

REFERENCES

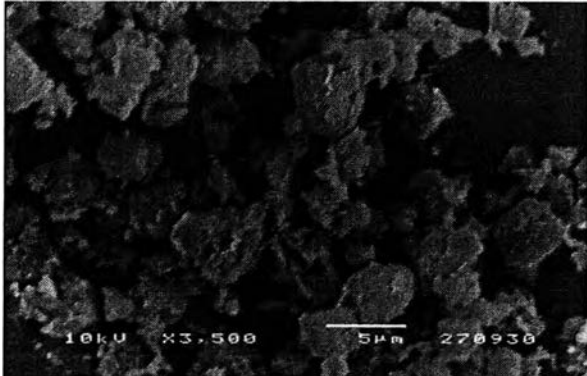
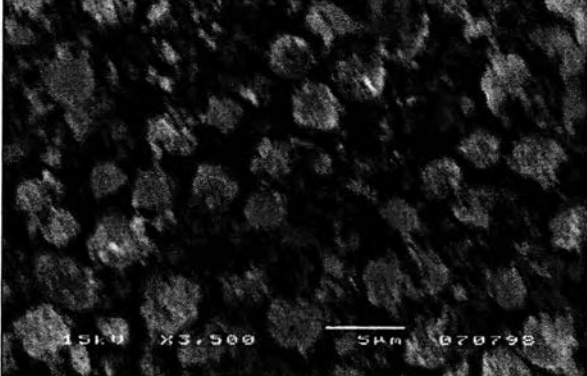
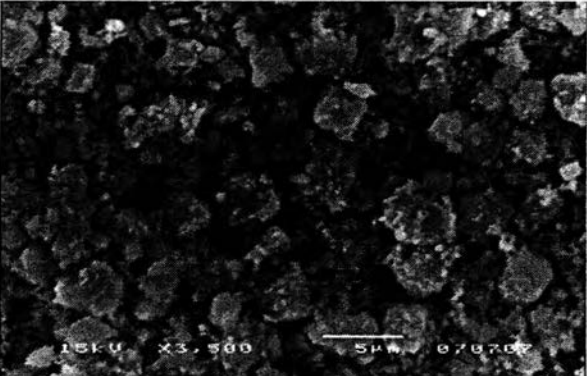
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APPENDICES

Appendix A: SEM Images of Molecular Sieve Zeolites

Table A1 SEM images of 1/8" molecular sieve

Number of batches	SEM images
Fresh	 <p>x 3500</p>
5 batches	 <p>x 3500</p>
15 batches	 <p>x 3500</p>

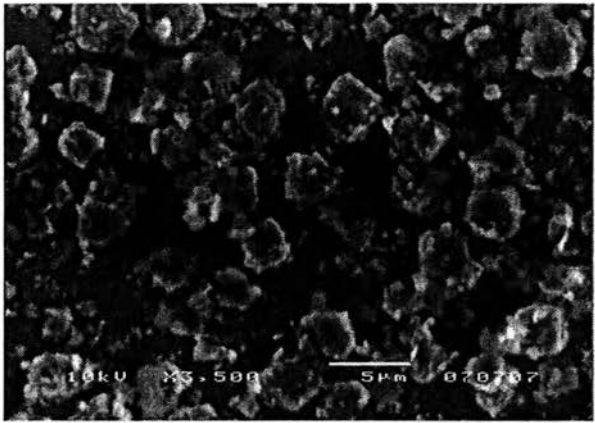
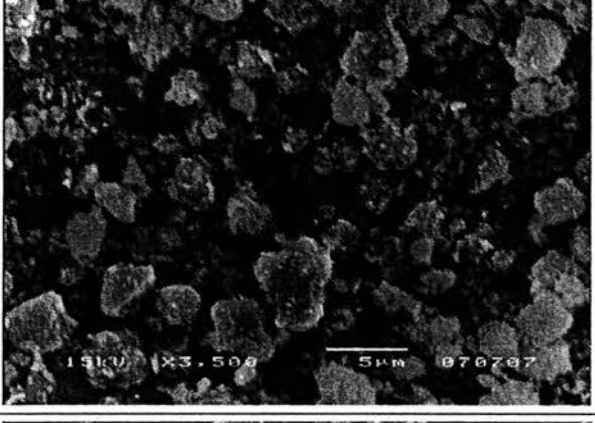
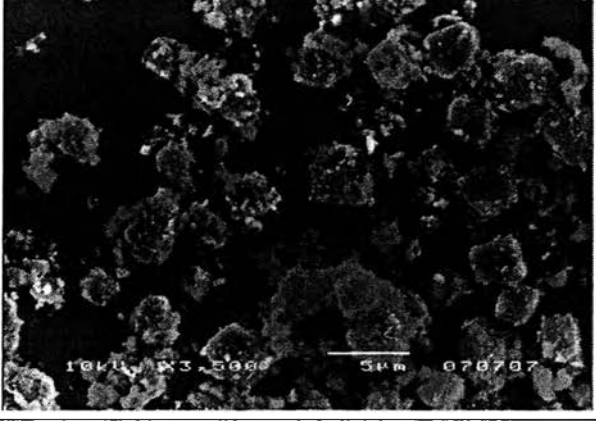
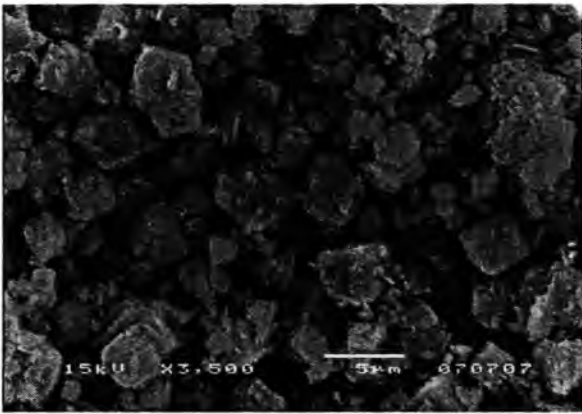
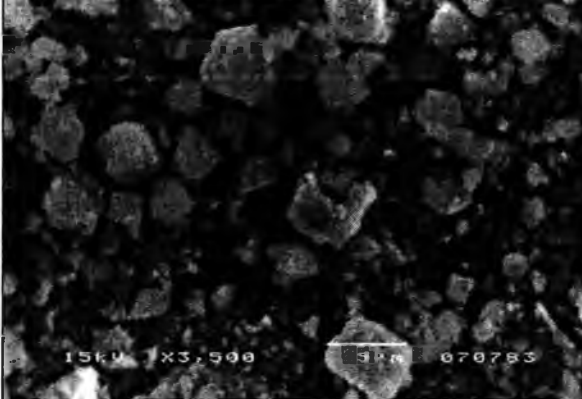
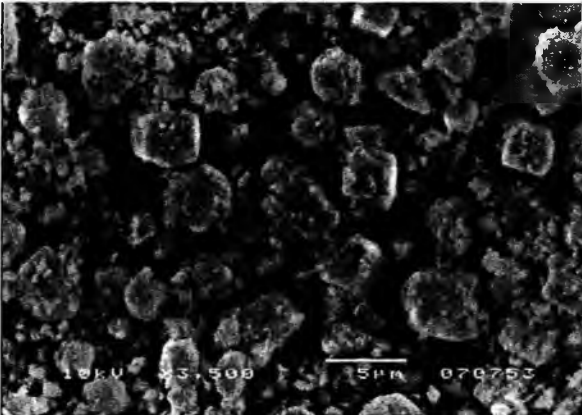
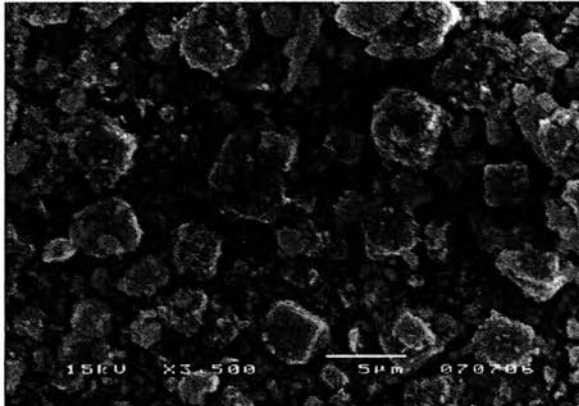
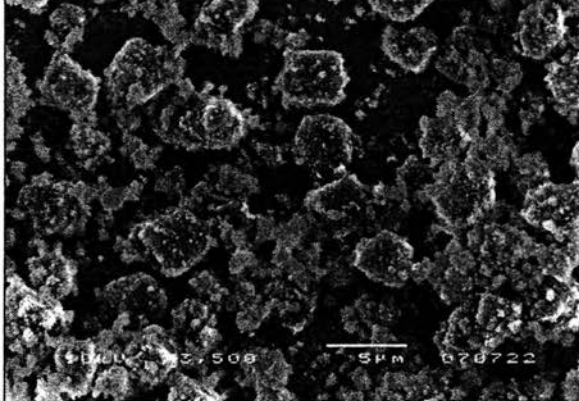
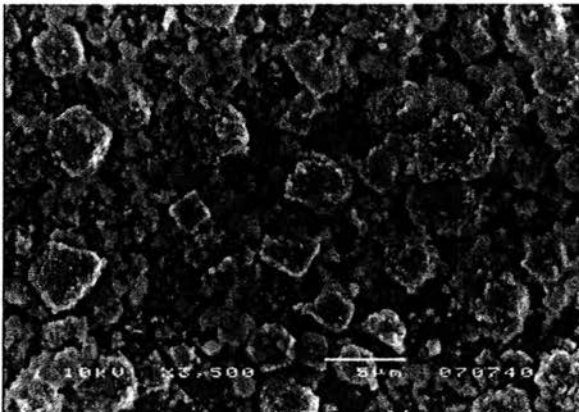
Number of batches	SEM images
25 batches	 <p>10kV X3,500 5µm 070707</p> <p>x 3500</p>
35 batches	 <p>10kV X3,500 5µm 070707</p> <p>x 3500</p>
45 batches	 <p>10kV X3,500 5µm 070707</p> <p>x 3500</p>

Table A2 SEM images of 1/16" molecular sieve

Number of batches	SEM images
Fresh	 <p data-bbox="1139 831 1235 862">x 3500</p>
5 batches	 <p data-bbox="1139 1249 1235 1281">x 3500</p>
15 batches	 <p data-bbox="1139 1680 1235 1711">x 3500</p>

Number of batches	SEM images	
25 batches		x 3500
35 batches		x 3500
45 batches		x 3500

Appendix B: Data of Crystal Size Distribution from SEM

Table B1 Data of crystal size distribution of 1/8" molecular sieve

Number of Batches Crystal size range (micron)	%quantity					
	fresh	5 batches	15 batches	25 batches	35 batches	45 batches
0.00-0.49	0	0	0	0	0	0
0.50-0.99	0	0	0	4	2	4
1.00-1.49	0	1	7	26	19	21
1.50-1.99	0	2	24	21	29	35
2.00-2.49	4	22	44	30	35	40
2.50-2.99	47	40	22	15	15	0
3.00-3.49	45	30	3	4	0	0
3.50-3.99	4	4	0	0	0	0
4.00-4.49	0	1	0	0	0	0
Average crystal size (micron)	2.99	2.805	2.195	1.96	1.955	1.8

Table B2 Data of crystal size distribution of 1/16" molecular sieve

Number of batches Crystal size range (micron)	%quantity					
	fresh	5 batches	15 batches	25 batches	35 batches	45 batches
0.00-0.49	0	0	0	0	0	0
0.50-0.99	0	0	2	4	2	2
1.00-1.49	0	3	15	14	20	32
1.50-1.99	5	7	23	30	32	39
2.00-2.49	9	17	42	34	25	17
2.50-2.99	35	33	18	18	20	10
3.00-3.49	33	26	0	0	1	0
3.50-3.99	16	13	0	0	0	0
4.00-4.49	2	1	0	0	0	0
Average crystal size (micron)	3.000	2.82	2.04	1.985	1.965	1.75

Appendix C: Bed Void Fraction

The bed void fraction of both fresh and deactivated adsorbents can be obtained from Figure A1.

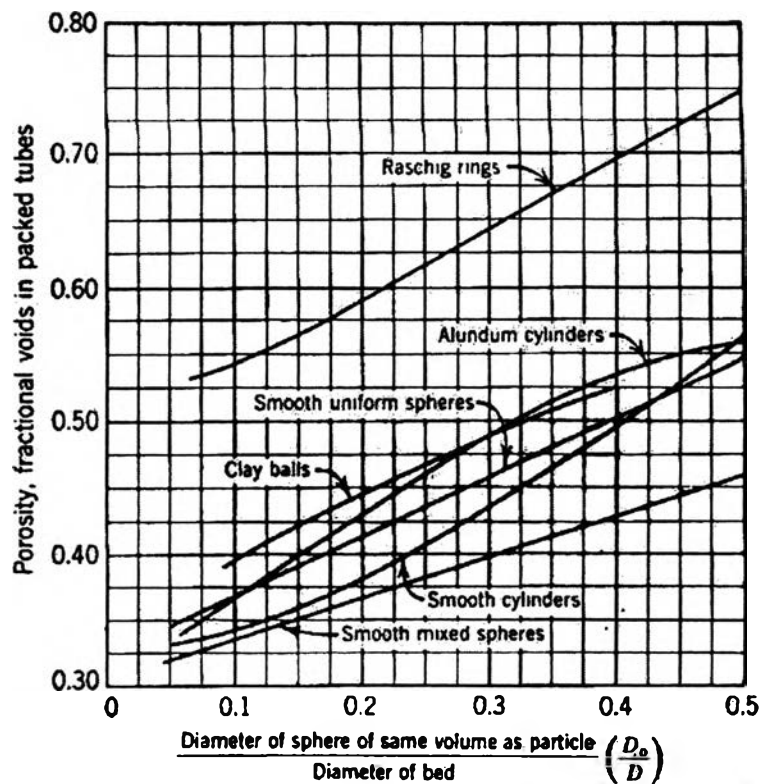


Figure C Porosity as a function of the ration of particle diameter to bed diameter (Leva, 1947).

Appendix D: Mass Transfer Coefficient

The mass transfer coefficient, k , of both fresh and deactivated adsorbents can be calculated by following equation (Murillo *et al.*, 2004).

$$\frac{1}{k} = \frac{R_p}{3k_f} K + \frac{R_p^2}{15\epsilon_p D_e} K \quad (D1)$$

where

k	=	mass transfer coefficient (1/sec)
k_f	=	fluid mass transfer coefficient (m/s)
R_p	=	radius of pellet (m)
K	=	equilibrium constant
ε_p	=	porosity of particle
D_e	=	effective diffusivity (m ² /s)

The effective diffusivity (D_e), which was used in equation D1, is related to Knudsen diffusivity (D_k) and molecular diffusivity (D_m), as follows.

$$\frac{1}{D_e} = \frac{\tau}{\varepsilon_p} \left(\frac{1}{D_m} + \frac{1}{D_k} \right) \quad (D2)$$

Also, the Knudsen diffusivity (D_k) and molecular diffusivity (D_m) can be obtained from equations D3 and D4, respectively.

$$D_k = 9.7 \times 10^3 r_p \left(\frac{T}{M} \right)^{1/2} \quad (D3)$$

$$D_m = \frac{0.0018583 T^{3/2} (1/M_A + 1/M_B)^{1/2}}{P^* \sigma_{AB}^2 \Omega_{AB}} \quad (D4)$$

r_p	=	mean pore radius (cm)
T	=	absolute temperature (K); and
M	=	molecular weight of diffusing species
M_A	=	average molecular weight of bulk species
M_B	=	molecular weight of adsorbate species
P	=	total pressure
σ_{AB}	=	collision diameter from Lennard-Jones potential; and
Ω_{AB}	=	collision integral

Appendix E: Breakthrough Curve Prediction Program

This program can be used for predict the breakthrough curve by input the degree of deactivation because the parameters in mass balance equation and the adsorption isotherm were written as a function of the degree of deactivation.

```

IMPLICIT NONE
DOUBLE PRECISION RHR,Velo,Alu,Bmol,Smol,DA,Db,Ds
DOUBLE PRECISION C0,C,q,dt,KC,Kq,time,Csat,RH
DOUBLE PRECISION v1,v,e_A,e_B,e_C
INTEGER i,j,imax,jmax,n
PARAMETER(imax=90,jmax=5000)
DIMENSION C(imax,jmax),q(imax,jmax),v(imax,jmax)
DIMENSION KC(4,imax,jmax),Kq(4,imax,jmax)

c .....INITIAL CONDITION.....
dt = 0.008
time=0
j=1 !at time = 0
Csat=1.2794E-03
C(1,j)=C0

OPEN(9,file='breakthrough.txt') !open file to receive input values
READ(9,*)Alu,Bmol,Smol,RHR,Velo
RH = RHR
C0 = RH*Csat/100 !inlet concentration (mol/l)
v1= Velo ! Superficial velocity
DA = Alu
Db = Bmol
Ds = Smol
e_A=-0.0000002834*DA**2-0.00001597 *DA+0.3698157 !void fraction as
a function of degree of deactivation
e_B=-0.00000003348 *Db**2-0.000004606*Db+0.3448013
If(Ds.LE.62.38) then
    e_C=-0.0004604*Ds**0.028037+0.329731
Else
    e_C=0.3691822-0.001106*Ds+7.44E-06*Ds**2
END if
v(1,j)=v1/e_A

WRITE(*,*)'Input Values' ! show input values
WRITE(*,*)'%deactivation of alumina=',DA
WRITE(*,*)'%deactivation of 1/8"4A Molsiv=',Db
WRITE(*,*)'%deactivation of 1/16"4A Molsiv=',Ds

```

```

WRITE(*,*)'%Relative Humidity=',RH
WRITE(*,*)'Superficial Velocity=',v1,'(cm/s)'
WRITE(*,*)'-----'
WRITE(*,*)' Running Program '
WRITE(*,*)' Please Wait '
WRITE(*,*)'-----'
OPEN(5,file='velocity.dat')

DO i=2,imax

    C(i,j)=0
    q(i,j)=0

END DO

OPEN(1,file='data1.dat')

DO i=1,imax
    WRITE(1,101)time,i,j,C(i,j),q(i,j),v(i,j)
END DO

    Call RK4(j,C,q,v,imax,jmax,KC,Kq,dt,v1,DA,Db,Ds)

GOTO 20

10 OPEN(2,FILE='DATA2.DAT')

DO i=2,imax

    READ(2,102)time,C(i,1),q(i,1),v(i,1),(KC(n,i,1),n=1,4)
1    ,(Kq(n,i,1),n=1,4)

END DO

20 DO j=2,jmax

    DO i=2,imax

        v(1,j)=v1/e_A

        C(1,j)=C0

        C(i,j)=C(i,j-1)+(dt/6)*(KC(1,i,j-1)+2*KC(2,i,j-1)
1          +2*KC(3,i,j-1)+KC(4,i,j-1))

        q(i,j)=q(i,j-1)+(dt/6)*(Kq(1,i,j-1)+2*Kq(2,i,j-1)
1          +2*Kq(3,i,j-1)+Kq(4,i,j-1))

```

```

        END DO

        Call RK4(j,C,q,v,imax,jmax,KC,Kq,dt,v1,DA,Db,Ds)

    END DO

C .....The Results.....

    DO j=1,jmax

        time=time+dt           !sec

    END DO

    CLOSE(2)
    OPEN(2,file='data2.dat')
    DO i=2,imax

        WRITE(2,102)time,C(i,jmax),q(i,jmax),v(i,jmax)
1    ,(KC(n,i,jmax),n=1,4),(Kq(n,i,jmax),n=1,4)

        WRITE(5,102)time,C(i,jmax),q(i,jmax),v(i,jmax)

        OPEN(3,file='RESULT.dat')
        IF(i.EQ.imax)THEN
            WRITE(3,102)time,C(i,jmax),q(i,jmax),v(i,jmax)

        ELSE
            END IF

    END DO

    CLOSE(2)
c .....Check Running Loop.....

    IF(time.LT.400000) THEN
        GOTO 10
    ELSE
        GOTO 999
    END IF

C .....Format for Input and Output Statements.....
99  FORMAT(E15.9,E15.9,E15.9,E15.9,E15.9)
101  FORMAT(F13.3,I3,I6,2E15.9,8E15.9)
102  FORMAT(F13.3,3E15.9,8E15.9)

```

```

999 STOP
      CLOSE(3)
      END

```

```

c
*****
*****

```

```

SUBROUTINE RK4(j,C,q,v,imax,jmax,KC,Kq,dt,v1,DA,Db,Ds)

```

```

      IMPLICIT NONE
      DOUBLE PRECISION DA,Db,Ds,v1
      DOUBLE PRECISION CC,qq,C,q,dC_dt,dq_dt,dt,KC,Kq,v
      INTEGER i,j,imax,jmax
      DIMENSION C(imax,jmax),q(imax,jmax),dC_dt(imax,jmax)
      DIMENSION dq_dt(imax,jmax),KC(4,imax,jmax),Kq(4,imax,jmax)
      DIMENSION CC(imax,jmax),qq(imax,jmax),v(imax,jmax)

```

```

c      .....Define Parameter.....

```

```

      !v1= Velo      ! Superficial velocity
      !DA = Alu
      !Db  = Bmol
      !Ds  = Smol

```

```

DO i=1,imax

```

```

      CC(i,j)=C(i,j)
      qq(i,j)=q(i,j)

```

```

END DO

```

```

      Call ODEs_EQ(j,imax,jmax,CC,qq,dC_dt,dq_dt,v,v1,DA,Db,Ds)

```

```

DO i=2,imax

```

```

      KC(1,i,j)=dC_dt(i,j)
      Kq(1,i,j)=dq_dt(i,j)
      CC(i,j)=CC(i,j)+(dt/2)*KC(1,i,j)
      qq(i,j)=qq(i,j)+(dt/2)*Kq(1,i,j)

```

```

END DO

```

```

      Call ODEs_EQ(j,imax,jmax,CC,qq,dC_dt,dq_dt,v,v1,DA,Db,Ds)

```

```

DO i=2,imax

```

```
KC(2,i,j)=dC_dt(i,j)
Kq(2,i,j)=dq_dt(i,j)
```

```
CC(i,j)=CC(i,j)+(dt/2)*KC(2,i,j)
qq(i,j)=qq(i,j)+(dt/2)*Kq(2,i,j)
```

```
END DO
```

```
Call ODEs_EQ(j,imax,jmax,CC,qq,dC_dt,dq_dt,v,v1,DA,Db,Ds)
```

```
DO i=2,imax
```

```
KC(3,i,j)=dC_dt(i,j)
Kq(3,i,j)=dq_dt(i,j)
```

```
CC(i,j)=CC(i,j)+(dt)*KC(3,i,j)
qq(i,j)=qq(i,j)+(dt)*Kq(3,i,j)
```

```
END DO
```

```
Call ODEs_EQ(j,imax,jmax,CC,qq;dC_dt,dq_dt,v,v1,DA,Db,Ds)
```

```
DO i=2,imax
```

```
KC(4,i,j)=dC_dt(i,j)
Kq(4,i,j)=dq_dt(i,j)
```

```
END DO
```

```
Return
```

```
End
```

```
c
```

```
*****
*****
```

```
SUBROUTINE ODEs_EQ(j,imax,jmax,c,q,dC_dt,dq_dt,v,v1,DA,Db,Ds)
```

```
IMPLICIT NONE
```

```
DOUBLE PRECISION
```

```
c,q,dC_dt,dz,L,d2C_dz2,DL_A,v1,e_A,e_B,e_C,dq_dt
```

```
DOUBLE PRECISION k1,k2,k3
```

```
DOUBLE PRECISION
```

```
dC_dz,qstar,a1,a2,a3,b1,db_A,db_B,db_C,DL_B,DL_C
```

```
DOUBLE PRECISION Csat,b2,t1,d1,b3,t2,d2,RT,Pa,Psat,P0
```

```
DOUBLE PRECISION v,dv_dz,Ct
```

```
DOUBLE PRECISION rd_A,rd_B,rd_C
```

```

DOUBLE PRECISION DA,Db,Ds
INTEGER i,j,imax,jmax
DIMENSION C(imax,jmax),q(imax,jmax),dC_dt(imax,jmax)
  DIMENSION d2C_dz2(imax,jmax),dC_dz(imax,jmax),qstar(imax,jmax)
DIMENSION dq_dt(imax,jmax),v(imax,jmax),dv_dz(imax,jmax)

```

```

!v1= Velo          ! Superficial velocity
!DA = Alu
!Db   = Bmol
!Ds   = Smol

```

cDefine Parameter.....

```

L =8.8                ! Total bed length
dz = L/ (imax-2)     ! Step size for length
Ct=0.040902639      ! P/RT
RT=24.45388         ! RT
Pa=1.0133E+08       ! atmospheric pressure
P0=1.01325E+06

```

cParameter of Adsorber Zone-A (Activated Alumina).....

```

db_A =0.73743        ! Bulk density of adsorbent
Zone-A
DL_A=0.028249704    ! Axial dispersion through Zone-A
e_A=-0.0000002834*DA**2-0.00001597*DA+0.3698157 !Void fraction
ofZone-A
rd_A=(-0.0053*DA**2-0.1761*DA-195.93)/10

```

cParameter of Adsorber Zone-B (UI-94 1/8").....

```

db_B=0.66529        ! Bulk density of adsorbent Zone-B
DL_B=0.027733066   ! Axial dispersion through Zone-B
e_B=-0.00000003348*Db**2-0.000004606*Db+0.3448013 !Void fraction of
C Zone-B
rd_B=(-0.0026461*Db**2-0.0098614*Db-283.2747)/10

```

cParameter of Adsorber Zone-C (UI-94 1/16").....

```

db_C =0.66529        ! Bulk density of adsorbent
Zone-C

```

```

DL_C=0.027170115          ! Axial dispersion through Zone-C
If(Ds.LE.62.38) then      ! Void fraction of Zone-C
  e_C=-0.0004604*Ds**0.028037+0.329731
  rd_C=(-53.02706*Ds**0.0287672-1167.399)/10

Else
  e_C=0.3691822-0.001106*Ds+7.44E-06*Ds**2
  rd_C=(3637.953-134.6133*Ds+0.9053535*Ds**2)/10
END if

c .....Adsorption Isotherm Constant Parameter.....
k1 =-0.000000001345*DA**2-0.0000003543*DA+0.00006169 ! Effective
overall mass transfer coefficient
k2 =-0.0000000008449*Db**2-0.0000003555*Db+0.00004525
k3 =-0.000000007212*Ds**2-0.0000007993*Ds+0.0001557
j=j
c .....Zone-A (Silica gel).....
Csat=1.2794E-03
a1=1.197121-0.0290791*DA+0.0001773*DA**2 ! For Freundlich-
Isotherm
if(DA.LE.67.9) then
  b1= 2.09E-05*DA**2.510129+0.8289536
Else
  b1=-0.0005461*DA**2+0.0834425*DA-1.48687
END if
DO i=2,4

  qstar(i,j)=a1*((100*C(i,j)/Csat)**b1)

  dq_dt(i,j)=k1*(qstar(i,j)-q(i,j))

  d2C_dz2(i,j)=(1/(dz**2))*(C(i+1,j)-2*C(i,j)+C(i-1,j))

  dC_dz(i,j)=(1/(2*dz))*(C(i+1,j)-C(i-1,j))

  dv_dz(i,j)=-v1*rd_A/(e_A*P0*((2*rd_A*(i-1)*dz/P0)+1)**1.5)

  v(i,j)=dz*(dv_dz(i,j))+v(i-1,j)

  dC_dt(i,j)=DL_A*d2C_dz2(i,j)-v(i,j)*dC_dz(i,j)
1  -((1-e_A)/e_A)*dq_dt(i,j)*db_A/1.8-C(i,j)*dv_dz(i,j)

END DO
c .....Zone-B (Mol Siv 1/8").....

Psat=3169904.00

```



```

a2=-1.269777*Db**0.5740309+17.50962
b2=70.87607*Db**0.3887716+20.02354
t1=-1.038514*Db**0.1542384+2.902765
d1=0.0425293*Db**0.4721149+0.1048701
P0=P0*((2*rd_A*0.3/P0)+1)**0.5
DO i=5,60

```

```

1      qstar(i,j)=(a2*b2*C(i,j)/Csat)/(((1+(b2*C(i,j)/Csat)**t1)**
      (1/t1))*(1-c(i,j)/Csat)**d1)

      dq_dt(i,j)=k2*(qstar(i,j)-q(i,j))

      d2C_dz2(i,j)=(1/(dz**2))*(C(i+1,j)-2*C(i,j)+C(i-1,j))

      dC_dz(i,j)=(1/(2*dz))*(C(i+1,j)-C(i-1,j))

      dv_dz(i,j)=-(v(4,j)*rd_B)/(P0*((2*rd_B*(i-4)*dz/P0)+1)**1.5)

      v(i,j)=dz*(dv_dz(i,j))+v(i-1,j)

      v(5,j)=v(5,j)*e_A/e_B

```

```

      dC_dt(i,j)=DL_B*d2C_dz2(i,j)-v(i,j)*dC_dz(i,j)
1      -((1-e_B)/e_B)*dq_dt(i,j)*db_B/1.8-C(i,j)*dv_dz(i,j)

```

```

END DO

```

```

c .....Zone-C (Mol Siv 1/16").....

```

```

a3=-1.441778*Ds**0.5831572+18.0277
b3=15.51344*Ds**0.7242306+24.18842
t2=-1.740397*Ds**0.1264964+3.877282
d2=0.0262151*Ds**0.7678798+0.1262725
Psat=3169904.00
P0=P0*((2*rd_B*5.6/P0)+1)**0.5
DO i=61,89

```

```

1      qstar(i,j)=(a3*b3*C(i,j)/Csat)/(((1+(b3*C(i,j)/Csat)**t2)**
      (1/t2))*(1-c(i,j)/Csat)**d2)

      dq_dt(i,j)=k3*(qstar(i,j)-q(i,j))

      d2C_dz2(i,j)=(1/(dz**2))*(C(i+1,j)-2*C(i,j)+C(i-1,j))

      dC_dz(i,j)=(1/(2*dz))*(C(i+1,j)-C(i-1,j))

      dv_dz(i,j)=-(v(60,j)*rd_C)/(P0*((2*rd_C*(i-60)*dz/P0)+1)**1.5)

```

```

v(61,j)=v(61,j)*e_B/e_C

v(i,j)=dz*(dv_dz(i,j))+v(i-1,j)

dC_dt(i,j)=DL_C*d2C_dz2(i,j)-v(i,j)*dC_dz(i,j)
1  -((1-e_C)/e_C)*dq_dt(i,j)*db_C/1.8-C(i,j)*dv_dz(i,j)

```

END DO

i=imax

qstar(imax,j)=qstar(imax-1,j)

dq_dt(imax,j)=dq_dt(imax-1,j)

d2C_dz2(imax,j)=0

dC_dz(imax,j)=0

dC_dt(imax,j)=dC_dt(imax-1,j)


dv_dz(imax,j)=dv_dz(imax-1,j)

v(imax,j)=v(imax-1,j)

Return

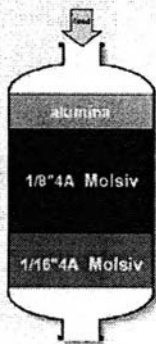
End

Breakthrough Curve Prediction

 Breakthrough Curve Prediction Program
Developed by PPC

Alumina	<input type="text"/>	%
1/8" 4 Amolecular sieve	<input type="text"/>	%
1/16" 4 Amolecular sieve	<input type="text"/>	%
% Relative Humidity	<input type="text"/>	%
Superficial Velocity	<input type="text"/>	cm/s

Start



CURRICULUM VITAE

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