.96	0.4000+j0.3000	0.0000	0.4166-j0.3125	1.038+j0.398	1.112/21.0°	0.3060+j0.2501	0.4175-j0.1379
	0.97	0.4000+j0.3000	0.0000	0.4123-j0.3092	1.042+j0.394	1.114/20.7°	0.3027+j0.2571	0.4171-j0.1484
	0.98	0.4000+j0.3000	0.0000	0.4081-j0.3061	1.046+j0.391	1.116/20.5°	0.2995+j0.2640	0.4167-j0.1589
	0.99	0.4000+j0.3000	0.0000	0.4040-j0.3030	1.049+j0.388	1.119/20.3°	0.2964+j0.2709	0.4163-j0.1693
	1.00	0.4000+j0.3000	0.0000	0.4000-j0.3000	1.053+j0.385	1.121/20.1°	0.2933+j0.2777	0.4160-j0.1797

(TO BE CONTINUED)

TABLE 10 (CONT'D)

Case No.	$\frac{E_R}{/0.0}$	$S_R = P_R + jQ_R$	C_X %	I_R	E_S	I_S	$S_S = P_S + jQ_S$	
1272	0.90	0.4000+j0.3000	-0.2000	0.4444-j0.1111	0.806+j0.445	0.920/28.9	0.3191+j0.3677	0.4209-j0.1543
	0.91	0.4000+j0.3000	-0.2000	0.4395-j0.1098	0.811+j0.440	0.923/28.5	0.3155+j0.3732	0.4206-j0.1637
	0.92	0.4000+j0.3000	-0.2000	0.4347-j0.1086	0.817+j0.436	0.926/28.1	0.3119+j0.3787	0.4203-j0.1731
	0.93	0.4000+j0.3000	-0.2000	0.4301-j0.1075	0.822+j0.432	0.929/27.7	0.3084+j0.3842	0.4201-j0.1825
	0.94	0.4000+j0.3000	-0.2000	0.4255-j0.1063	0.828+j0.429	0.932/27.4	0.3050+j0.3897	0.4198-j0.1918
	0.95	0.4000+j0.3000	-0.2000	0.4210-j0.1052	0.833+j0.425	0.936/27.0	0.3017+j0.3951	0.4196-j0.2011
	0.96	0.4000+j0.3000	-0.2000	0.4166-j0.1041	0.839+j0.421	0.939/26.6	0.2984+j0.4005	0.4194-j0.2104
	0.97	0.4000+j0.3000	-0.2000	0.4123-j0.1030	0.845+j0.417	0.942/26.2	0.2952+j0.4059	0.4192-j0.2197
	0.98	0.4000+j0.3000	-0.2000	0.4081-j0.1020	0.851+j0.414	0.946/25.9	0.2921+j0.4113	0.4190-j0.2290
	0.99	0.4000+j0.3000	-0.2000	0.4040-j0.1010	0.856+j0.410	0.950/25.6	0.2890+j0.4167	0.4189-j0.2383
	1.00	0.4000+j0.3000	-0.2000	0.4000-j0.1000	0.862+j0.407	0.954/25.3	0.2860+j0.4221	0.4187-j0.2475
1431	0.90	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.649+j0.029	0.650/2.6	-0.0052+j0.4357	0.0094-j0.2833
	0.91	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.657+j0.029	0.657/2.6	-0.0053+j0.4406	0.0096-j0.2896
	0.92	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.664+j0.030	0.664/2.6	-0.0053+j0.4454	0.0098-j0.2960
	0.93	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.671+j0.030	0.672/2.6	-0.0054+j0.4503	0.0101-j0.3025
	0.94	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.678+j0.030	0.679/2.6	-0.0054+j0.4551	0.0103-j0.3090
	0.95	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.685+j0.031	0.686/2.6	-0.0055+j0.4600	0.0105-j0.3157
	0.96	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.693+j0.031	0.693/2.6	-0.0056+j0.4648	0.0107-j0.3223
	0.97	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.700+j0.031	0.701/2.6	-0.0056+j0.4696	0.0110-j0.3291
	0.98	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.707+j0.032	0.708/2.6	-0.0057+j0.4745	0.0112-j0.3359
	0.99	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.714+j0.032	0.715/2.6	-0.0057+j0.4793	0.0114-j0.3428
	1.00	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.722+j0.032	0.722/2.6	-0.0058+j0.4842	0.0116-j0.3498

(TO BE CONTINUED)

TABLE 10 (CONT'D)

a_{CSR} HCM	E_R /0.0°	$S_R = P_R + jQ_R$	θ_X %	I_S	E_S	I_S	$S_S = P_S + jQ_S$	
1431	0.90	0.0000+j0.0000	0.2000	0.0000-j0.2222	0.860+j0.007	0.860/0.5°	0.0020+j0.2753	0.0037-j0.2368
	0.91	0.0000+j0.0000	0.2000	0.0000-j0.2197	0.865+j0.007	0.865/0.5°	0.0019+j0.2819	0.0038-j0.2438
	0.92	0.0000+j0.0000	0.2000	0.0000-j0.2173	0.870+j0.008	0.870/0.5°	0.0017+j0.2885	0.0039-j0.2510
	0.93	0.0000+j0.0000	0.2000	0.0000-j0.2150	0.875+j0.008	0.875/0.5°	0.0016+j0.2950	0.0040-j0.2581
	0.94	0.0000+j0.0000	0.2000	0.0000-j0.2127	0.880+j0.009	0.880/0.6°	0.0014+j0.3015	0.0041-j0.2653
	0.95	0.0000+j0.0000	0.2000	0.0000-j0.2105	0.885+j0.010	0.885/0.6°	0.0013+j0.3079	0.0043-j0.2726
	0.96	0.0000+j0.0000	0.2000	0.0000-j0.2083	0.890+j0.010	0.890/0.6°	0.0012+j0.3144	0.0044-j0.2799
	0.97	0.0000+j0.0000	0.2000	0.0000-j0.2061	0.895+j0.011	0.895/0.7°	0.0011+j0.3208	0.0045-j0.2872
	0.98	0.0000+j0.0000	0.2000	0.0000-j0.2040	0.900+j0.011	0.900/0.7°	0.0009+j0.3271	0.0047-j0.2946
	0.99	0.0000+j0.0000	0.2000	0.0000-j0.2020	0.906+j0.012	0.906/0.7°	0.0008+j0.3335	0.0048-j0.3021
	1.00	0.0000+j0.0000	0.2000	0.0000-j0.2000	0.911+j0.012	0.911/0.7°	0.0007+j0.3398	0.0050-j0.3096
	0.90	0.0000+j0.0000	0.3000	0.0000-j0.3333	0.965-j0.003	0.965/-0.2°	0.0056+j0.1951	0.0047-j0.1883
	0.91	0.0000+j0.0000	0.3000	0.0000-j0.3296	0.969-j0.003	0.969/-0.2°	0.0055+j0.2025	0.0047-j0.1963
	0.92	0.0000+j0.0000	0.3000	0.0000-j0.3260	0.972-j0.002	0.972/-0.1°	0.0053+j0.2100	0.0046-j0.2043
	0.93	0.0000+j0.0000	0.3000	0.0000-j0.3225	0.976-j0.001	0.976/-0.1°	0.0051+j0.2174	0.0046-j0.2123
	0.94	0.0000+j0.0000	0.3000	0.0000-j0.3191	0.980-j0.001	0.980/-0.1°	0.0049+j0.2247	0.0046-j0.2204
	0.95	0.0000+j0.0000	0.3000	0.0000-j0.3157	0.984-j0.000	0.984/-0.0°	0.0048+j0.2319	0.0046-j0.2284
	0.96	0.0000+j0.0000	0.3000	0.0000-j0.3125	0.988+j0.000	0.988/0.0°	0.0046+j0.2392	0.0046-j0.2365
	0.97	0.0000+j0.0000	0.3000	0.0000-j0.3092	0.993+j0.000	0.993/0.0°	0.0044+j0.2463	0.0046-j0.2446
	0.98	0.0000+j0.0000	0.3000	0.0000-j0.3061	0.997+j0.001	0.997/0.1°	0.0043+j0.2534	0.0046-j0.2528
	0.99	0.0000+j0.0000	0.3000	0.0000-j0.3030	1.001+j0.002	1.001/0.1°	0.0041+j0.2605	0.0047-j0.2609
	1.00	0.0000+j0.0000	0.3000	0.0000-j0.3000	1.006+j0.002	1.006/0.1°	0.0040+j0.2676	0.0047-j0.2691

(TO BE CONTINUED)

TABLE 10 (CONT'D)

CSR MCK	E_R /0.0R	$S_R = P_R + jQ_R$	Q %X	I_R	E_S	I_S	$S_S = P_S + jQ_S$	
1431	0.90	0.4000+j0.3000	0.0000	0.4444-j0.3333	1.009+j0.416	1.092/22.4	0.3266+j0.2097	0.4172-j0.0756
	0.91	0.4000+j0.3000	0.0000	0.4395-j0.3296	1.013+j0.412	1.094/22.1	0.3228+j0.2170	0.4167-j0.0865
	0.92	0.4000+j0.3000	0.0000	0.4347-j0.3260	1.016+j0.409	1.095/21.9	0.3192+j0.2243	0.4163-j0.0974
	0.93	0.4000+j0.3000	0.0000	0.4301-j0.3225	1.019+j0.405	1.097/21.7	0.3157+j0.2315	0.4158-j0.1082
	0.94	0.4000+j0.3000	0.0000	0.4255-j0.3191	1.023+j0.401	1.099/21.4	0.3122+j0.2387	0.4154-j0.1189
	0.95	0.4000+j0.3000	0.0000	0.4210-j0.3157	1.027+j0.398	1.101/21.2	0.3088+j0.2458	0.4150-j0.1295
	0.96	0.4000+j0.3000	0.0000	0.4166-j0.3125	1.030+j0.394	1.103/20.9	0.3055+j0.2529	0.4147-j0.1401
	0.97	0.4000+j0.3000	0.0000	0.4123-j0.3092	1.034+j0.391	1.105/20.7	0.3022+j0.2599	0.4143-j0.1506
	0.98	0.4000+j0.3000	0.0000	0.4081-j0.3061	1.038+j0.387	1.108/20.4	0.2990+j0.2669	0.4140-j0.1611
	0.99	0.4000+j0.3000	0.0000	0.4040-j0.3030	1.042+j0.384	1.110/20.2	0.2959+j0.2738	0.4137-j0.1716
	1.00	0.4000+j0.3000	0.0000	0.4000-j0.3000	1.046+j0.381	1.113/20.0	0.2928+j0.2807	0.4134-j0.1820
	0.90	0.4000+j0.3000	-0.2000	0.4444-j0.1111	0.799+j0.439	0.912/28.8	0.3192+j0.3701	0.4178-j0.1557
	0.91	0.4000+j0.3000	-0.2000	0.4395-j0.1098	0.805+j0.434	0.915/28.4	0.3156+j0.3757	0.4175-j0.1652
	0.92	0.4000+j0.3000	-0.2000	0.4347-j0.1086	0.810+j0.430	0.918/28.0	0.3121+j0.3812	0.4173-j0.1746
	0.93	0.4000+j0.3000	-0.2000	0.4301-j0.1075	0.816+j0.426	0.921/27.6	0.3086+j0.3868	0.4171-j0.1840
	0.94	0.4000+j0.3000	-0.2000	0.4255-j0.1063	0.822+j0.422	0.924/27.2	0.3052+j0.3923	0.4169-j0.1934
	0.95	0.4000+j0.3000	-0.2000	0.4201-j0.1052	0.827+j0.419	0.927/26.8	0.3019+j0.3978	0.4167-j0.2027
	0.96	0.4000+j0.3000	-0.2000	0.4166-j0.1041	0.833+j0.415	0.931/26.5	0.2986+j0.4033	0.4165-j0.2121
	0.97	0.4000+j0.3000	-0.2000	0.4123-j0.1030	0.839+j0.411	0.934/26.1	0.2954+j0.4088	0.4163-j0.2214
	0.98	0.4000+j0.3000	-0.2000	0.4081-j0.1020	0.845+j0.408	0.938/25.7	0.2923+j0.4142	0.4162-j0.2307
	0.99	0.4000+j0.3000	-0.2000	0.4040-j0.1010	0.850+j0.404	0.942/25.4	0.2892+j0.4197	0.4160-j0.2400
	1.00	0.4000+j0.3000	-0.2000	0.4000-j0.1000	0.856+j0.401	0.946/25.1	0.2862+j0.4251	0.4159-j0.2493

(TO BE CONTINUED)

TABLE 10 (CONT'D)

ACSR MCN	$\frac{E_R}{V}$	$S_R = P_R + jQ_R$	$\frac{Q}{X}$ %	I_R	E_S	I_S	$S_S = P_S + jQ_S$	
1590	0.90	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.649+j0.026	0.650/2.3°	-0.0048+j0.4396	0.0086-j0.2857
	0.91	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.656+j0.027	0.657/2.3°	-0.0048+j0.4445	0.0088-j0.2920
	0.92	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.664+j0.027	0.664/2.3°	-0.0049+j0.4493	0.0090-j0.2985
	0.93	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.671+j0.027	0.671/2.3°	-0.0049+j0.4542	0.0092-j0.3050
	0.94	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.678+j0.028	0.679/2.3°	-0.0050+j0.4591	0.0094-j0.3116
	0.95	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.685+j0.028	0.686/2.3°	-0.0050+j0.4640	0.0096-j0.3183
	0.96	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.692+j0.028	0.693/2.3°	-0.0051+j0.4689	0.0098-j0.3250
	0.97	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.700+j0.028	0.700/2.3°	-0.0052+j0.4738	0.0100-j0.3318
	0.98	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.707+j0.029	0.707/2.3°	-0.0052+j0.4787	0.0103-j0.3387
	0.99	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.714+j0.029	0.715/2.3°	-0.0053+j0.4835	0.0105-j0.3457
	1.00	0.0000+j0.0000	0.0000	0.0000-j0.0000	0.721+j0.029	0.722/2.3°	-0.0053+j0.4884	0.0107-j0.3527
	0.90	0.0000+j0.0000	0.2000	0.0000-j0.2222	0.858+j0.006	0.858/0.4°	0.0018+j0.2792	0.0034-j0.2396
	0.91	0.0000+j0.0000	0.2000	0.0000-j0.2197	0.863+j0.007	0.863/0.5°	0.0016+j0.2858	0.0035-j0.2467
	0.92	0.0000+j0.0000	0.2000	0.0000-j0.2173	0.868+j0.007	0.868/0.5°	0.0015+j0.2924	0.0036-j0.2538
	0.93	0.0000+j0.0000	0.2000	0.0000-j0.2150	0.873+j0.008	0.873/0.5°	0.0014+j0.2990	0.0037-j0.2611
	0.94	0.0000+j0.0000	0.2000	0.0000-j0.2127	0.878+j0.008	0.878/0.5°	0.0013+j0.3055	0.0038-j0.2683
	0.95	0.0000+j0.0000	0.2000	0.0000-j0.2105	0.883+j0.009	0.883/0.5°	0.0011+j0.3120	0.0039-j0.2756
	0.96	0.0000+j0.0000	0.2000	0.0000-j0.2083	0.888+j0.009	0.888/0.6°	0.0010+j0.3185	0.0040-j0.2830
	0.97	0.0000+j0.0000	0.2000	0.0000-j0.2061	0.893+j0.010	0.893/0.6°	0.0009+j0.3249	0.0042-j0.2904
	0.98	0.0000+j0.0000	0.2000	0.0000-j0.2040	0.898+j0.010	0.898/0.6°	0.0008+j0.3314	0.0043-j0.2978
	0.99	0.0000+j0.0000	0.2000	0.0000-j0.2020	0.904+j0.011	0.904/0.7°	0.0007+j0.3377	0.0044-j0.3054
	1.00	0.0000+j0.0000	0.2000	0.0000-j0.2000	0.909+j0.011	0.909/0.7°	0.0006+j0.3441	0.0046-j0.3129

(TO BE CONTINUED)

TABLE 10 (CONT'D)

ACSR MCM	$\frac{E_R}{0.0}$	$S_R = P_R + jQ_R$	$\% X$	I_R	E_S	I_S	$S_S = P_S + jQ_S$
1590	0.90	0.0000+j0.0000	0.3000	0.0000-j0.3333	0.962-j0.003	0.962/-0.2	0.0051+j0.1990
	0.91	0.0000+j0.0000	0.3000	0.0000-j0.3296	0.966-j0.002	0.966/-0.1	0.0049+j0.2065
	0.92	0.0000+j0.0000	0.3000	0.0000-j0.3260	0.970-j0.001	0.970/-0.1	0.0048+j0.2140
	0.93	0.0000+j0.0000	0.3000	0.0000-j0.3225	0.974-j0.001	0.974/-0.1	0.0046+j0.2214
	0.94	0.0000+j0.0000	0.3000	0.0000-j0.3191	0.978-j0.000	0.978/-0.0	0.0044+j0.2288
	0.95	0.0000+j0.0000	0.3000	0.0000-j0.3157	0.982-j0.000	0.982/-0.0	0.0043+j0.2361
	0.96	0.0000+j0.0000	0.3000	0.0000-j0.3125	0.986+j0.000	0.986/0.0	0.0041+j0.2433
	0.97	0.0000+j0.0000	0.3000	0.0000-j0.3092	0.990+j0.001	0.990/0.1	0.0040+j0.2505
	0.98	0.0000+j0.0000	0.3000	0.0000-j0.3061	0.994+j0.001	0.994/0.1	0.0038+j0.2577
	0.99	0.0000+j0.0000	0.3000	0.0000-j0.3030	0.999+j0.002	0.999/0.1	0.0037+j0.2648
	1.00	0.0000+j0.0000	0.3000	0.0000-j0.3000	1.003+j0.002	1.003/0.1	0.0036+j0.2719
	0.90	0.4000+j0.3000	0.0000	0.4444-j0.3333	1.002+j0.413	1.084/22.4	0.3259+j0.2123
	0.91	0.4000+j0.3000	0.0000	0.4395-j0.3296	1.006+j0.410	1.086/22.2	0.3222+j0.2196
	0.92	0.4000+j0.3000	0.0000	0.4347-j0.3260	1.009+j0.406	1.088/21.9	0.3186+j0.2270
	0.93	0.4000+j0.3000	0.0000	0.4301-j0.3225	1.012+j0.402	1.089/21.7	0.3150+j0.2342
	0.94	0.4000+j0.3000	0.0000	0.4255-j0.3191	1.016+j0.398	1.091/21.4	0.3116+j0.2415
	0.95	0.4000+j0.3000	0.0000	0.4210-j0.3157	1.020+j0.395	1.094/21.2	0.3082+j0.2487
	0.96	0.4000+j0.3000	0.0000	0.4166-j0.3125	1.023+j0.391	1.096/20.9	0.3049+j0.2558
	0.97	0.4000+j0.3000	0.0000	0.4123-j0.3092	1.027+j0.388	1.098/20.7	0.3016+j0.2629
	0.98	0.4000+j0.3000	0.0000	0.4081-j0.3061	1.031+j0.384	1.101/20.4	0.2985+j0.2699
	0.99	0.4000+j0.3000	0.0000	0.4040-j0.3030	1.035+j0.381	1.103/20.2	0.2953+j0.2769
	1.00	0.4000+j0.3000	0.0000	0.4000-j0.3000	1.039+j0.378	1.106/20.0	0.2923+j0.2838

(TO BE CONTINUED)

TABLE 10 (CONT'D)

ACSR MCN	$\frac{E_R}{1.0}$	$S_R = P_R + jQ_R$	α_x %	I_R	E_S	I_S	$S_S = P_S + jQ_S$
1590	0.90	0.4000+j0.3000	-0.2000	0.4444-j0.1111	0.794+j0.434	0.904/28.6°	0.3192+j0.3727
	0.91	0.4000+j0.3000	-0.2000	0.4395-j0.1098	0.799+j0.429	0.907/28.2°	0.4153-j0.1573
	0.92	0.4000+j0.3000	-0.2000	0.4347-j0.1086	0.805+j0.425	0.911/27.8°	0.4150-j0.1668
	0.93	0.4000+j0.3000	-0.2000	0.4301-j0.1075	0.811+j0.421	0.914/27.4°	0.4148-j0.1763
	0.94	0.4000+j0.3000	-0.2000	0.4255-j0.1063	0.816+j0.417	0.917/27.1°	0.4146-j0.1875
	0.95	0.4000+j0.3000	-0.2000	0.4210-j0.1052	0.822+j0.414	0.917/26.7°	0.4144-j0.1951
	0.96	0.4000+j0.3000	-0.2000	0.4166-j0.1041	0.828+j0.410	0.920/26.3°	0.4143-j0.2045
	0.97	0.4000+j0.3000	-0.2000	0.4123-j0.1030	0.834+j0.406	0.924/25.9°	0.4141-j0.2138
	0.98	0.4000+j0.3000	-0.2000	0.4081-j0.1020	0.840+j0.403	0.928/25.6°	0.4140-j0.2232
	0.99	0.4000+j0.3000	-0.2000	0.4040-j0.1010	0.845+j0.399	0.931/25.3°	0.4138-j0.2326
	1.00	0.4000+j0.3000	-0.2000	0.4000-j0.1000	0.851+j0.396	0.935/25.0°	0.4137-j0.2419
						0.939/25.0°	0.4136-j0.2513

(RESULTS FROM IBM 1620 DIGITAL COMPUTER)

Base KV = 230 KV

Base MVA = 200 MVA

Full Load = 100 MVA 0.8 p.f. lagging

Distance = 700 KM

All in p.u.

TABLE 11

LOADING CONDITIONS OF 7 CONDUCTOR SIZES FOR LOAD 0 - 150 MVA

ACSR MCM	LOAD MVA	$S_R = P_R + jQ_R$	$\frac{U_X}{\%}$	I_R	E_S	I_S	$S_S = P_S + jQ_S$	
636	0	0.0000+j0.0000	0.3000	0.0000-j0.3000	1.026+j0.001	1.026/0.1°	0.0092+j0.2372	0.0098-j0.2434
FCR E_R =1.0 /C.C	10	0.0400+j0.0300	0.2500	0.0400-j0.2800	1.015+j0.046	1.016/2.6°	0.0367+j0.2544	0.0491-j0.2565
	20	0.0800+j0.0600	0.2000	0.0800-j0.2600	1.003+j0.091	1.008/5.2°	0.0642+j0.2716	0.0893-j0.2668
	30	0.1200+j0.0900	0.1500	0.1200-j0.2400	0.992+j0.136	1.002/7.8°	0.0917+j0.2888	0.1305-j0.2741
	40	0.1600+j0.1200	0.1000	0.1600-j0.2200	0.981+j0.181	0.998/10.4°	0.1192+j0.3060	0.1726-j0.2787
	50	0.2000+j0.1500	0.0500	0.2000-j0.2000	0.970+j0.226	0.996/13.1°	0.1468+j0.3232	0.2156-j0.2803
	60	0.2400+j0.1800	0.0000	0.2400-j0.1800	0.958+j0.271	0.996/15.8°	0.1743+j0.3404	0.2596-j0.2791
	70	0.2800+j0.2100	-0.0500	0.2800-j0.1600	0.947+j0.316	0.999/18.4°	0.2018+j0.3577	0.3045-j0.2750
	80	0.3200+j0.2400	-0.1000	0.3200-j0.1400	0.936+j0.361	1.003/21.1°	0.2293+j0.3749	0.3503-j0.2680
	90	0.3600+j0.2700	-0.1500	0.3600-j0.1200	0.925+j0.406	1.010/23.7°	0.2569+j0.3921	0.3971-j0.2582
	100	0.4000+j0.3000	-0.2000	0.4000-j0.1000	0.913+j0.451	1.019/26.2°	0.2844+j0.4093	0.4448-j0.2455
	110	0.4400+j0.3300	-0.2000	0.4400-j0.1300	0.953+j0.485	1.069/27.0°	0.3154+j0.3904	0.4901-j0.2190
	120	0.4800+j0.3600	-0.2000	0.4800-j0.1600	0.992+j0.519	1.120/27.6°	0.3463+j0.3715	0.5367-j0.1889
	130	0.5200+j0.3900	-0.2000	0.5200-j0.1900	1.031+j0.553	1.170/28.2°	0.3773+j0.3525	0.5844-j0.1551
	140	0.5600+j0.4200	-0.2000	0.5600-j0.2200	1.071+j0.586	1.221/28.7°	0.4083+j0.3336	0.6332-j0.1178
	150	0.6000+j0.4500	-0.2000	0.6000-j0.2500	1.110+j0.620	1.272/29.2°	0.4392+j0.3147	0.6832-j0.0770
795	0	0.0000+j0.0000	0.3000	0.0000-j0.3000	1.020+j0.002	1.020/0.1°	0.0074+j0.2452	0.0081-j0.2503
	10	0.0400+j0.0300	0.2500	0.0400-j0.2800	1.007+j0.045	1.008/2.6°	0.0351+j0.2620	0.0474-j0.2624
	20	0.0800+j0.0600	0.2000	0.0800-j0.2600	0.995+j0.089	0.999/5.1°	0.0629+j0.2787	0.0874-j0.2718

(TO BE CONTINUED)

TABLE 11 (CONT'D)

ACSR MCM	LOAD kVA	$S_R = P_R + jQ_R$	Q_x %	I_R	E_S		I_S	$S_S = P_S + jQ_S$	
795	30	0.1200+j0.0900	0.1500	0.1200-j0.2400	0.982+j0.152	0.991/7.6°	0.0906+j0.2954	0.1282-j0.2783	
FOR E_R =1.0 /0.0°	40	0.1600+j0.1200	0.1000	0.1600-j0.2200	0.970+j0.175	0.985/10.2°	0.1184+j0.3121	0.1697-j0.2820	
	50	0.2000+j0.1500	0.0500	0.2000-j0.2000	0.957+j0.219	0.982/12.6°	0.1461+j0.3288	0.2120-j0.2828	
	60	0.2400+j0.1800	0.0000	0.2400-j0.1800	0.944+j0.262	0.980/15.5°	0.1739+j0.3456	0.2551-j0.2808	
	70	0.2800+j0.2100	-0.0500	0.2800-j0.1600	0.932+j0.306	0.981/18.2°	0.2016+j0.3623	0.2989-j0.2760	
	80	0.3200+j0.2400	-0.1000	0.3200-j0.1400	0.919+j0.349	0.983/20.8°	0.2294+j0.3790	0.3435-j0.2684	
	90	0.3600+j0.2700	-0.1500	0.3600-j0.1200	0.907+j0.392	0.988/23.4°	0.2571+j0.3957	0.3888-j0.2579	
	100	0.4000+j0.3000	-0.2000	0.4000-j0.1000	0.894+j0.436	0.995/26.0°	0.2849+j0.4124	0.4348-j0.2446	
	110	0.4400+j0.3300	-0.2000	0.4400-j0.1300	0.931+j0.470	1.043/26.8°	0.3155+j0.3930	0.4789-j0.2176	
	120	0.4800+j0.3600	-0.2000	0.4800-j0.1600	0.968+j0.504	1.092/27.5°	0.3461+j0.3736	0.5240-j0.1872	
	130	0.5200+j0.3900	-0.2000	0.5200-j0.1900	1.005+j0.539	1.147/28.2°	0.3767+j0.3543	0.5700-j0.1531	
	140	0.5600+j0.4200	-0.2000	0.5600-j0.2200	1.042+j0.573	1.190/28.8°	0.4073+j0.3349	0.6169-j0.1156	
	150	0.6000+j0.4500	-0.2000	0.6000-j0.2500	1.080+j0.607	1.239/29.3°	0.4379+j0.3155	0.6647-j0.0745	
	954	0	0.0000+j0.0000	0.3000	0.0000-j0.3000	1.015+j0.002	1.015/0.1°	0.0060+j0.2519	0.0068-j0.2559
	FOR E_R =1.0 /0.0°	10	0.0400+j0.0300	0.2500	0.0400-j0.2800	1.002+j0.044	1.003/2.5°	0.0340+j0.2682	0.0460-j0.2673
		20	0.0800+j0.0600	0.2000	0.0800-j0.2600	0.988+j0.086	0.992/5.0°	0.0619+j0.2846	0.0859-j0.2760
30		0.1200+j0.0900	0.1500	0.1200-j0.2400	0.975+j0.129	0.983/7.5°	0.0898+j0.3009	0.1264-j0.2818	
40		0.1600+j0.1200	0.1000	0.1600-j0.2200	0.961+j0.171	0.976/10.0°	0.1178+j0.3173	0.1676-j0.2849	
50		0.2000+j0.1500	0.0500	0.2000-j0.2000	0.947+j0.213	0.971/12.6°	0.1457+j0.3336	0.2093-j0.2851	

(TO BE CONTINUED)

TABLE 11 (CONT'D)

ACSR MCM	LOAD MVA	$S_R = P_R + jQ_R$	Q_X %	I_R	E_S	I_S	$S_S = P_S + jQ_S$	
954 FOR E_R =1.0 /0.0	60	0.2400+j0.1800	0.0000	0.2400-j0.1800	0.934+j0.255	0.968/15.3°	0.1736+j0.3499	0.2517-j0.2826
	70	0.2800+j0.2100	-0.0500	0.2800-j0.1600	0.920+j0.297	0.967/17.9°	0.2016+j0.3663	0.2947-j0.2722
	80	0.3200+j0.2400	-0.1000	0.3200-j0.1400	0.907+j0.339	0.968/20.5°	0.2295+j0.3826	0.3383-j0.2691
	90	0.3600+j0.2700	-0.1500	0.3600-j0.1200	0.893+j0.382	0.971/23.1°	0.2574+j0.3990	0.3825-j0.2581
	100	0.4000+j0.3000	-0.2000	0.4000-j0.1000	0.879+j0.424	0.976/25.8°	0.2854+j0.4153	0.4273-j0.2444
	110	0.4400+j0.3300	-0.2000	0.4400-j0.1300	0.915+j0.458	1.023/26.6°	0.3157+j0.3955	0.4705-j0.2171
	120	0.4800+j0.3600	-0.2000	0.4800-j0.1600	0.950+j0.493	1.071/27.4°	0.3460+j0.3758	0.5145-j0.1864
	130	0.5200+j0.3900	-0.2000	0.5200-j0.1900	0.986+j0.528	1.118/28.1°	0.3763+j0.3560	0.5592-j0.1522
	140	0.5600+j0.4200	-0.2000	0.5600-j0.2200	1.021+j0.565	1.166/28.9°	0.4066+j0.3363	0.6047-j0.1145
	150	0.6000+j0.4500	-0.2000	0.6000-j0.2500	1.056+j0.597	1.214/29.5°	0.4369+j0.3165	0.6509-j0.0733
1113	0	0.0000+j0.0000	0.3000	0.0000-j0.3000	1.012+j0.002	1.012/0.1°	0.0051+j0.2579	0.0059-j0.2610
FOR E_R =1.0 /0.0	10	0.0400+j0.0300	0.2500	0.0400-j0.2800	0.997+j0.043	0.998/2.5°	0.0332+j0.2740	0.0451-j0.2719
	20	0.0800+j0.0600	0.2000	0.0800-j0.2600	0.983+j0.085	0.987/4.9°	0.0612+j0.2900	0.0849-j0.2801
	30	0.1200+j0.0900	0.1500	0.1200-j0.2400	0.969+j0.126	0.977/7.4°	0.0893+j0.3061	0.1253-j0.2855
	40	0.1600+j0.1200	0.1000	0.1600-j0.2200	0.955+j0.167	0.969/9.9°	0.1174+j0.3222	0.1661-j0.2881
	50	0.2000+j0.1500	0.0500	0.2000-j0.2000	0.941+j0.208	0.963/12.5°	0.1454+j0.3383	0.2075-j0.2880
	60	0.2400+j0.1800	0.0000	0.2400-j0.1800	0.926+j0.250	0.959/15.1°	0.1735+j0.3544	0.2495-j0.2850
	70	0.2800+j0.2100	-0.0500	0.2800-j0.1600	0.912+j0.291	0.957/17.7°	0.2015+j0.3705	0.2918-j0.2794
	80	0.3200+j0.2400	-0.1000	0.3200-j0.1400	0.898+j0.332	0.957/20.3°	0.2296+j0.3866	0.3348-j0.2709

(TO BE CONTINUED)

TABLE 11 (CONT'D)

ACSR MCM	LOAD MVA	$S_R = P_R + jQ_R$	ϵ_X %	I_R	E_S	I_S	$S_S = P_S + jQ_S$	
1113	90	0.3600+j0.2700	-0.1500	0.3600-j0.1200	0.884+j0.373	0.959/22.8	0.2576+j0.4027	0.3783-j0.2597
FOR	100	0.4000+j0.3000	-0.2000	0.4000-j0.1000	0.869+j0.415	0.963/25.5	0.2857+j0.4187	0.4223-j0.2457
μ_R	110	0.4400+j0.3300	-0.2000	0.4400-j0.1300	0.904+j0.449	1.009/26.4	0.3158+j0.3987	0.4649-j0.2184
=1.0	120	0.4800+j0.3600	-0.2000	0.4800-j0.1600	0.938+j0.484	1.056/27.3	0.3459+j0.3787	0.5081-j0.1876
/0.0	130	0.5200+j0.3900	-0.2000	0.5200-j0.1900	0.972+j0.519	1.102/28.1	0.3760+j0.3587	0.5520-j0.1534
	140	0.5600+j0.4200	-0.2000	0.5600-j0.2200	1.006+j0.554	1.149/28.9	0.4062+j0.3387	0.5966-j0.1157
	150	0.6000+j0.4500	-0.2000	0.6000-j0.2500	1.040+j0.589	1.195/29.5	0.4363+j0.3187	0.6418-j0.0746
1272	0	0.0000+j0.0000	0.3000	0.0000-j0.3000	1.008+j0.002	1.008/0.1	0.0045+j0.2631	0.0052-j0.2654
FOR	10	0.0400+j0.0300	0.2500	0.0400-j0.2800	0.994+j0.043	0.995/2.5	0.0326+j0.2790	0.0445-j0.2760
E_R	20	0.0800+j0.0600	0.2000	0.0800-j0.2600	0.979+j0.083	0.983/4.8	0.0608+j0.2949	0.0842-j0.2838
=1.0	30	0.1200+j0.0900	0.1500	0.1200-j0.2400	0.964+j0.124	0.972/7.3	0.0889+j0.3108	0.1244-j0.2888
/0.0	40	0.1600+j0.1200	0.1000	0.1600-j0.2200	0.950+j0.164	0.964/9.8	0.1171+j0.3267	0.1651-j0.2912
	50	0.2000+j0.1500	0.0500	0.2000-j0.2000	0.935+j0.205	0.957/12.4	0.1452+j0.3426	0.2062-j0.2908
	60	0.2400+j0.1800	0.0000	0.2400-j0.1800	0.921+j0.245	0.953/14.9	0.1734+j0.3585	0.2478-j0.2876
	70	0.2800+j0.2100	-0.0500	0.2800-j0.1600	0.906+j0.286	0.950/17.5	0.2015+j0.3744	0.2898-j0.2817
	80	0.3200+j0.2400	-0.1000	0.3200-j0.1400	0.891+j0.326	0.949/20.1	0.2297+j0.3903	0.3323-j0.2731
	90	0.3600+j0.2700	-0.1500	0.3600-j0.1200	0.877+j0.367	0.950/22.7	0.2578+j0.4062	0.3753-j0.2617
	100	0.4000+j0.3000	-0.2000	0.4000-j0.1000	0.862+j0.407	0.954/25.3	0.2860+j0.4221	0.4187-j0.2475
	110	0.4400+j0.3300	-0.2000	0.4400-j0.1300	0.895+j0.442	0.999/26.3	0.3159+j0.4019	0.4608-j0.2202

(TO BE CONTINUED)

TABLE 11 (CONT'D)

ACSR MCM	LOAD MVA	$S_R = P_R + jQ_R$	ϵ_X %	I_R	E_S	I_S	$S_S = P_S + jQ_S$	
1272	120	0.4800+j0.3600	-0.2000	0.4800-j0.1600	0.928+j0.477	1.044/27.2	0.3459+j0.3817	0.5035-j0.1895
FOR	130	0.5200+j0.3900	-0.2000	0.5200-j0.1900	0.962+j0.512	1.089/28.0	0.3759+j0.3615	0.5468-j0.1553
E_R	140	0.5600+j0.4200	-0.2000	0.5600-j0.2200	0.995+j0.547	1.135/28.4	0.4059+j0.3413	0.5907-j0.1177
=1.0 /0.0	150	0.6000+j0.4500	-0.2000	0.6000-j0.2500	1.028+j0.581	1.181/29.5	0.4358+j0.3211	0.6351-j0.0766
1431	0	0.0000+j0.0000	0.3000	0.0000-j0.3000	1.006+j0.002	1.006/0.1	0.0040+j0.2676	0.0047-j0.2691
FOR	10	0.0400+j0.0300	0.2500	0.0400-j0.2800	0.991+j0.042	0.992/2.4	0.0322+j0.2833	0.0040-j0.2794
E_R	20	0.0800+j0.0600	0.2000	0.0800-j0.2600	0.976+j0.082	0.979/4.8	0.0604+j0.2991	0.0836-j0.2869
=1.0 /0.0	30	0.1200+j0.0900	0.1500	0.1200-j0.2400	0.961+j0.122	0.969/7.2	0.0886+j0.3148	0.1237-j0.2918
	40	0.1600+j0.1200	0.1000	0.1600-j0.2200	0.946+j0.162	0.960/9.7	0.1169+j0.3306	0.1642-j0.2939
	50	0.2000+j0.1500	0.0500	0.2000-j0.2000	0.931+j0.202	0.953/12.2	0.1451+j0.3463	0.2051-j0.2932
	60	0.2400+j0.1800	0.0000	0.2400-j0.1800	0.916+j0.241	0.947/14.7	0.1733+j0.3621	0.2465-j0.2899
	70	0.2800+j0.2100	-0.0500	0.2800-j0.1600	0.901+j0.281	0.944/17.3	0.2015+j0.3778	0.2882-j0.2838
	80	0.3200+j0.2400	-0.1000	0.3200-j0.1400	0.886+j0.321	0.943/19.9	0.2298+j0.3936	0.3304-j0.2751
	90	0.3600+j0.2700	-0.1500	0.3600-j0.1200	0.871+j0.361	0.943/22.5	0.2580+j0.4094	0.3729-j0.2635
	100	0.4000+j0.3000	-0.2000	0.4000-j0.1000	0.856+j0.401	0.946/25.1	0.2862+j0.4251	0.4159-j0.2493
	110	0.4400+j0.3300	-0.2000	0.4400-j0.1300	0.889+j0.436	0.990/26.1	0.3161+j0.4048	0.4577-j0.2220
	120	0.4800+j0.3600	-0.2000	0.4800-j0.1600	0.921+j0.471	1.035/27.1	0.3459+j0.3844	0.5000-j0.1913
	130	0.5200+j0.3900	-0.2000	0.5200-j0.1900	0.954+j0.505	1.079/27.9	0.3758+j0.3641	0.5428-j0.1572
	140	0.5600+j0.4200	-0.2000	0.5600-j0.2200	0.986+j0.540	1.125/28.7	0.4057+j0.3437	0.5861-j0.1196

(TO BE CONTINUED)

TABLE 11 (CONT'D)

ACSR MCM	LOAD MVA	$S_R = P_R + jQ_R$	$\cos \phi$ %	I_R	E_S	I_S	$S_S = P_S + jQ_S$	
1431	150	0.6000+j0.4500	-0.2000	0.6000-j0.2500	1.018+j0.575	1.170/29.5°	0.4355+j0.3234	0.6300-j0.0787
1590	0	0.0000+j0.0000	0.3000	0.0000-j0.3000	1.003+j0.002	1.003/0.1°	0.0036+j0.2719	0.0043-j0.2728
FCR	10	0.0400+j0.0300	0.2500	0.0400-j0.2800	0.988+j0.042	0.989/2.5°	0.0318+j0.2875	0.0436-j0.2828
	20	0.0800+j0.0600	0.2000	0.0800-j0.2600	0.973+j0.081	0.976/4.7°	0.0601+j0.3031	0.0832-j0.2901
B R	30	0.1200+j0.0900	0.1500	0.1200-j0.2400	0.957+j0.120	0.965/7.1°	0.0884+j0.3188	0.1232-j0.2947
	40	0.1600+j0.1200	0.1000	0.1600-j0.2200	0.942+j0.160	0.956/9.6°	0.1166+j0.3344	0.1635-j0.2966
=1.0	50	0.2000+j0.1500	0.0500	0.2000-j0.2000	0.927+j0.199	0.948/12.1°	0.1449+j0.3500	0.2043-j0.2952
	60	0.2400+j0.1800	0.0000	0.2400-j0.1800	0.912+j0.238	0.943/14.6°	0.1732+j0.3657	0.2454-j0.2923
0.0°	70	0.2800+j0.2100	-0.0500	0.2800-j0.1600	0.897+j0.278	0.939/17.2°	0.2015+j0.3813	0.2869-j0.2861
	80	0.3200+j0.2400	-0.1000	0.3200-j0.1400	0.887+j0.317	0.937/19.6°	0.2297+j0.3969	0.3288-j0.2772
	90	0.3600+j0.2700	-0.1500	0.3600-j0.1200	0.866+j0.356	0.937/22.4°	0.2580+j0.4126	0.3710-j0.2656
	100	0.4000+j0.3000	-0.2000	0.4000-j0.1000	0.851+j0.396	0.939/24.9°	0.2863+j0.4282	0.4136-j0.2513
	110	0.4400+j0.3300	-0.2000	0.4400-j0.1300	0.883+j0.431	0.983/26.0°	0.3161+j0.4077	0.4551-j0.2240
	120	0.4800+j0.3600	-0.2000	0.4800-j0.1600	0.915+j0.466	1.027/27.0°	0.3458+j0.3873	0.4971-j0.1933
	130	0.5200+j0.3900	-0.2000	0.5200-j0.1900	0.947+j0.500	1.071/27.8°	0.3756+j0.3668	0.5395-j0.1593
	140	0.5600+j0.4200	-0.2000	0.5600-j0.2200	0.978+j0.535	1.115/28.7°	0.4054+j0.3464	0.5824-j0.1219
	150	0.6000+j0.4500	-0.2000	0.6000-j0.2500	1.010+j0.570	1.160/29.4°	0.4351+j0.3259	0.6258-j0.0811

(RESULTS FROM IBM 1620 DIGITAL COMPUTER)

COMPENSATION AT RECEIVING END MAX = +60 & -40 MVAR

Base KV = 230 KV ; Base MVA = 200 MVA ; DISTANCE = 700 KM ; LOAD = 0 - 150 MVA 0.8 p.f. lagging

All in p.u.

TABLE 12

LOADING CONDITIONS OF TIE LINE BETWEEN BANGKOK - KRABI

LOAD MVA	E_R /G.C.*	$S_R = P_R + jQ_R$	Q_X %	I_R	E_S	I_S	$S_S = P_S + jQ_S$	
0	1.06	0.0000+j0.0000	0.2000	0.0000-j0.1886	0.953+j0.025	0.953/1.5°	0.0005+j0.3534	0.0096-j0.3368
0	1.07	0.0000+j0.0000	0.2000	0.0000-j0.1869	0.958+j0.026	0.959/1.6°	0.0003+j0.3593	0.0099-j0.3444
0	1.08	0.0000+j0.0000	0.2000	0.0000-j0.1851	0.964+j0.027	0.964/1.6°	0.0001+j0.3651	0.0102-j0.3520
0	1.09	0.0000+j0.0000	0.2000	0.0000-j0.1834	0.969+j0.028	0.970/1.7°	0.0000+j0.3710	0.0105-j0.3597
0	1.0	0.0000+j0.0000	0.2500	0.0000-j0.2500	0.970+j0.011	0.970/0.6°	0.0045+j0.2814	0.0076-j0.2731
110	1.0	0.4400+j0.3300	-0.2500	0.4400-j0.0800	0.881+j0.479	1.003/28.5°	0.3127+j0.4292	0.4816-j0.2284
120	1.0	0.4800+j0.3600	-0.3000	0.4800-j0.0600	0.869+j0.523	1.014/31.0°	0.3404+j0.4459	0.5292-j0.2095
130	1.0	0.5200+j0.3900	-0.3000	0.5200-j0.0900	0.906+j0.557	1.064/31.6°	0.3710+j0.4265	0.5741-j0.1797
140	1.0	0.5600+j0.4200	-0.3000	0.5600-j0.1200	0.943+j0.591	1.113/32.1°	0.4016+j0.4071	0.6199-j0.1464
150	1.0	0.6000+j0.4500	-0.3000	0.6000-j0.1500	0.980+j0.626	1.163/32.6°	0.4322+j0.3877	0.6666-j0.1095

* (For Load 10 - 100 MVA is the same as shown in TABLE 11)

Base kV = 230 kV

Base MVA = 200 MVA

Distance = 700 KM

Conductor 795 MCM ACSR

Load at 0.8 p.f. lagging

Maximum Compensation at Receiving End
= +50/-60 MVAR

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