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ศูนย์วิทยทรัพยากร
จุฬาลงกรณ์มหาวิทยาลัย



ภาคผนวก

ศูนย์วิทยทรัพยากร
จุฬาลงกรณ์มหาวิทยาลัย

ภาคผนวก ก

รายละเอียดของไฟไนต์เอลิเมนต์เมตริกซ์ที่ประดิษฐ์ขึ้น

ในบทนี้จะเป็นการแสดงรายละเอียดของไฟไนต์เอลิเมนต์เมตริกซ์ที่ประดิษฐ์ขึ้นในบทที่ 3 โดยจะเริ่มจากค่าฟังก์ชันการประมาณภายในสำหรับความเร็วและความดันซึ่งอยู่ในรูปดังต่อไปนี้

สำหรับความเร็วที่จุดต่อ $N_1 = L_1$ (3.12ก)

$$N_2 = L_2 \quad (3.12ข)$$

$$N_3 = L_3 \quad (3.12ค)$$

สำหรับความเร็วไว้จุดต่อ $N_4 = 4L_2L_3$ (3.12ง)

$$N_5 = 4L_1L_3 \quad (3.12จ)$$

$$N_6 = 4L_1L_2 \quad (3.12ฉ)$$

สำหรับความดัน $H_1 = L_1$ (3.13ก)

$$H_2 = L_2 \quad (3.13ข)$$

$$H_3 = L_3 \quad (3.13ค)$$

เมื่อ L_i คือค่าพิกัดพื้นที่สำหรับจุดต่อ i ซึ่งเป็นฟังก์ชันของพิกัด x และ y ดังนี้

$$L_i(x, y) = \frac{1}{2A}(a_i + b_i x + c_i y) \quad i = 1, 2, 3 \quad (3.10)$$

เมื่อ A = พื้นที่ของเอลิเมนต์ที่พิจารณา

$$= \frac{1}{2}[x_1(y_2 - y_3) + x_2(y_3 - y_1) + x_3(y_1 - y_2)] \quad (3.11)$$

$$a_1 = x_2 y_3 - x_3 y_2 \quad b_1 = y_2 - y_3 \quad c_1 = x_3 - x_2$$

$$a_2 = x_3 y_1 - x_1 y_3 \quad b_2 = y_3 - y_1 \quad c_2 = x_1 - x_3$$

$$a_3 = x_1 y_2 - x_2 y_1 \quad b_3 = y_1 - y_2 \quad c_3 = x_2 - x_1$$

สามารถเขียนค่าอนุพันธ์อันดับหนึ่งของฟังก์ชันการประมาณภายในของความเร็วให้อยู่ในรูปดังนี้

$$\frac{\partial}{\partial x} \{N_i\} = \frac{\partial}{\partial x} \begin{Bmatrix} L_1 \\ L_2 \\ L_3 \\ 4L_2 L_3 \\ 4L_1 L_3 \\ 4L_1 L_2 \end{Bmatrix} = \frac{1}{2A} \begin{Bmatrix} b_1 \\ b_2 \\ b_3 \\ 4(b_2 L_3 + b_3 L_2) \\ 4(b_3 L_1 + b_1 L_3) \\ 4(b_1 L_2 + b_2 L_1) \end{Bmatrix} \quad (ก.1)$$

$$\frac{\partial}{\partial y} \{N_i\} = \frac{\partial}{\partial y} \begin{Bmatrix} L_1 \\ L_2 \\ L_3 \\ 4L_2 L_3 \\ 4L_1 L_3 \\ 4L_1 L_2 \end{Bmatrix} = \frac{1}{2A} \begin{Bmatrix} c_1 \\ c_2 \\ c_3 \\ 4(c_2 L_3 + c_3 L_2) \\ 4(c_3 L_1 + c_1 L_3) \\ 4(c_1 L_2 + c_2 L_1) \end{Bmatrix} \quad (ก.2)$$

และการหาค่าอินทิกรัลของฟังก์ชันที่สามารถคำนวณได้จากสูตร

$$\int_A L_1^\alpha L_2^\beta L_3^\gamma dA = \frac{\alpha! \beta! \gamma!}{(\alpha + \beta + \gamma + 2)!} \cdot 2A \quad (ก.3)$$

สามารถคำนวณหาค่าไฟไนต์เอลิเมนต์เมตริกซ์ที่ประดิษฐ์ขึ้นในบทที่ 3 ได้ดังต่อไปนี้

จาก $K_{\alpha\beta\gamma} = \int_{\Omega} N_\alpha N_\beta N_{\gamma,x} d\Omega \quad (3.23ก)$

จะได้ว่า $K_{\alpha\beta,i} = \int_A N_\alpha N_\beta N_{i,x} dA$
 $= \int_A N_\alpha N_\beta \frac{b_i}{2A} dA$

$$= \frac{b_i}{360} \begin{bmatrix} 30 & 15 & 15 & 12 & 24 & 24 \\ 15 & 30 & 15 & 24 & 12 & 24 \\ 15 & 15 & 30 & 24 & 24 & 12 \\ 12 & 24 & 24 & 32 & 16 & 16 \\ 24 & 12 & 24 & 16 & 32 & 16 \\ 24 & 24 & 12 & 16 & 16 & 32 \end{bmatrix}$$

$$\begin{aligned}
 K_{\alpha\beta_2'} &= \int_A N_\alpha N_\beta N_{2,x} dA \\
 &= \int_A N_\alpha N_\beta \frac{b_2}{2A} dA \\
 &= \frac{b_2}{360} \begin{bmatrix} 30 & 15 & 15 & 12 & 24 & 24 \\ 15 & 30 & 15 & 24 & 12 & 24 \\ 15 & 15 & 30 & 24 & 24 & 12 \\ 12 & 24 & 24 & 32 & 16 & 16 \\ 24 & 12 & 24 & 16 & 32 & 16 \\ 24 & 24 & 12 & 16 & 16 & 32 \end{bmatrix}
 \end{aligned}$$

$$\begin{aligned}
 K_{\alpha\beta_3'} &= \int_A N_\alpha N_\beta N_{3,x} dA \\
 &= \int_A N_\alpha N_\beta \frac{b_3}{2A} dA \\
 &= \frac{b_3}{360} \begin{bmatrix} 30 & 15 & 15 & 12 & 24 & 24 \\ 15 & 30 & 15 & 24 & 12 & 24 \\ 15 & 15 & 30 & 24 & 24 & 12 \\ 12 & 24 & 24 & 32 & 16 & 16 \\ 24 & 12 & 24 & 16 & 32 & 16 \\ 24 & 24 & 12 & 16 & 16 & 32 \end{bmatrix}
 \end{aligned}$$

$$\begin{aligned}
 K_{\alpha\beta_4'} &= \int_A N_\alpha N_\beta N_{4,x} dA \\
 &= \frac{2b}{A} \int_A N_\alpha N_\beta L_3 dA + \frac{2b}{A} \int_A N_\alpha N_\beta L_2 dA \\
 &= \frac{b_2}{630} \begin{bmatrix} 42 & 21 & 42 & 28 & 56 & 28 \\ 21 & 42 & 42 & 56 & 28 & 28 \\ 42 & 42 & 126 & 84 & 84 & 28 \\ 28 & 56 & 84 & 96 & 48 & 32 \\ 56 & 28 & 84 & 48 & 96 & 32 \\ 28 & 28 & 28 & 32 & 32 & 32 \end{bmatrix} + \frac{b_3}{630} \begin{bmatrix} 42 & 42 & 21 & 28 & 28 & 56 \\ 42 & 126 & 42 & 84 & 28 & 84 \\ 21 & 42 & 42 & 56 & 28 & 28 \\ 28 & 84 & 56 & 96 & 32 & 48 \\ 28 & 28 & 28 & 32 & 32 & 32 \\ 56 & 84 & 28 & 48 & 32 & 96 \end{bmatrix}
 \end{aligned}$$

$$\begin{aligned}
 K_{\alpha\beta_5'} &= \int_A N_\alpha N_\beta N_{5,x} dA \\
 &= \frac{2b}{A} \int_A N_\alpha N_\beta L_3 dA + \frac{2b}{A} \int_A N_\alpha N_\beta L_1 dA
 \end{aligned}$$

$$= \frac{b_1}{630} \begin{bmatrix} 42 & 21 & 42 & 28 & 56 & 28 \\ 21 & 42 & 42 & 56 & 28 & 28 \\ 42 & 42 & 126 & 84 & 84 & 28 \\ 28 & 56 & 84 & 96 & 48 & 32 \\ 56 & 28 & 84 & 48 & 96 & 32 \\ 28 & 28 & 28 & 32 & 32 & 32 \end{bmatrix} + \frac{b_3}{630} \begin{bmatrix} 126 & 42 & 42 & 28 & 84 & 84 \\ 42 & 42 & 21 & 28 & 28 & 56 \\ 42 & 21 & 42 & 28 & 56 & 28 \\ 28 & 28 & 28 & 32 & 32 & 32 \\ 84 & 28 & 56 & 32 & 96 & 48 \\ 84 & 56 & 28 & 32 & 48 & 96 \end{bmatrix}$$

$$\begin{aligned} K_{\alpha\beta\epsilon'} &= \int_A N_\alpha N_\beta N_{\epsilon'} dA \\ &= \frac{2b_1}{A} \int_A N_\alpha N_\beta L_2 dA + \frac{2b_2}{A} \int_A N_\alpha N_\beta L_1 dA \\ &= \frac{b_1}{630} \begin{bmatrix} 42 & 42 & 21 & 28 & 28 & 56 \\ 42 & 126 & 42 & 84 & 28 & 84 \\ 21 & 42 & 42 & 56 & 28 & 28 \\ 28 & 84 & 56 & 96 & 32 & 48 \\ 28 & 28 & 28 & 32 & 32 & 32 \\ 56 & 84 & 28 & 48 & 32 & 96 \end{bmatrix} + \frac{b_2}{630} \begin{bmatrix} 126 & 42 & 42 & 28 & 84 & 84 \\ 42 & 42 & 21 & 28 & 28 & 56 \\ 42 & 21 & 42 & 28 & 56 & 28 \\ 28 & 28 & 28 & 32 & 32 & 32 \\ 84 & 28 & 56 & 32 & 96 & 48 \\ 84 & 56 & 28 & 32 & 48 & 96 \end{bmatrix} \end{aligned}$$

จาก $K_{\alpha\beta\gamma'} = \int_\Omega N_\alpha N_\beta N_{\gamma'} d\Omega$ (3.23ข)

จะได้ว่า

$$K_{\alpha\beta 1'} = \int_A N_\alpha N_\beta N_{1,y} dA$$

$$= \int_A N_\alpha N_\beta \frac{c_1}{2A} dA$$

$$= \frac{c_1}{360} \begin{bmatrix} 30 & 15 & 15 & 12 & 24 & 24 \\ 15 & 30 & 15 & 24 & 12 & 24 \\ 15 & 15 & 30 & 24 & 24 & 12 \\ 12 & 24 & 24 & 32 & 16 & 16 \\ 24 & 12 & 24 & 16 & 32 & 16 \\ 24 & 24 & 12 & 16 & 16 & 32 \end{bmatrix}$$

$$K_{\alpha\beta 2'} = \int_A N_\alpha N_\beta N_{2,y} dA$$

$$= \int_A N_\alpha N_\beta \frac{c_2}{2A} dA$$

$$= \frac{c_2}{360} \begin{bmatrix} 30 & 15 & 15 & 12 & 24 & 24 \\ 15 & 30 & 15 & 24 & 12 & 24 \\ 15 & 15 & 30 & 24 & 24 & 12 \\ 12 & 24 & 24 & 32 & 16 & 16 \\ 24 & 12 & 24 & 16 & 32 & 16 \\ 24 & 24 & 12 & 16 & 16 & 32 \end{bmatrix}$$

$$\begin{aligned}
 K_{\alpha\beta\gamma} &= \int_A N_\alpha N_\beta N_{3,y} dA \\
 &= \int_A N_\alpha N_\beta \frac{c_3}{2A} dA \\
 &= \frac{c_3}{360} \begin{bmatrix} 30 & 15 & 15 & 12 & 24 & 24 \\ 15 & 30 & 15 & 24 & 12 & 24 \\ 15 & 15 & 30 & 24 & 24 & 12 \\ 12 & 24 & 24 & 32 & 16 & 16 \\ 24 & 12 & 24 & 16 & 32 & 16 \\ 24 & 24 & 12 & 16 & 16 & 32 \end{bmatrix}
 \end{aligned}$$

$$\begin{aligned}
 K_{\alpha\beta\gamma} &= \int_A N_\alpha N_\beta N_{4,y} dA \\
 &= \frac{2c}{A} \int_A N_\alpha N_\beta L_3 dA + \frac{2c}{A} \int_A N_\alpha N_\beta L_2 dA \\
 &= \frac{c_2}{630} \begin{bmatrix} 42 & 21 & 42 & 28 & 56 & 28 \\ 21 & 42 & 42 & 56 & 28 & 28 \\ 42 & 42 & 126 & 84 & 84 & 28 \\ 28 & 56 & 84 & 96 & 48 & 32 \\ 56 & 28 & 84 & 48 & 96 & 32 \\ 28 & 28 & 28 & 32 & 32 & 32 \end{bmatrix} + \frac{c_3}{630} \begin{bmatrix} 42 & 42 & 21 & 28 & 28 & 56 \\ 42 & 126 & 42 & 84 & 28 & 84 \\ 21 & 42 & 42 & 56 & 28 & 28 \\ 28 & 84 & 56 & 96 & 32 & 48 \\ 28 & 28 & 28 & 32 & 32 & 32 \\ 56 & 84 & 28 & 48 & 32 & 96 \end{bmatrix}
 \end{aligned}$$

$$\begin{aligned}
 K_{\alpha\beta\gamma} &= \int_A N_\alpha N_\beta N_{5,y} dA \\
 &= \frac{2c}{A} \int_A N_\alpha N_\beta L_3 dA + \frac{2c}{A} \int_A N_\alpha N_\beta L_1 dA \\
 &= \frac{c_1}{630} \begin{bmatrix} 42 & 21 & 42 & 28 & 56 & 28 \\ 21 & 42 & 42 & 56 & 28 & 28 \\ 42 & 42 & 126 & 84 & 84 & 28 \\ 28 & 56 & 84 & 96 & 48 & 32 \\ 56 & 28 & 84 & 48 & 96 & 32 \\ 28 & 28 & 28 & 32 & 32 & 32 \end{bmatrix} + \frac{c_3}{630} \begin{bmatrix} 126 & 42 & 42 & 28 & 84 & 84 \\ 42 & 42 & 21 & 28 & 28 & 56 \\ 42 & 21 & 42 & 28 & 56 & 28 \\ 28 & 28 & 28 & 32 & 32 & 32 \\ 84 & 28 & 56 & 32 & 96 & 48 \\ 84 & 56 & 28 & 32 & 48 & 96 \end{bmatrix}
 \end{aligned}$$

$$\begin{aligned}
 K_{\alpha\beta\gamma} &= \int_A N_\alpha N_\beta N_{6,y} dA \\
 &= \frac{2c}{A} \int_A N_\alpha N_\beta L_2 dA + \frac{2c}{A} \int_A N_\alpha N_\beta L_1 dA
 \end{aligned}$$

$$= \frac{c_1}{630} \begin{bmatrix} 42 & 42 & 21 & 28 & 28 & 56 \\ 42 & 126 & 42 & 84 & 28 & 84 \\ 21 & 42 & 42 & 56 & 28 & 28 \\ 28 & 84 & 56 & 96 & 32 & 48 \\ 28 & 28 & 28 & 32 & 32 & 32 \\ 56 & 84 & 28 & 48 & 32 & 96 \end{bmatrix} + \frac{c_2}{630} \begin{bmatrix} 126 & 42 & 42 & 28 & 84 & 84 \\ 42 & 42 & 21 & 28 & 28 & 56 \\ 42 & 21 & 42 & 28 & 56 & 28 \\ 28 & 28 & 28 & 32 & 32 & 32 \\ 84 & 28 & 56 & 32 & 96 & 48 \\ 84 & 56 & 28 & 32 & 48 & 96 \end{bmatrix}$$

จาก $H_{\alpha\mu} = \frac{1}{\rho_\Omega} \int N_{\alpha,x} H_\mu d\Omega$ (3.23ก)

$$= \frac{1}{6\rho} \begin{bmatrix} b_1 & b_1 & b_1 \\ b_2 & b_2 & b_2 \\ b_3 & b_3 & b_3 \\ b_2 + b_3 & b_2 + 2b_3 & 2b_2 + b_3 \\ b_1 + 2b_3 & b_1 + b_3 & 2b_1 + b_3 \\ b_1 + 2b_2 & 2b_1 + b_2 & b_1 + b_2 \end{bmatrix}$$

จาก $H_{\alpha\mu} = \frac{1}{\rho_\Omega} \int N_{\alpha,y} H_\mu d\Omega$ (3.23ข)

$$= \frac{1}{6\rho} \begin{bmatrix} c_1 & c_1 & c_1 \\ c_2 & c_2 & c_2 \\ c_3 & c_3 & c_3 \\ c_2 + c_3 & c_2 + 2c_3 & 2c_2 + c_3 \\ c_1 + 2c_3 & c_1 + c_3 & 2c_1 + c_3 \\ c_1 + 2c_2 & 2c_1 + c_2 & c_1 + c_2 \end{bmatrix}$$

จาก $S_{\alpha\beta^n} = 2v \int_A N_{\alpha,x} N_{\beta,x} dA + v \int_A N_{\alpha,y} N_{\beta,y} dA$ (3.23ค)

จะได้ว่า $= 2vM_{\alpha\beta^n} + vM_{\alpha\beta^n}$

เช่นเดียวกัน $S_{\alpha\beta^v} = v \int_A N_{\alpha,y} N_{\beta,x} dA$ (3.23ด)
 $= vM_{\alpha\beta^v}$

$$S_{\alpha\beta^n} = v \int_A N_{\alpha,x} N_{\beta,y} dA$$
 (3.23ด)
 $= vM_{\alpha\beta^n}$

$$\begin{aligned}
 S_{\alpha\beta\gamma} &= v \int_A N_{\alpha,x} N_{\beta,x} dA + 2v \int_A N_{\alpha,y} N_{\beta,y} dA \\
 &= vM_{\alpha\beta\gamma} + 2vM_{\alpha\beta\gamma}
 \end{aligned}
 \tag{3.23ข}$$

ซึ่งเมื่อทำการอินทิเกรต จะได้ผลลัพธ์ดังนี้

สำหรับ $M_{\alpha\beta\gamma}$ จะได้ว่า

$$\begin{aligned}
 M_{11} &= \frac{b_1 b_1}{4A} & M_{12} &= \frac{b_1 b_2}{4A} & M_{13} &= \frac{b_1 b_3}{4A} \\
 M_{21} &= \frac{b_2 b_1}{4A} & M_{22} &= \frac{b_2 b_2}{4A} & M_{23} &= \frac{b_2 b_3}{4A} \\
 M_{31} &= \frac{b_3 b_1}{4A} & M_{32} &= \frac{b_3 b_2}{4A} & M_{33} &= \frac{b_3 b_3}{4A} \\
 M_{14} &= \frac{b_1}{3A} (b_2 + b_3) & M_{15} &= \frac{b_1}{3A} (b_3 + b_1) & M_{16} &= \frac{b_1}{3A} (b_1 + b_2) \\
 M_{24} &= \frac{b_2}{3A} (b_2 + b_3) & M_{25} &= \frac{b_2}{3A} (b_3 + b_1) & M_{26} &= \frac{b_2}{3A} (b_1 + b_2) \\
 M_{34} &= \frac{b_3}{3A} (b_2 + b_3) & M_{35} &= \frac{b_3}{3A} (b_3 + b_1) & M_{36} &= \frac{b_3}{3A} (b_1 + b_2) \\
 M_{41} &= \frac{b_1}{3A} (b_2 + b_3) & M_{42} &= \frac{b_1}{3A} (b_2 + b_3) & M_{43} &= \frac{b_1}{3A} (b_2 + b_3) \\
 M_{51} &= \frac{b_1}{3A} (b_3 + b_1) & M_{52} &= \frac{b_1}{3A} (b_3 + b_1) & M_{53} &= \frac{b_1}{3A} (b_3 + b_1) \\
 M_{61} &= \frac{b_1}{3A} (b_1 + b_2) & M_{62} &= \frac{b_1}{3A} (b_1 + b_2) & M_{63} &= \frac{b_1}{3A} (b_1 + b_2) \\
 M_{44} &= \frac{2}{3A} (b_2^2 + b_2 b_3 + b_3^2) & M_{54} &= \frac{1}{3A} (2b_1 b_2 + b_1 b_3 + b_2 b_3 + b_3^2) \\
 M_{45} &= \frac{1}{3A} (2b_1 b_2 + b_1 b_3 + b_2 b_3 + b_3^2) & M_{55} &= \frac{2}{3A} (b_1^2 + b_1 b_3 + b_3^2) \\
 M_{46} &= \frac{1}{3A} (2b_1 b_3 + b_1 b_2 + b_3 b_2 + b_2^2) & M_{56} &= \frac{1}{3A} (2b_2 b_3 + b_1 b_2 + b_1 b_3 + b_1^2) \\
 M_{64} &= \frac{1}{3A} (2b_1 b_3 + b_1 b_2 + b_3 b_2 + b_2^2) & & & & \\
 M_{65} &= \frac{1}{3A} (2b_2 b_3 + b_1 b_2 + b_1 b_3 + b_1^2) & & & & \\
 M_{66} &= \frac{2}{3A} (b_1^2 + b_1 b_2 + b_2^2) & & & &
 \end{aligned}$$

สำหรับ $M_{\alpha\beta^n}$ จะได้ว่า

$$\begin{aligned}
 M_{11^n} &= \frac{b_1 c_1}{4A} & M_{12^n} &= \frac{b_1 c_2}{4A} & M_{13^n} &= \frac{b_1 c_3}{4A} \\
 M_{21^n} &= \frac{b_2 c_1}{4A} & M_{22^n} &= \frac{b_2 c_2}{4A} & M_{23^n} &= \frac{b_2 c_3}{4A} \\
 M_{31^n} &= \frac{b_3 c_1}{4A} & M_{32^n} &= \frac{b_3 c_2}{4A} & M_{33^n} &= \frac{b_3 c_3}{4A} \\
 M_{14^n} &= \frac{b_1}{3A}(c_2 + c_3) & M_{15^n} &= \frac{b_1}{3A}(c_3 + c_1) & M_{16^n} &= \frac{b_1}{3A}(c_1 + c_2) \\
 M_{24^n} &= \frac{b_2}{3A}(c_2 + c_3) & M_{25^n} &= \frac{b_2}{3A}(c_3 + c_1) & M_{26^n} &= \frac{b_2}{3A}(c_1 + c_2) \\
 M_{34^n} &= \frac{b_3}{3A}(c_2 + c_3) & M_{35^n} &= \frac{b_3}{3A}(c_3 + c_1) & M_{36^n} &= \frac{b_3}{3A}(c_1 + c_2) \\
 M_{41^n} &= \frac{c_1}{3A}(b_2 + b_3) & M_{42^n} &= \frac{c_2}{3A}(b_2 + b_3) & M_{43^n} &= \frac{c_3}{3A}(b_2 + b_3) \\
 M_{51^n} &= \frac{c_1}{3A}(b_3 + b_1) & M_{52^n} &= \frac{c_2}{3A}(b_3 + b_1) & M_{53^n} &= \frac{c_3}{3A}(b_3 + b_1) \\
 M_{61^n} &= \frac{c_1}{3A}(b_1 + b_2) & M_{62^n} &= \frac{c_2}{3A}(b_1 + b_2) & M_{63^n} &= \frac{c_3}{3A}(b_1 + b_2) \\
 M_{44^n} &= \frac{1}{3A}(2b_2 c_2 + b_2 c_3 + b_3 c_2 + 2b_3 c_3) \\
 M_{45^n} &= \frac{1}{3A}(2b_2 c_1 + b_2 c_3 + b_3 c_1 + b_3 c_3) \\
 M_{46^n} &= \frac{1}{3A}(b_2 c_1 + b_2 c_2 + 2b_3 c_1 + b_3 c_2) \\
 M_{54^n} &= \frac{1}{3A}(2b_1 c_2 + b_1 c_3 + b_3 c_2 + b_3 c_3) \\
 M_{55^n} &= \frac{1}{3A}(2b_1 c_1 + b_1 c_3 + b_3 c_1 + 2b_3 c_3) \\
 M_{56^n} &= \frac{1}{3A}(b_1 c_1 + b_1 c_2 + b_3 c_1 + 2b_3 c_2) \\
 M_{64^n} &= \frac{1}{3A}(b_1 c_2 + 2b_1 c_3 + b_2 c_2 + b_2 c_3) \\
 M_{65^n} &= \frac{1}{3A}(b_1 c_1 + b_1 c_3 + b_2 c_1 + 2b_2 c_3) \\
 M_{66^n} &= \frac{1}{3A}(2b_1 c_1 + b_1 c_2 + b_2 c_1 + 2b_2 c_2)
 \end{aligned}$$

สำหรับ $M_{\alpha\beta^n}$ จะได้ว่า

$$M_{\alpha\beta^n} = M_{\beta\alpha^n}$$

สำหรับ $M_{\alpha\beta}$ จะได้ว่า

$$\begin{aligned}
 M_{11} &= \frac{c_1 c_1}{4A} & M_{12} &= \frac{c_1 c_2}{4A} & M_{13} &= \frac{c_1 c_3}{4A} \\
 M_{21} &= \frac{c_2 c_1}{4A} & M_{22} &= \frac{c_2 c_2}{4A} & M_{23} &= \frac{c_2 c_3}{4A} \\
 M_{31} &= \frac{c_3 c_1}{4A} & M_{32} &= \frac{c_3 c_2}{4A} & M_{33} &= \frac{c_3 c_3}{4A} \\
 M_{14} &= \frac{c_1}{3A} (c_2 + c_3) & M_{15} &= \frac{c_1}{3A} (c_3 + c_1) & M_{16} &= \frac{c_1}{3A} (c_1 + c_2) \\
 M_{24} &= \frac{c_2}{3A} (c_2 + c_3) & M_{25} &= \frac{c_2}{3A} (c_3 + c_1) & M_{26} &= \frac{c_2}{3A} (c_1 + c_2) \\
 M_{34} &= \frac{c_3}{3A} (c_2 + c_3) & M_{35} &= \frac{c_3}{3A} (c_3 + c_1) & M_{36} &= \frac{c_3}{3A} (c_1 + c_2) \\
 M_{41} &= \frac{c_1}{3A} (c_2 + c_3) & M_{42} &= \frac{c_2}{3A} (c_2 + c_3) & M_{43} &= \frac{c_3}{3A} (c_2 + c_3) \\
 M_{51} &= \frac{c_1}{3A} (c_3 + c_1) & M_{52} &= \frac{c_2}{3A} (c_3 + c_1) & M_{53} &= \frac{c_3}{3A} (c_3 + c_1) \\
 M_{61} &= \frac{c_1}{3A} (c_1 + c_2) & M_{62} &= \frac{c_2}{3A} (c_1 + c_2) & M_{63} &= \frac{c_3}{3A} (c_1 + c_2) \\
 M_{44} &= \frac{2}{3A} (c_2^2 + c_2 c_3 + c_3^2) & M_{54} &= \frac{1}{3A} (2c_1 c_2 + c_1 c_3 + c_2 c_3 + c_3^2) \\
 M_{45} &= \frac{1}{3A} (2c_1 c_2 + c_1 c_3 + c_2 c_3 + c_3^2) & M_{55} &= \frac{2}{3A} (c_1^2 + c_1 c_3 + c_3^2) \\
 M_{46} &= \frac{1}{3A} (2c_1 c_3 + c_1 c_2 + c_2 c_3 + c_2^2) & M_{56} &= \frac{1}{3A} (2c_2 c_3 + c_1 c_2 + c_2 c_3 + c_1^2) \\
 M_{64} &= \frac{1}{3A} (2c_1 c_3 + c_1 c_2 + c_2 c_3 + c_2^2) & & & & \\
 M_{65} &= \frac{1}{3A} (2c_2 c_3 + c_1 c_2 + c_2 c_3 + c_1^2) & & & & \\
 M_{66} &= \frac{2}{3A} (c_1^2 + c_1 c_2 + c_2^2) & & & &
 \end{aligned}$$

ศูนย์วิทยุทรัพยากร
จุฬาลงกรณ์มหาวิทยาลัย

ภาคผนวก ข

รายละเอียดของโปรแกรม NVNL

โปรแกรมคอมพิวเตอร์ NVNL ที่ประดิษฐ์ขึ้นดังที่ได้กล่าวไว้ในบทที่ 4 มี

รายละเอียดดังนี้

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C
C   PROGRAM NVNL
C   A FINITE ELEMENT COMPUTER PROGRAM FOR SOLVING NAVIER-STOKES
C   EQUATIONS OF VISCOUS INCOMPRESSIBLE FLOW
C
C   PARAMETER (MXPOIV=2000, MXPOIP=1000, MXELE=2000)
C   PARAMETER (MXNEQ=2*MXPOIV+MXPOIP)
C
C   IMPLICIT REAL*8 (A-H,O-Z)
C   DIMENSION COORD(MXPOIV,2), TEXT(20)
C   DIMENSION UVEL(MXPOIV), VVEL(MXPOIV), PRES(MXPOIV)
C   DIMENSION SYSK(MXNEQ,MXNEQ), SYSR(MXNEQ)
C   DIMENSION SOL(MXNEQ), DSOL(MXNEQ)
C   DIMENSION ACHECK(MXPOIP,MXPOIP,2)
C   CHARACTER*20 INPUT, OUTPUT
C
C   INTEGER INTMAT(MXELE,6)
C   INTEGER IBCU(MXPOIV), IBCV(MXPOIV), IBCP(MXPOIV)
C   INTEGER NUMBER(MXPOIP,MXPOIP)
C
10  WRITE(6,20)
20  FORMAT(/, 'PLEASE ENTER THE INPUT FILE NAME:', /)
    READ(5, '(A)', ERR=10) INPUT
    OPEN(UNIT=7, FILE=INPUT, STATUS='OLD', ERR=10)
30  WRITE(6,40)
40  FORMAT(/, 'PLEASE ENTER FILE NAME FOR VELOCITY & PRESSURE',
*      ' SOLUTIONS:', / )
    READ(5, '(A)', ERR=30) OUTPUT
    OPEN(UNIT=8, FILE=OUTPUT, STATUS='NEW', ERR=30)
C
C   READ TITLE OF COMPUTATION:
C
C   READ(7,*) NLINES
C   DO 50 ILINE=1,NLINES
C     READ(7,1) TEXT
1   FORMAT(20A4)
50  CONTINUE
C
C   READ INPUT DATA
C
C   READ(7,1) TEXT
```

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READ(7,*) NPOIP, NELEM, NITER, TOL
IF(NPOIP.GT.MXPOIP) WRITE(6,60) NPOIP
60 FORMAT(/, ' PLEASE INCREASE THE PARAMETER MXPOIP TO',15)
IF(NPOIP.GT.MXPOIP) STOP
IF(NELEM.GT.MXELE) WRITE(6,70) NELEM
70 FORMAT(/, ' PLEASE INCREASE THE PARAMETER MXELE TO',15)
IF(NELEM.GT.MXELE) STOP

C
C READ FLUID PROPERTIES
C
READ(7,1) TEXT
READ(7,*) DEN, VIS

C
C READ NODAL COORDINATES, BOUNDARY CONDITIONS, THEIR VALUES
C
READ(7,1) TEXT
DO 90 IP=1,NPOIP
READ(7,*) I, IBCU(I), IBCV(I), IBCP(I),
*      (COORD(I,K), K=1,2), UVEL(I), VVEL(I), PRES(I)
IF(I.NE.IP) WRITE(6,80) IP
80 FORMAT(/, ' NODE NO.', 15, ' IN DATA FILE IS MISSING')
IF(I.NE.IP) STOP
90 CONTINUE

C
C READ ELEMENT NODAL CONNECTIONS
C
READ(7,1) TEXT
DO 110 IE=1,NELEM
READ(7,*) I, (INTMAT(I,J), J=1,3)
IF(I.NE.IE) WRITE(6,120) IE
120 FORMAT(/, ' ELEMENT NO.', 15, ' IN DATA FILE IS MISSING')
IF(I.NE.IE) STOP
110 CONTINUE

C
C CREATE NODELESS VARIABLES ON EACH ELEMENT
C
NPOIV = NPOIP
DO 130 I=1,NPOIP
DO 130 J=1,NPOIP
DO 130 K=1,2
ACHECK(I,J,K) = 0.
130 CONTINUE

DO 200 IE=NELEM,1,-1
II = INTMAT(IE,1)
JJ = INTMAT(IE,2)
KK = INTMAT(IE,3)
ACHECK(JJ,KK,2) = ACHECK(JJ,KK,2) + 1.
ACHECK(KK,JJ,2) = ACHECK(KK,JJ,2) + 1.
IF(ACHECK(JJ,KK,1).EQ.1) GO TO 140
ACHECK(JJ,KK,1) = 1.

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ACHECK(KK,JJ,1) = 1.
NPOIV = NPOIV + 1
INTMAT(IE,4) = NPOIV
NUMBER(JJ,KK) = NPOIV
NUMBER(KK,JJ) = NPOIV
COORD(NPOIV,1) = (COORD(JJ,1)+COORD(KK,1))/2.
COORD(NPOIV,2) = (COORD(JJ,2)+COORD(KK,2))/2.
IF(IBC(U).EQ.1.AND.IBC(V).EQ.1) IBC(NPOIV) = 1.
IF(IBC(W).EQ.1.AND.IBC(X).EQ.1) IBC(NPOIV) = 1.
GO TO 150
140 CONTINUE
INTMAT(IE,4) = NUMBER(JJ,KK)
150 CONTINUE
ACHECK(II,KK,2) = ACHECK(II,KK,2) + 1.
ACHECK(KK,II,2) = ACHECK(KK,II,2) + 1.
IF(ACHECK(II,KK,1).EQ.1.) GO TO 160
ACHECK(II,KK,1) = 1.
ACHECK(KK,II,1) = 1.
NPOIV = NPOIV + 1
INTMAT(IE,5) = NPOIV
NUMBER(II,KK) = NPOIV
NUMBER(KK,II) = NPOIV
COORD(NPOIV,1) = (COORD(II,1)+COORD(KK,1))/2.
COORD(NPOIV,2) = (COORD(II,2)+COORD(KK,2))/2.
IF(IBC(U).EQ.1.AND.IBC(V).EQ.1) IBC(NPOIV) = 1.
IF(IBC(W).EQ.1.AND.IBC(X).EQ.1) IBC(NPOIV) = 1.
GO TO 170
160 CONTINUE
INTMAT(IE,5) = NUMBER(II,KK)
170 CONTINUE
ACHECK(II,JJ,2) = ACHECK(II,JJ,2) + 1.
ACHECK(JJ,II,2) = ACHECK(JJ,II,2) + 1.
IF(ACHECK(II,JJ,1).EQ.1.) GO TO 180
ACHECK(II,JJ,1) = 1.
ACHECK(JJ,II,1) = 1.
NPOIV = NPOIV + 1
INTMAT(IE,6) = NPOIV
NUMBER(II,JJ) = NPOIV
NUMBER(JJ,II) = NPOIV
COORD(NPOIV,1) = (COORD(II,1)+COORD(JJ,1))/2.
COORD(NPOIV,2) = (COORD(II,2)+COORD(JJ,2))/2.
IF(IBC(U).EQ.1.AND.IBC(V).EQ.1) IBC(NPOIV) = 1.
IF(IBC(W).EQ.1.AND.IBC(X).EQ.1) IBC(NPOIV) = 1.
GO TO 190
180 CONTINUE
INTMAT(IE,6) = NUMBER(II,JJ)
190 CONTINUE
200 CONTINUE
DO 210 I=1,NPOIP
DO 210 J=1,NPOIP

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IF(ACHECK(I,J,2).LT.2.) GO TO 210
NUM = NUMBER(I,J)
IBCU(NUM) = 0.
IBCV(NUM) = 0.
210 CONTINUE
C
IF(NPOIV.GT.MXPOIV) WRITE(6,220) NPOIV
220 FORMAT(/, ' PLEASE INCREASE THE PARAMETER MXPOIV TO',I5)
IF(NPOIV.GT.MXPOIV) STOP
C
WRITE(6,230) NPOIV, NPOIP, NELEM, NITER, TOL
230 FORMAT(/, ' *** THE FINITE ELEMENT MODEL CONSISTS OF:', /,
*      '   NUMBER OF VELOCITY      =', I6, /,
*      '   NUMBER OF PRESSURE      =', I6, /,
*      '   NUMBER OF ELEMENTS      =', I6, /,
*      '   WITH NUMBER OF ITERATIONS REQUIRED =', I6, /,
*      '   OR SPECIFIED STOPPING TOLERANCE =', F6.2 )
C
DO 240 I=1,NPOIV
SOL(I) = UVEL(I)
SOL(I+NPOIV) = VVEL(I)
240 CONTINUE
DO 250 I=1,NPOIP
SOL(I+NPOIV+NPOIV) = PRES(I)
250 CONTINUE
C
NEQ = 2*NPOIV + NPOIP
C
C ENTER ITERATION LOOP
C
DO 380 ITER=1,NITER
C
C RESET THE SYSTEM EQUATIONS
C
DO 260 I=1,NEQ
SYSR(I) = 0.
260 CONTINUE
DO 270 I=1,NEQ
DO 270 J=1,NEQ
SYSK(I,J) = 0.
270 CONTINUE
C
WRITE(6,280) ITER
280 FORMAT(/, 3X, ' * PERFORMING COMPUTATION AT ITERATION NUMBER',
*      I16, ':')
C
C ESTABLISH ELEMENT MATRICES AND ASSEMBLE ELEMENT EQUATIONS
C
WRITE(6,290)
290 FORMAT(/, ' *** ESTABLISHING ELEMENT MATRICES AND',

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*      ' ASSEMBLING ELEMENT EQUATIONS **** ' )
CALL TRI(NPOIV, NELEM, DEN, VIS, COORD,
*      INTMAT, SYSK, SYSR, SOL, MXPOIV,
*      MXELE, MXNEQ      )
C
C  APPLY BOUNDARY CONDITIONS OF NODAL VELOCITIES AND PRESSURE
C
  WRITE(6,300)
300 FORMAT(/, '*** APPLYING BOUNDARY CONDITIONS OF NODAL',
*      ' INCREMENTS **** ' )
  CALL APPLYBC(NPOIV, NEQ, IBCU, IBCV, IBCP,
*      SYSK, SYSR, MXPOIV, MXNEQ  )
C
C  SOLVE A SET OF SIMULTANEOUS SYSTEM EQUATIONS FOR SOLUTIONS
C
  WRITE(6,310)
310 FORMAT(/, '*** SOLVING A SET OF SIMULTANEOUS EQS. FOR',
*      ' NODAL INCREMENTS **** ' )
  WRITE(6,320) NEQ
320 FORMAT(5X,( 'TOTAL OF', I5,' EQUATIONS TO BE SOLVED '))
  CALL GAUSS(NEQ, SYSK, SYSR, DSOL, MXNEQ)
C
C  CHECK FOR CONVERGENCE
C
  UP = 0.
  DOWN = 0.
  DO 330 I=1,NEQ
  ERROR = DSOL(I)
  UP = UP + ABS(ERROR)
  VALUE = SOL(I)
  DOWN = DOWN + ABS(VALUE)
330 CONTINUE
  RATIO = UP*100./DOWN
  WRITE(6,340) RATIO
340 FORMAT(6X, 'CURRENT SOLUTION HAS GLOBAL ERROR OF',
*      F8.2, '%')
  IF(RATIO.GT.TOL) GO TO 360
C
C  SOLUTION CONVERGED WITHIN THE SPECIFIED TOLERANCE
C
  WRITE(6,350)
350 FORMAT(/, 3X, '*** SOLUTION CONVERGED WITHIN SPECIFIED',
*      ' TOLERANCE ****, //)
  GO TO 400
360 CONTINUE
C
C  UPDATE NODAL SOLUTIONS
C
  DO 370 I=1,NEQ
  SOL(I) = SOL(I) + DSOL(I)

```

```

370 CONTINUE
380 CONTINUE
C
C SOLUTION NOT CONVERGED WITHIN THE SPECIFIED TOLERANCE
C
WRITE(6,390)
390 FORMAT(/, 3X, ' ??? SOLUTION NOT CONVERGED WITHIN'
* ' SPECIFIED TOLERANCE ???', //)
C
400 CONTINUE
C
C PRINT OUT SOLUTIONS OF NODAL VELOCITIES AND PRESSURES
C
WRITE(8,410)
410 FORMAT(2X, 'NODE', 6X, 'U-VELOCITY', 6X, 'V-VELOCITY',
* 8X, 'PRESSURE' )
C
C ROUND-OFF SOLUTION VALUES FOR NEAT OUTPUT
C
ROFF = 1.E-6
DO 420 IEQ=1,NEQ
VALUE = SOL(IEQ)
IF(ABS(VALUE).LT.ROFF) SOL(IEQ) = 0.
420 CONTINUE
C
DO 440 IP=1,NPOIP
IEQU = IP
IEQV = NPOIV + IP
IEQP = 2*NPOIV + IP
WRITE(8,430) IP, SOL(IEQU), SOL(IEQV), SOL(IEQP)
430 FORMAT(I6, 3E16.7)
440 CONTINUE
C
STOP
END
C
C-----
C
SUBROUTINE APPLYBC(NPOIV, NEQ, IBCU, IBCV, IBCP,
* SYSK, SYSR, MXPOIV, MXNEQ )
C
C APPLY BOUNDARY CONDITIONS FOR NODAL VELOCITIES AND PRESSURES
C WITH CONDITION CODES OF
C 0 = FREE TO CHANGE (TO BE COMPUTED)
C 1 = FIXED AS SPECIFIED
C
IMPLICIT REAL*8 (A-H,O-Z)
DIMENSION SYSK(MXNEQ,MXNEQ), SYSR(MXNEQ)
C
INTEGER IBCU(MXPOIV), IBCV(MXPOIV), IBCP(MXPOIV)

```

```

C
C   APPLY BOUNDARY CONDITIONS FOR U-VELOCITIES
C
    IEQ1 = 1
    IEQ2 = NPOIV
    DO 100 IEQ=IEQ1,IEQ2
    IEQU = IEQ
    IF(BCU(IEQU),EQ.0) GO TO 100
C
    DO 110 IR=1,NEQ
    IF(IR,EQ,IEQ) GO TO 110
    SYSK(IR,IEQ) = 0.
110 CONTINUE
C
    DO 120 IC=1,NEQ
    SYSK(IEQ,IC) = 0.
120 CONTINUE
    SYSK(IEQ,IEQ) = 1.
    SYSR(IEQ) = 0.
C
100 CONTINUE
C
C   APPLY BOUNDARY CONDITIONS FOR V-VELOCITIES
C
    IEQ1 = NPOIV + 1
    IEQ2 = 2*NPOIV
    DO 200 IEQ=IEQ1,IEQ2
    IEQV = IEQ - NPOIV
    IF(BCV(IEQV),EQ.0) GO TO 200
C
    DO 210 IR=1,NEQ
    IF(IR,EQ,IEQ) GO TO 210
    SYSK(IR,IEQ) = 0.
210 CONTINUE
C
    DO 220 IC=1,NEQ
    SYSK(IEQ,IC) = 0.
220 CONTINUE
    SYSK(IEQ,IEQ) = 1.
    SYSR(IEQ) = 0.
C
200 CONTINUE
C
C   APPLY BOUNDARY CONDITIONS FOR PRESSURES
C
    IEQ1 = 2*NPOIV + 1
    IEQ2 = NEQ
    DO 300 IEQ=IEQ1,IEQ2
    IEQP = IEQ - 2*NPOIV
    IF(BCP(IEQP),EQ.0) GO TO 300

```

```

C
DO 310 IR=1,NEQ
IF(IR.EQ.IEQ) GO TO 310
SYSK(IR,IEQ) = 0.
310 CONTINUE
C
DO 320 IC=1,NEQ
SYSK(IEQ,IC) = 0.
320 CONTINUE
SYSK(IEQ,IEQ) = 1.
SYSR(IEQ) = 0.
C
300 CONTINUE
C
RETURN
END
C-----
C
SUBROUTINE ASSMBLE( IE, INTMAT, AKELE, RELE, SYSK, SYSR,
*                NPOIV, MXNEQ, MXELE )
C
C ASSEMBLE ELEMENT EQUATIONS INTO SYSTEM EQUATIONS
C
C IMPLICIT REAL*8 (A-H,O-Z)
C DIMENSION AKELE(15,15), RELE(15)
C DIMENSION SYSK(MXNEQ,MXNEQ), SYSR(MXNEQ)
C
C INTEGER INTMAT(MXELE,6)
C
C ASSEMBLING SYSTEM STIFFNESS MATRIX
C
C CONTRIBUTION OF COEFFICIENTS ASSOCIATED WITH U & V VELOCITIES
C
DO 100 I=1,6
DO 100 J=1,6
II = INTMAT(IE,I)
JJ = INTMAT(IE,J)
K = I + 6
L = J + 6
KK = NPOIV + II
LL = NPOIV + JJ
SYSK(II,JJ) = SYSK(II,JJ) + AKELE(I,J)
SYSK(II,LL) = SYSK(II,LL) + AKELE(I,L)
SYSK(KK,JJ) = SYSK(KK,JJ) + AKELE(K,J)
SYSK(KK,LL) = SYSK(KK,LL) + AKELE(K,L)
100 CONTINUE
C
C CONTRIBUTION OF COEFFICIENTS ASSOCIATED WITH PRESSURE
C

```

```

DO 200 I=1,6
DO 200 J=1,3
II = INTMAT(IE,I)
JJ = INTMAT(IE,J)
K = I + 6
L = J + 12
KK = NPOIV + II
LL = 2*NPOIV + JJ
SYSK(II,LL) = SYSK(II,LL) + AKELE(I,L)
SYSK(KK,LL) = SYSK(KK,LL) + AKELE(K,L)
SYSK(LL,II) = SYSK(LL,II) + AKELE(L,I)
SYSK(LL,KK) = SYSK(LL,KK) + AKELE(L,K)
200 CONTINUE
C
C ASSEMBLING SYSTEM LOAD VECTOR
C
C CONTRIBUTION OF VALUES ASSOCIATED WITH U & V VELOCITIES
C
DO 300 I=1,6
II = INTMAT(IE,I)
K = I + 6
KK = NPOIV + II
SYSR(II) = SYSR(II) + RELE(I)
SYSR(KK) = SYSR(KK) + RELE(K)
300 CONTINUE
C
C CONTRIBUTION OF VALUES ASSOCIATED WITH PRESSURE
C
DO 400 I=1,3
II = INTMAT(IE,I)
K = I + 12
KK = 2*NPOIV + II
SYSR(KK) = SYSR(KK) + RELE(K)
400 CONTINUE
C
RETURN
END
C
C-----
C
SUBROUTINE GAUSS(N, A, B, X, MXNEQ)
IMPLICIT REAL*8 (A-H,O-Z)
DIMENSION A(MXNEQ,MXNEQ), B(MXNEQ), X(MXNEQ)
C
C PERFORM SCALING
C
CALL SCALE(N, A, B, MXNEQ)
C
C FORWARD ELIMINATION
C

```

```

C   PERFORM ACCORDING TO ORDER OF 'PRIME' FROM 1 TO N-1
C
C   DO 100 IP=1,N-1
C
C   PERFORM PARTIAL PIVOTING
C
C   CALL PIVOT(N, A, B, MXNEQ, IP)
C
C   LOOP OVER EACH EQUATION STARTING FROM THE ONE THAT CORRESPONDS
C   WITH THE ORDER OF 'PRIME' PLUS ONE
C
C   DO 200 IE=IP+1,N
C   RATIO = A(IE,IP)/A(IP,IP)
C
C   COMPUTE NEW COEFFICIENTS OF THE EQUATION CONSIDERED
C
C   DO 300 IC=IP+1,N
C   A(IE,IC) = A(IE,IC) - RATIO*A(IP,IC)
300 CONTINUE
C   B(IE) = B(IE) - RATIO*B(IP)
200 CONTINUE
C
C   SET COEFFICIENTS ON LOWER LEFT PORTION TO ZERO
C
C   DO 400 IE=IP+1,N
C   A(IE,IP) = 0.
400 CONTINUE
100 CONTINUE
C
C   BACK SUBSTITUTION
C
C   COMPUTE SOLUTION OF THE LAST EQUATION
C
C   X(N) = B(N)/A(N,N)
C
C   THEN COMPUTE SOLUTIONS FROM EQUATION N-1 TO 1
C
C   DO 500 IE=N-1,1,-1
C   SUM = 0.
C   DO 600 IC=IE+1,N
C   SUM = SUM + A(IE,IC)*X(IC)
600 CONTINUE
C   X(IE) = (B(IE) - SUM)/A(IE,IE)
500 CONTINUE
C   RETURN
C   END
C
C-----
C
C   SUBROUTINE PIVOT(N, A, B, MXNEQ, IP)

```



```

IMPLICIT REAL*8 (A-H,O-Z)
DIMENSION A(MXNEQ,MXNEQ), B(MXNEQ)

C
C   PERFORM PARTIAL PIVOTING
C
    JP = IP
    BIG = ABS(A(IP,IP))
    DO 10 I=IP+1,N
        AMAX = ABS(A(I,IP))
        IF(AMAX.GT.BIG) THEN
            BIG = AMAX
            JP = I
        ENDIF
10  CONTINUE
    IF(JP.NE.IP) THEN
        DO 20 J=IP,N
            DUMMY = A(JP,J)
            A(JP,J) = A(IP,J)
            A(IP,J) = DUMMY
20  CONTINUE
        DUMMY = B(JP)
        B(JP) = B(IP)
        B(IP) = DUMMY
    ENDIF
    RETURN
    END

C
C-----
C
SUBROUTINE SCALE(N, A, B, MXNEQ)
IMPLICIT REAL*8 (A-H,O-Z)
DIMENSION A(MXNEQ,MXNEQ), B(MXNEQ)

C
C   PERFORM SCALING:
C
    DO 10 IE=1,N
        BIG = ABS(A(IE,1))
        DO 20 IC=2,N
            AMAX = ABS(A(IE,IC))
            IF(AMAX.GT.BIG) BIG = AMAX
20  CONTINUE
        DO 30 IC=1,N
            A(IE,IC) = A(IE,IC)/BIG
30  CONTINUE
        B(IE) = B(IE)/BIG
10  CONTINUE
    RETURN
    END

C
C-----

```

```

C
SUBROUTINE TRI( NPOIV, NELEM, DEN, VIS, COORD,
*             INTMAT, SYSK, SYSR, SOL, MXPOIV,
*             MXELE, MXNEQ )
C
C ESTABLISH ALL ELEMENT MATRICES AND ASSEMBLE THEM TO FORM
C UP SYSTEM EQUATIONS
C
IMPLICIT REAL*8 (A-H,O-Z)
DIMENSION COORD(MXPOIV,2), SYSK(MXNEQ,MXNEQ)
DIMENSION SYSR(MXNEQ), SOL(MXNEQ)
DIMENSION B(3), C(3)
DIMENSION UELE(6), VELE(6), PELE(3)
DIMENSION HX(6,3), HXT(3,6), HY(6,3), HYT(3,6)
DIMENSION AMXX(6,6), AMYY(6,6), AMXY(6,6), AMYX(6,6)
DIMENSION SXX(6,6), SXY(6,6), SYX(6,6), SYI(6,6)
DIMENSION AKX(6,6,6), AKY(6,6,6)
DIMENSION GXX(6,6), GYY(6,6), ALX(6,6), ALY(6,6)
DIMENSION FX(6), FY(6), FI(3)
DIMENSION AKELE(15,15), RELE(15)
C
C INTEGER INTMAT(MXELE,6)
C
C COMPUTE KINEMATIC VISCOSITY
C
ANEW = VIS/DEN
C
C LOOP OVER THE NUMBER OF ELEMENTS
C
DO 500 IE=1,NELEM
C
C FIND ELEMENT LOCAL COORDINATES
C
II = INTMAT(IE,1)
JJ = INTMAT(IE,2)
KK = INTMAT(IE,3)
LL = INTMAT(IE,4)
MM = INTMAT(IE,5)
NN = INTMAT(IE,6)
C
XG1 = COORD(II,1)
XG2 = COORD(JJ,1)
XG3 = COORD(KK,1)
YG1 = COORD(II,2)
YG2 = COORD(JJ,2)
YG3 = COORD(KK,2)
AREA= 0.5*(XG2*(YG3-YG1) + XG1*(YG2-YG3) + XG3*(YG1-YG2))
IF(AREA.LE.0.) WRITE(6,5) IE
5 FORMAT(/, ' !!! ERROR !!! ELEMENT NO.', I5,
*         ' HAS NEGATIVE OR ZERO AREA ', /,

```

```

*          ' --- CHECK F.E. MODEL FOR NODAL COORDINATES',
*          ' AND ELEMENT NODAL CONNECTIONS ---'      )
IF(AREA.LE.0.) STOP
C
B(1) = YG2 - YG3
B(2) = YG3 - YG1
B(3) = YG1 - YG2
C(1) = XG3 - XG2
C(2) = XG1 - XG3
C(3) = XG2 - XG1
C
C
C SET UP [MXX] MATRIX
C
DO 10 I=1,3
DO 10 J=1,3
AMXX(I,J) = B(I)*B(J)/4./AREA
10 CONTINUE
DO 20 I=1,3
DO 20 J=4,6
K = J-3
AMXX(I,J) = B(I)*(B(1)+B(2)+B(3)-B(K))/3./AREA
AMXX(J,I) = AMXX(I,J)
20 CONTINUE
AMXX(4,4) = 2.*(B(2)*B(2)+B(2)*B(3)+B(3)*B(3))/3./AREA
AMXX(5,5) = 2.*(B(1)*B(1)+B(1)*B(3)+B(3)*B(3))/3./AREA
AMXX(6,6) = 2.*(B(2)*B(2)+B(2)*B(1)+B(1)*B(1))/3./AREA
AMXX(4,5) = (2.*B(1)*B(2)+B(1)*B(3)+B(2)*B(3)+B(3)*B(3))/3./AREA
AMXX(5,4) = AMXX(4,5)
AMXX(4,6) = (2.*B(1)*B(3)+B(1)*B(2)+B(2)*B(3)+B(2)*B(2))/3./AREA
AMXX(6,4) = AMXX(4,6)
AMXX(5,6) = (2.*B(2)*B(3)+B(1)*B(3)+B(2)*B(1)+B(1)*B(1))/3./AREA
AMXX(6,5) = AMXX(5,6)
C
C
C SETUP [MYX] MATRIX
C
DO 30 I=1,3
DO 30 J=1,3
AMYY(I,J) = C(I)*C(J)/4./AREA
30 CONTINUE
DO 40 I=1,3
DO 40 J=4,6
K = J-3
AMYY(I,J) = C(I)*(C(1)+C(2)+C(3)-C(K))/3./AREA
AMYY(J,I) = AMYY(I,J)
40 CONTINUE
AMYY(4,4) = 2.*(C(2)*C(2)+C(2)*C(3)+C(3)*C(3))/3./AREA
AMYY(5,5) = 2.*(C(1)*C(1)+C(1)*C(3)+C(3)*C(3))/3./AREA
AMYY(6,6) = 2.*(C(2)*C(2)+C(2)*C(1)+C(1)*C(1))/3./AREA
AMYY(4,5) = (2.*C(1)*C(2)+C(1)*C(3)+C(2)*C(3)+C(3)*C(3))/3./AREA
AMYY(5,4) = AMYY(4,5)

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```

AMY(4,6) = (2.*C(1)*C(3)+C(1)*C(2)+C(2)*C(3)+C(2)*C(2))/3./AREA
AMY(6,4) = AMY(4,6)
AMY(5,6) = (2.*C(2)*C(3)+C(1)*C(3)+C(2)*C(1)+C(1)*C(1))/3./AREA
AMY(6,5) = AMY(5,6)

C
C  SETUP [MYX] MATRIX
C
DO 50 I=1,3
DO 50 J=1,3
AMYX(I,J) = B(I)*C(J)/4./AREA

50 CONTINUE
DO 60 I=1,3
DO 60 J=4,6
K = J-3
AMYX(I,J) = B(I)*(C(1)+C(2)+C(3)-C(K))/3./AREA
AMYX(J,I) = C(I)*(B(1)+B(2)+B(3)-B(K))/3./AREA

60 CONTINUE
AMYX(4,4) = (2.*B(2)*C(2)+B(2)*C(3)+B(3)*C(2)+2.*B(3)*C(3))/3.
*
/AREA
AMYX(4,5) = (2.*B(2)*C(1)+B(2)*C(3)+B(3)*C(1)+B(3)*C(3))/3./AREA
AMYX(4,6) = (2.*B(3)*C(1)+B(3)*C(2)+B(2)*C(1)+B(2)*C(2))/3./AREA
AMYX(5,4) = (2.*B(1)*C(2)+B(1)*C(3)+B(3)*C(2)+B(3)*C(3))/3./AREA
AMYX(5,5) = (2.*B(1)*C(1)+B(1)*C(3)+B(3)*C(1)+2.*B(3)*C(3))/3.
*
/AREA
AMYX(5,6) = (2.*B(3)*C(2)+B(3)*C(1)+B(1)*C(2)+B(1)*C(1))/3./AREA
AMYX(6,4) = (2.*B(1)*C(3)+B(1)*C(2)+B(2)*C(3)+B(2)*C(2))/3./AREA
AMYX(6,5) = (2.*B(2)*C(3)+B(2)*C(1)+B(1)*C(3)+B(1)*C(1))/3./AREA
AMYX(6,6) = (2.*B(1)*C(1)+B(1)*C(2)+B(2)*C(1)+2.*B(2)*C(2))/3.
*
/AREA

C
C  SETUP [MXY] MATRIX
C
DO 70 I=1,6
DO 70 J=1,6
AMXY(I,J) = AMYX(J,I)

70 CONTINUE

C
C  SETUP [SXX], [SXY], [SYX], AND [SYY] MATRICES
C
DO 80 I=1,6
DO 80 J=1,6
SXX(I,J) = 2.*ANEW*AMXX(I,J) + ANEW*AMY(I,J)

80 CONTINUE

C
DO 90 I=1,6
DO 90 J=1,6
SXY(I,J) = ANEW*AMXY(I,J)

90 CONTINUE

C
DO 100 I=1,6

```

```

DO 100 J=1,6
SYX(I,J) = ANEW*AMYX(I,J)
100 CONTINUE
C
DO 110 I=1,6
DO 110 J=1,6
SYY(I,J) = ANEW*AMXX(I,J) + 2.*ANEW*AMYY(I,J)
110 CONTINUE
C
C SETUP [HX] AND [HXT] MATRICES
C
DO 120 I=1,3
DO 120 J=1,3
HX(I,J) = B(1)/6./DEN
120 CONTINUE
HX(4,1) = B(2)/6./DEN + B(3)/6./DEN
HX(4,2) = B(2)/6./DEN + B(3)/3./DEN
HX(4,3) = B(2)/3./DEN + B(3)/6./DEN
HX(5,1) = B(3)/3./DEN + B(1)/6./DEN
HX(5,2) = B(3)/6./DEN + B(1)/6./DEN
HX(5,3) = B(3)/6./DEN + B(1)/3./DEN
HX(6,1) = B(1)/6./DEN + B(2)/3./DEN
HX(6,2) = B(1)/3./DEN + B(2)/6./DEN
HX(6,3) = B(1)/6./DEN + B(2)/6./DEN
DO 130 I=1,3
DO 130 J=1,6
HXT(I,J) = HX(J,I)
130 CONTINUE
C
C SETUP [HY] AND [HYT] MATRICES
C
DO 140 I=1,3
DO 140 J=1,3
HY(I,J) = C(1)/6./DEN
140 CONTINUE
HY(4,1) = C(2)/6./DEN + C(3)/6./DEN
HY(4,2) = C(2)/6./DEN + C(3)/3./DEN
HY(4,3) = C(2)/3./DEN + C(3)/6./DEN
HY(5,1) = C(3)/3./DEN + C(1)/6./DEN
HY(5,2) = C(3)/6./DEN + C(1)/6./DEN
HY(5,3) = C(3)/6./DEN + C(1)/3./DEN
HY(6,1) = C(1)/6./DEN + C(2)/3./DEN
HY(6,2) = C(1)/3./DEN + C(2)/6./DEN
HY(6,3) = C(1)/6./DEN + C(2)/6./DEN
DO 150 I=1,3
DO 150 J=1,6
HYT(I,J) = HY(J,I)
150 CONTINUE
C
C SET UP [AKX-1] MATRIX

```

C

$$FAC = B(1)/360.$$

$$I = 1$$

$$AKX(1,1,1) = 30.*FAC$$

$$AKX(1,2,1) = 15.*FAC$$

$$AKX(1,3,1) = 15.*FAC$$

$$AKX(1,4,1) = 12.*FAC$$

$$AKX(1,5,1) = 24.*FAC$$

$$AKX(1,6,1) = 24.*FAC$$

$$AKX(2,1,1) = 15.*FAC$$

$$AKX(2,2,1) = 30.*FAC$$

$$AKX(2,3,1) = 15.*FAC$$

$$AKX(2,4,1) = 24.*FAC$$

$$AKX(2,5,1) = 12.*FAC$$

$$AKX(2,6,1) = 24.*FAC$$

$$AKX(3,1,1) = 15.*FAC$$

$$AKX(3,2,1) = 15.*FAC$$

$$AKX(3,3,1) = 30.*FAC$$

$$AKX(3,4,1) = 24.*FAC$$

$$AKX(3,5,1) = 24.*FAC$$

$$AKX(3,6,1) = 12.*FAC$$

$$AKX(4,1,1) = 12.*FAC$$

$$AKX(4,2,1) = 24.*FAC$$

$$AKX(4,3,1) = 24.*FAC$$

$$AKX(4,4,1) = 32.*FAC$$

$$AKX(4,5,1) = 16.*FAC$$

$$AKX(4,6,1) = 16.*FAC$$

$$AKX(5,1,1) = 24.*FAC$$

$$AKX(5,2,1) = 12.*FAC$$

$$AKX(5,3,1) = 24.*FAC$$

$$AKX(5,4,1) = 16.*FAC$$

$$AKX(5,5,1) = 32.*FAC$$

$$AKX(5,6,1) = 16.*FAC$$

$$AKX(6,1,1) = 24.*FAC$$

$$AKX(6,2,1) = 24.*FAC$$

$$AKX(6,3,1) = 12.*FAC$$

$$AKX(6,4,1) = 16.*FAC$$

$$AKX(6,5,1) = 16.*FAC$$

$$AKX(6,6,1) = 32.*FAC$$

C

C SET UP [AKY-1] MATRIX

C

$$FAC = C(1)/360.$$

$$I = 1$$

$$AKY(1,1,1) = 30.*FAC$$

$$AKY(1,2,1) = 15.*FAC$$

$$AKY(1,3,1) = 15.*FAC$$

$$AKY(1,4,1) = 12.*FAC$$

$$AKY(1,5,1) = 24.*FAC$$

$$AKY(1,6,1) = 24.*FAC$$



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AKY(2,1,1) = 15.*FAC
 AKY(2,2,1) = 30.*FAC
 AKY(2,3,1) = 15.*FAC
 AKY(2,4,1) = 24.*FAC
 AKY(2,5,1) = 12.*FAC
 AKY(2,6,1) = 24.*FAC
 AKY(3,1,1) = 15.*FAC
 AKY(3,2,1) = 15.*FAC
 AKY(3,3,1) = 30.*FAC
 AKY(3,4,1) = 24.*FAC
 AKY(3,5,1) = 24.*FAC
 AKY(3,6,1) = 12.*FAC
 AKY(4,1,1) = 12.*FAC
 AKY(4,2,1) = 24.*FAC
 AKY(4,3,1) = 24.*FAC
 AKY(4,4,1) = 32.*FAC
 AKY(4,5,1) = 16.*FAC
 AKY(4,6,1) = 16.*FAC
 AKY(5,1,1) = 24.*FAC
 AKY(5,2,1) = 12.*FAC
 AKY(5,3,1) = 24.*FAC
 AKY(5,4,1) = 16.*FAC
 AKY(5,5,1) = 32.*FAC
 AKY(5,6,1) = 16.*FAC
 AKY(6,1,1) = 24.*FAC
 AKY(6,2,1) = 24.*FAC
 AKY(6,3,1) = 12.*FAC
 AKY(6,4,1) = 16.*FAC
 AKY(6,5,1) = 16.*FAC
 AKY(6,6,1) = 32.*FAC

C

C SET UP [AKX-2] MATRIX

C

FAC = B(2)/360.

I = 2

AKX(1,1,1) = 30.*FAC
 AKX(1,2,1) = 15.*FAC
 AKX(1,3,1) = 15.*FAC
 AKX(1,4,1) = 12.*FAC
 AKX(1,5,1) = 24.*FAC
 AKX(1,6,1) = 24.*FAC
 AKX(2,1,1) = 15.*FAC
 AKX(2,2,1) = 30.*FAC
 AKX(2,3,1) = 15.*FAC
 AKX(2,4,1) = 24.*FAC
 AKX(2,5,1) = 12.*FAC
 AKX(2,6,1) = 24.*FAC
 AKX(3,1,1) = 15.*FAC
 AKX(3,2,1) = 15.*FAC
 AKX(3,3,1) = 30.*FAC



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AKX(3,4,1) = 24.*FAC
 AKX(3,5,1) = 24.*FAC
 AKX(3,6,1) = 12.*FAC
 AKX(4,1,1) = 12.*FAC
 AKX(4,2,1) = 24.*FAC
 AKX(4,3,1) = 24.*FAC
 AKX(4,4,1) = 32.*FAC
 AKX(4,5,1) = 16.*FAC
 AKX(4,6,1) = 16.*FAC
 AKX(5,1,1) = 24.*FAC
 AKX(5,2,1) = 12.*FAC
 AKX(5,3,1) = 24.*FAC
 AKX(5,4,1) = 16.*FAC
 AKX(5,5,1) = 32.*FAC
 AKX(5,6,1) = 16.*FAC
 AKX(6,1,1) = 24.*FAC
 AKX(6,2,1) = 24.*FAC
 AKX(6,3,1) = 12.*FAC
 AKX(6,4,1) = 16.*FAC
 AKX(6,5,1) = 16.*FAC
 AKX(6,6,1) = 32.*FAC

C

C SET UP [AKY-2] MATRIX

C

FAC = C(2)/360.

I = 2

AKY(1,1,1) = 30.*FAC
 AKY(1,2,1) = 15.*FAC
 AKY(1,3,1) = 15.*FAC
 AKY(1,4,1) = 12.*FAC
 AKY(1,5,1) = 24.*FAC
 AKY(1,6,1) = 24.*FAC
 AKY(2,1,1) = 15.*FAC
 AKY(2,2,1) = 30.*FAC
 AKY(2,3,1) = 15.*FAC
 AKY(2,4,1) = 24.*FAC
 AKY(2,5,1) = 12.*FAC
 AKY(2,6,1) = 24.*FAC
 AKY(3,1,1) = 15.*FAC
 AKY(3,2,1) = 15.*FAC
 AKY(3,3,1) = 30.*FAC
 AKY(3,4,1) = 24.*FAC
 AKY(3,5,1) = 24.*FAC
 AKY(3,6,1) = 12.*FAC
 AKY(4,1,1) = 12.*FAC
 AKY(4,2,1) = 24.*FAC
 AKY(4,3,1) = 24.*FAC
 AKY(4,4,1) = 32.*FAC
 AKY(4,5,1) = 16.*FAC
 AKY(4,6,1) = 16.*FAC



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$AKY(5,1,1) = 24.*FAC$
 $AKY(5,2,1) = 12.*FAC$
 $AKY(5,3,1) = 24.*FAC$
 $AKY(5,4,1) = 16.*FAC$
 $AKY(5,5,1) = 32.*FAC$
 $AKY(5,6,1) = 16.*FAC$
 $AKY(6,1,1) = 24.*FAC$
 $AKY(6,2,1) = 24.*FAC$
 $AKY(6,3,1) = 12.*FAC$
 $AKY(6,4,1) = 16.*FAC$
 $AKY(6,5,1) = 16.*FAC$
 $AKY(6,6,1) = 32.*FAC$

C

C SET UP [AKX-3] MATRIX

C

$FAC = B(3)/360.$

$I = 3$

$AKX(1,1,1) = 30.*FAC$
 $AKX(1,2,1) = 15.*FAC$
 $AKX(1,3,1) = 15.*FAC$
 $AKX(1,4,1) = 12.*FAC$
 $AKX(1,5,1) = 24.*FAC$
 $AKX(1,6,1) = 24.*FAC$
 $AKX(2,1,1) = 15.*FAC$
 $AKX(2,2,1) = 30.*FAC$
 $AKX(2,3,1) = 15.*FAC$
 $AKX(2,4,1) = 24.*FAC$
 $AKX(2,5,1) = 12.*FAC$
 $AKX(2,6,1) = 24.*FAC$
 $AKX(3,1,1) = 15.*FAC$
 $AKX(3,2,1) = 15.*FAC$
 $AKX(3,3,1) = 30.*FAC$
 $AKX(3,4,1) = 24.*FAC$
 $AKX(3,5,1) = 24.*FAC$
 $AKX(3,6,1) = 12.*FAC$
 $AKX(4,1,1) = 12.*FAC$
 $AKX(4,2,1) = 24.*FAC$
 $AKX(4,3,1) = 24.*FAC$
 $AKX(4,4,1) = 32.*FAC$
 $AKX(4,5,1) = 16.*FAC$
 $AKX(4,6,1) = 16.*FAC$
 $AKX(5,1,1) = 24.*FAC$
 $AKX(5,2,1) = 12.*FAC$
 $AKX(5,3,1) = 24.*FAC$
 $AKX(5,4,1) = 16.*FAC$
 $AKX(5,5,1) = 32.*FAC$
 $AKX(5,6,1) = 16.*FAC$
 $AKX(6,1,1) = 24.*FAC$
 $AKX(6,2,1) = 24.*FAC$
 $AKX(6,3,1) = 12.*FAC$



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AKX(6,4,1) = 16.*FAC
 AKX(6,5,1) = 16.*FAC
 AKX(6,6,1) = 32.*FAC

C

C SET UP [AKY-3] MATRIX

C

FAC = C(3)/360.

I = 3

AKY(1,1,1) = 30.*FAC
 AKY(1,2,1) = 15.*FAC
 AKY(1,3,1) = 15.*FAC
 AKY(1,4,1) = 12.*FAC
 AKY(1,5,1) = 24.*FAC
 AKY(1,6,1) = 24.*FAC
 AKY(2,1,1) = 15.*FAC
 AKY(2,2,1) = 30.*FAC
 AKY(2,3,1) = 15.*FAC
 AKY(2,4,1) = 24.*FAC
 AKY(2,5,1) = 12.*FAC
 AKY(2,6,1) = 24.*FAC
 AKY(3,1,1) = 15.*FAC
 AKY(3,2,1) = 15.*FAC
 AKY(3,3,1) = 30.*FAC
 AKY(3,4,1) = 24.*FAC
 AKY(3,5,1) = 24.*FAC
 AKY(3,6,1) = 12.*FAC
 AKY(4,1,1) = 12.*FAC
 AKY(4,2,1) = 24.*FAC
 AKY(4,3,1) = 24.*FAC
 AKY(4,4,1) = 32.*FAC
 AKY(4,5,1) = 16.*FAC
 AKY(4,6,1) = 16.*FAC
 AKY(5,1,1) = 24.*FAC
 AKY(5,2,1) = 12.*FAC
 AKY(5,3,1) = 24.*FAC
 AKY(5,4,1) = 16.*FAC
 AKY(5,5,1) = 32.*FAC
 AKY(5,6,1) = 16.*FAC
 AKY(6,1,1) = 24.*FAC
 AKY(6,2,1) = 24.*FAC
 AKY(6,3,1) = 12.*FAC
 AKY(6,4,1) = 16.*FAC
 AKY(6,5,1) = 16.*FAC
 AKY(6,6,1) = 32.*FAC

C

C SET UP [AKX-4] MATRIX

C

FAC1 = B(2)/630.

FAC2 = B(3)/630.

I = 4



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$AKX(1,1,1) = 42 \cdot FAC1 + 42 \cdot FAC2$
 $AKX(1,2,1) = 21 \cdot FAC1 + 42 \cdot FAC2$
 $AKX(1,3,1) = 42 \cdot FAC1 + 21 \cdot FAC2$
 $AKX(1,4,1) = 28 \cdot FAC1 + 28 \cdot FAC2$
 $AKX(1,5,1) = 56 \cdot FAC1 + 28 \cdot FAC2$
 $AKX(1,6,1) = 28 \cdot FAC1 + 56 \cdot FAC2$
 $AKX(2,1,1) = 21 \cdot FAC1 + 42 \cdot FAC2$
 $AKX(2,2,1) = 42 \cdot FAC1 + 126 \cdot FAC2$
 $AKX(2,3,1) = 42 \cdot FAC1 + 42 \cdot FAC2$
 $AKX(2,4,1) = 56 \cdot FAC1 + 84 \cdot FAC2$
 $AKX(2,5,1) = 28 \cdot FAC1 + 28 \cdot FAC2$
 $AKX(2,6,1) = 28 \cdot FAC1 + 84 \cdot FAC2$
 $AKX(3,1,1) = 42 \cdot FAC1 + 21 \cdot FAC2$
 $AKX(3,2,1) = 42 \cdot FAC1 + 42 \cdot FAC2$
 $AKX(3,3,1) = 126 \cdot FAC1 + 42 \cdot FAC2$
 $AKX(3,4,1) = 84 \cdot FAC1 + 56 \cdot FAC2$
 $AKX(3,5,1) = 84 \cdot FAC1 + 28 \cdot FAC2$
 $AKX(3,6,1) = 28 \cdot FAC1 + 28 \cdot FAC2$
 $AKX(4,1,1) = 28 \cdot FAC1 + 28 \cdot FAC2$
 $AKX(4,2,1) = 56 \cdot FAC1 + 84 \cdot FAC2$
 $AKX(4,3,1) = 84 \cdot FAC1 + 56 \cdot FAC2$
 $AKX(4,4,1) = 96 \cdot FAC1 + 96 \cdot FAC2$
 $AKX(4,5,1) = 48 \cdot FAC1 + 32 \cdot FAC2$
 $AKX(4,6,1) = 32 \cdot FAC1 + 48 \cdot FAC2$
 $AKX(5,1,1) = 56 \cdot FAC1 + 28 \cdot FAC2$
 $AKX(5,2,1) = 28 \cdot FAC1 + 28 \cdot FAC2$
 $AKX(5,3,1) = 84 \cdot FAC1 + 28 \cdot FAC2$
 $AKX(5,4,1) = 48 \cdot FAC1 + 32 \cdot FAC2$
 $AKX(5,5,1) = 96 \cdot FAC1 + 32 \cdot FAC2$
 $AKX(5,6,1) = 32 \cdot FAC1 + 32 \cdot FAC2$
 $AKX(6,1,1) = 28 \cdot FAC1 + 56 \cdot FAC2$
 $AKX(6,2,1) = 28 \cdot FAC1 + 84 \cdot FAC2$
 $AKX(6,3,1) = 28 \cdot FAC1 + 28 \cdot FAC2$
 $AKX(6,4,1) = 32 \cdot FAC1 + 48 \cdot FAC2$
 $AKX(6,5,1) = 32 \cdot FAC1 + 32 \cdot FAC2$
 $AKX(6,6,1) = 32 \cdot FAC1 + 96 \cdot FAC2$

C

C SET UP [AKY-4] MATRIX

C

$$FAC1 = C(2)/630.$$

$$FAC2 = C(3)/630.$$

$$I = 4$$

$AKY(1,1,1) = 42 \cdot FAC1 + 42 \cdot FAC2$
 $AKY(1,2,1) = 21 \cdot FAC1 + 42 \cdot FAC2$
 $AKY(1,3,1) = 42 \cdot FAC1 + 21 \cdot FAC2$
 $AKY(1,4,1) = 28 \cdot FAC1 + 28 \cdot FAC2$
 $AKY(1,5,1) = 56 \cdot FAC1 + 28 \cdot FAC2$
 $AKY(1,6,1) = 28 \cdot FAC1 + 56 \cdot FAC2$
 $AKY(2,1,1) = 21 \cdot FAC1 + 42 \cdot FAC2$
 $AKY(2,2,1) = 42 \cdot FAC1 + 126 \cdot FAC2$

$AKY(2,3,1) = 42.*FAC1+42.*FAC2$
 $AKY(2,4,1) = 56.*FAC1+84.*FAC2$
 $AKY(2,5,1) = 28.*FAC1+28.*FAC2$
 $AKY(2,6,1) = 28.*FAC1+84.*FAC2$
 $AKY(3,1,1) = 42.*FAC1+21.*FAC2$
 $AKY(3,2,1) = 42.*FAC1+42.*FAC2$
 $AKY(3,3,1) = 126.*FAC1+42.*FAC2$
 $AKY(3,4,1) = 84.*FAC1+56.*FAC2$
 $AKY(3,5,1) = 84.*FAC1+28.*FAC2$
 $AKY(3,6,1) = 28.*FAC1+28.*FAC2$
 $AKY(4,1,1) = 28.*FAC1+28.*FAC2$
 $AKY(4,2,1) = 56.*FAC1+84.*FAC2$
 $AKY(4,3,1) = 84.*FAC1+56.*FAC2$
 $AKY(4,4,1) = 96.*FAC1+96.*FAC2$
 $AKY(4,5,1) = 48.*FAC1+32.*FAC2$
 $AKY(4,6,1) = 32.*FAC1+48.*FAC2$
 $AKY(5,1,1) = 56.*FAC1+28.*FAC2$
 $AKY(5,2,1) = 28.*FAC1+28.*FAC2$
 $AKY(5,3,1) = 84.*FAC1+28.*FAC2$
 $AKY(5,4,1) = 48.*FAC1+32.*FAC2$
 $AKY(5,5,1) = 96.*FAC1+32.*FAC2$
 $AKY(5,6,1) = 32.*FAC1+32.*FAC2$
 $AKY(6,1,1) = 28.*FAC1+56.*FAC2$
 $AKY(6,2,1) = 28.*FAC1+84.*FAC2$
 $AKY(6,3,1) = 28.*FAC1+28.*FAC2$
 $AKY(6,4,1) = 32.*FAC1+48.*FAC2$
 $AKY(6,5,1) = 32.*FAC1+32.*FAC2$
 $AKY(6,6,1) = 32.*FAC1+96.*FAC2$

C

C SET UP [AKX-5] MATRIX

C

 $FAC1 = B(1)/630.$
 $FAC2 = B(3)/630.$
 $I = 5$

$AKX(1,1,1) = 42.*FAC1+126.*FAC2$
 $AKX(1,2,1) = 21.*FAC1+42.*FAC2$
 $AKX(1,3,1) = 42.*FAC1+42.*FAC2$
 $AKX(1,4,1) = 28.*FAC1+28.*FAC2$
 $AKX(1,5,1) = 56.*FAC1+84.*FAC2$
 $AKX(1,6,1) = 28.*FAC1+84.*FAC2$
 $AKX(2,1,1) = 21.*FAC1+42.*FAC2$
 $AKX(2,2,1) = 42.*FAC1+42.*FAC2$
 $AKX(2,3,1) = 42.*FAC1+21.*FAC2$
 $AKX(2,4,1) = 56.*FAC1+28.*FAC2$
 $AKX(2,5,1) = 28.*FAC1+28.*FAC2$
 $AKX(2,6,1) = 28.*FAC1+56.*FAC2$
 $AKX(3,1,1) = 42.*FAC1+42.*FAC2$
 $AKX(3,2,1) = 42.*FAC1+21.*FAC2$
 $AKX(3,3,1) = 126.*FAC1+42.*FAC2$
 $AKX(3,4,1) = 84.*FAC1+28.*FAC2$

$AKX(3,5,1) = 84.*FAC1+56.*FAC2$
 $AKX(3,6,1) = 28.*FAC1+28.*FAC2$
 $AKX(4,1,1) = 28.*FAC1+28.*FAC2$
 $AKX(4,2,1) = 56.*FAC1+28.*FAC2$
 $AKX(4,3,1) = 84.*FAC1+28.*FAC2$
 $AKX(4,4,1) = 96.*FAC1+32.*FAC2$
 $AKX(4,5,1) = 48.*FAC1+32.*FAC2$
 $AKX(4,6,1) = 32.*FAC1+32.*FAC2$
 $AKX(5,1,1) = 56.*FAC1+84.*FAC2$
 $AKX(5,2,1) = 28.*FAC1+28.*FAC2$
 $AKX(5,3,1) = 84.*FAC1+56.*FAC2$
 $AKX(5,4,1) = 48.*FAC1+32.*FAC2$
 $AKX(5,5,1) = 96.*FAC1+96.*FAC2$
 $AKX(5,6,1) = 32.*FAC1+48.*FAC2$
 $AKX(6,1,1) = 28.*FAC1+84.*FAC2$
 $AKX(6,2,1) = 28.*FAC1+56.*FAC2$
 $AKX(6,3,1) = 28.*FAC1+28.*FAC2$
 $AKX(6,4,1) = 32.*FAC1+32.*FAC2$
 $AKX(6,5,1) = 32.*FAC1+48.*FAC2$
 $AKX(6,6,1) = 32.*FAC1+96.*FAC2$

C

C SET UP [AKY-5] MATRIX

C

$$FAC1 = C(1)/630.$$

$$FAC2 = C(3)/630.$$

$$I = 5$$

$AKY(1,1,1) = 42.*FAC1+126.*FAC2$
 $AKY(1,2,1) = 21.*FAC1+42.*FAC2$
 $AKY(1,3,1) = 42.*FAC1+42.*FAC2$
 $AKY(1,4,1) = 28.*FAC1+28.*FAC2$
 $AKY(1,5,1) = 56.*FAC1+84.*FAC2$
 $AKY(1,6,1) = 28.*FAC1+84.*FAC2$
 $AKY(2,1,1) = 21.*FAC1+42.*FAC2$
 $AKY(2,2,1) = 42.*FAC1+42.*FAC2$
 $AKY(2,3,1) = 42.*FAC1+21.*FAC2$
 $AKY(2,4,1) = 56.*FAC1+28.*FAC2$
 $AKY(2,5,1) = 28.*FAC1+28.*FAC2$
 $AKY(2,6,1) = 28.*FAC1+56.*FAC2$
 $AKY(3,1,1) = 42.*FAC1+42.*FAC2$
 $AKY(3,2,1) = 42.*FAC1+21.*FAC2$
 $AKY(3,3,1) = 126.*FAC1+42.*FAC2$
 $AKY(3,4,1) = 84.*FAC1+28.*FAC2$
 $AKY(3,5,1) = 84.*FAC1+56.*FAC2$
 $AKY(3,6,1) = 28.*FAC1+28.*FAC2$
 $AKY(4,1,1) = 28.*FAC1+28.*FAC2$
 $AKY(4,2,1) = 56.*FAC1+28.*FAC2$
 $AKY(4,3,1) = 84.*FAC1+28.*FAC2$
 $AKY(4,4,1) = 96.*FAC1+32.*FAC2$
 $AKY(4,5,1) = 48.*FAC1+32.*FAC2$
 $AKY(4,6,1) = 32.*FAC1+32.*FAC2$

$AKY(5,1,1) = 56.*FAC1+84.*FAC2$
 $AKY(5,2,1) = 28.*FAC1+28.*FAC2$
 $AKY(5,3,1) = 84.*FAC1+56.*FAC2$
 $AKY(5,4,1) = 48.*FAC1+32.*FAC2$
 $AKY(5,5,1) = 96.*FAC1+96.*FAC2$
 $AKY(5,6,1) = 32.*FAC1+48.*FAC2$
 $AKY(6,1,1) = 28.*FAC1+84.*FAC2$
 $AKY(6,2,1) = 28.*FAC1+56.*FAC2$
 $AKY(6,3,1) = 28.*FAC1+28.*FAC2$
 $AKY(6,4,1) = 32.*FAC1+32.*FAC2$
 $AKY(6,5,1) = 32.*FAC1+48.*FAC2$
 $AKY(6,6,1) = 32.*FAC1+96.*FAC2$

C

C SET UP [AKX-6] MATRIX

C

$FAC1 = B(1)/630.$

$FAC2 = B(2)/630.$

$I = 6$

$AKX(1,1,1) = 42.*FAC1+126.*FAC2$
 $AKX(1,2,1) = 42.*FAC1+42.*FAC2$
 $AKX(1,3,1) = 21.*FAC1+42.*FAC2$
 $AKX(1,4,1) = 28.*FAC1+28.*FAC2$
 $AKX(1,5,1) = 28.*FAC1+84.*FAC2$
 $AKX(1,6,1) = 56.*FAC1+84.*FAC2$
 $AKX(2,1,1) = 42.*FAC1+42.*FAC2$
 $AKX(2,2,1) = 126.*FAC1+42.*FAC2$
 $AKX(2,3,1) = 42.*FAC1+21.*FAC2$
 $AKX(2,4,1) = 84.*FAC1+28.*FAC2$
 $AKX(2,5,1) = 28.*FAC1+28.*FAC2$
 $AKX(2,6,1) = 84.*FAC1+56.*FAC2$
 $AKX(3,1,1) = 21.*FAC1+42.*FAC2$
 $AKX(3,2,1) = 42.*FAC1+21.*FAC2$
 $AKX(3,3,1) = 42.*FAC1+42.*FAC2$
 $AKX(3,4,1) = 56.*FAC1+28.*FAC2$
 $AKX(3,5,1) = 28.*FAC1+56.*FAC2$
 $AKX(3,6,1) = 28.*FAC1+28.*FAC2$
 $AKX(4,1,1) = 28.*FAC1+28.*FAC2$
 $AKX(4,2,1) = 84.*FAC1+28.*FAC2$
 $AKX(4,3,1) = 56.*FAC1+28.*FAC2$
 $AKX(4,4,1) = 96.*FAC1+32.*FAC2$
 $AKX(4,5,1) = 32.*FAC1+32.*FAC2$
 $AKX(4,6,1) = 48.*FAC1+32.*FAC2$
 $AKX(5,1,1) = 28.*FAC1+84.*FAC2$
 $AKX(5,2,1) = 28.*FAC1+28.*FAC2$
 $AKX(5,3,1) = 28.*FAC1+56.*FAC2$
 $AKX(5,4,1) = 32.*FAC1+32.*FAC2$
 $AKX(5,5,1) = 32.*FAC1+96.*FAC2$
 $AKX(5,6,1) = 32.*FAC1+48.*FAC2$
 $AKX(6,1,1) = 56.*FAC1+84.*FAC2$
 $AKX(6,2,1) = 84.*FAC1+56.*FAC2$

$AKX(6,3,1) = 28.*FAC1+28.*FAC2$
 $AKX(6,4,1) = 48.*FAC1+32.*FAC2$
 $AKX(6,5,1) = 32.*FAC1+48.*FAC2$
 $AKX(6,6,1) = 96.*FAC1+96.*FAC2$

C

C SET UP [AKY-6] MATRIX

C

FAC1 = C(1)/630.

FAC2 = C(2)/630.

I = 6

AKY(1,1,1) = 42.*FAC1+126.*FAC2

AKY(1,2,1) = 42.*FAC1+42.*FAC2

AKY(1,3,1) = 21.*FAC1+42.*FAC2

AKY(1,4,1) = 28.*FAC1+28.*FAC2

AKY(1,5,1) = 28.*FAC1+84.*FAC2

AKY(1,6,1) = 56.*FAC1+84.*FAC2

AKY(2,1,1) = 42.*FAC1+42.*FAC2

AKY(2,2,1) = 126.*FAC1+42.*FAC2

AKY(2,3,1) = 42.*FAC1+21.*FAC2

AKY(2,4,1) = 84.*FAC1+28.*FAC2

AKY(2,5,1) = 28.*FAC1+28.*FAC2

AKY(2,6,1) = 84.*FAC1+56.*FAC2

AKY(3,1,1) = 21.*FAC1+42.*FAC2

AKY(3,2,1) = 42.*FAC1+21.*FAC2

AKY(3,3,1) = 42.*FAC1+42.*FAC2

AKY(3,4,1) = 56.*FAC1+28.*FAC2

AKY(3,5,1) = 28.*FAC1+56.*FAC2

AKY(3,6,1) = 28.*FAC1+28.*FAC2

AKY(4,1,1) = 28.*FAC1+28.*FAC2

AKY(4,2,1) = 84.*FAC1+28.*FAC2

AKY(4,3,1) = 56.*FAC1+28.*FAC2

AKY(4,4,1) = 96.*FAC1+32.*FAC2

AKY(4,5,1) = 32.*FAC1+32.*FAC2

AKY(4,6,1) = 48.*FAC1+32.*FAC2

AKY(5,1,1) = 28.*FAC1+84.*FAC2

AKY(5,2,1) = 28.*FAC1+28.*FAC2

AKY(5,3,1) = 28.*FAC1+56.*FAC2

AKY(5,4,1) = 32.*FAC1+32.*FAC2

AKY(5,5,1) = 32.*FAC1+96.*FAC2

AKY(5,6,1) = 32.*FAC1+48.*FAC2

AKY(6,1,1) = 56.*FAC1+84.*FAC2

AKY(6,2,1) = 84.*FAC1+56.*FAC2

AKY(6,3,1) = 28.*FAC1+28.*FAC2

AKY(6,4,1) = 48.*FAC1+32.*FAC2

AKY(6,5,1) = 32.*FAC1+48.*FAC2

AKY(6,6,1) = 96.*FAC1+96.*FAC2

C

C EXTRACT ELEMENT NODAL U, V, P

C

UELE(1) = SOL(II)

```

UELE(2) = SOL(JJ)
UELE(3) = SOL(KK)
UELE(4) = SOL(LL)
UELE(5) = SOL(MM)
UELE(6) = SOL(NN)
VELE(1) = SOL(II+NPOIV)
VELE(2) = SOL(JJ+NPOIV)
VELE(3) = SOL(KK+NPOIV)
VELE(4) = SOL(LL+NPOIV)
VELE(5) = SOL(MM+NPOIV)
VELE(6) = SOL(NN+NPOIV)
PELE(1) = SOL(II+NPOIV+NPOIV)
PELE(2) = SOL(JJ+NPOIV+NPOIV)
PELE(3) = SOL(KK+NPOIV+NPOIV)
C
C  SET UP [GX], [GY], [ALX], [ALY] MATRICES
C
DO 160 I=1,6
DO 160 J=1,6
GXX(I,J) = 0.
GYY(I,J) = 0.
ALX(I,J) = 0.
ALY(I,J) = 0.
DO 170 K=1,6
GXX(I,J) = GXX(I,J) + AKX(I,J,K)*UELE(K) + AKX(I,K,J)*UELE(K) +
*      AKY(I,K,J)*VELE(K)
GYY(I,J) = GYY(I,J) + AKY(I,J,K)*VELE(K) + AKY(I,K,J)*VELE(K) +
*      AKX(I,K,J)*UELE(K)
ALX(I,J) = ALX(I,J) + AKX(I,J,K)*VELE(K)
ALY(I,J) = ALY(I,J) + AKY(I,J,K)*UELE(K)
170 CONTINUE
GXX(I,J) = GXX(I,J) + SXX(I,J)
GYY(I,J) = GYY(I,J) + SYX(I,J)
ALX(I,J) = ALX(I,J) + SXY(I,J)
ALY(I,J) = ALY(I,J) + SYX(I,J)
160 CONTINUE
C
C  THEN THE MATRIX 15*15 ON LHS OF THE ELEMENT EQS. IS
C
DO 180 I=1,6
DO 190 J=1,6
AKELE(I ,J ) = GXX(I,J)
AKELE(I+6,J+6) = GYY(I,J)
AKELE(I ,J+6) = ALY(I,J)
AKELE(I+6,J ) = ALX(I,J)
190 CONTINUE
DO 200 J=1,3
AKELE(I ,J+12) = -1.*HX(I,J)
AKELE(I+6,J+12) = -1.*HY(I,J)
200 CONTINUE

```



```

180 CONTINUE
    DO 210 I=1,3
        DO 220 J=1,6
            AKELE(I+12,J ) = HXT(I,J)
            AKELE(I+12,J+6) = HYT(I,J)
220 CONTINUE
        DO 230 J=1,3
            AKELE(I+12,J+12) = 0.
230 CONTINUE
210 CONTINUE
C
C   COMPUTE [FX] MATRIX
C
    DO 240 I=1,6
        SUMKX = 0.
        SUMKY = 0.
        SUMHX = 0.
        SUMSXX = 0.
        SUMSXY = 0.
        DO 250 J=1,6
            DO 250 K=1,6
                SUMKX = SUMKX + AKX(I,J,K)*UELE(J)*UELE(K)
                SUMKY = SUMKY + AKY(I,J,K)*VELE(J)*VELE(K)
250 CONTINUE
            DO 260 J=1,3
                SUMHX = SUMHX + HX(I,J)*PELE(J)
260 CONTINUE
            DO 270 J=1,6
                SUMSXX = SUMSXX + SXX(I,J)*UELE(J)
                SUMSXY = SUMSXY + SXY(I,J)*VELE(J)
270 CONTINUE
            FX(I) = SUMKX + SUMKY - SUMHX + SUMSXX + SUMSXY
240 CONTINUE
C
C   COMPUTE [FY] MATRIX
C
    DO 280 I=1,6
        SUMKX = 0.
        SUMKY = 0.
        SUMHY = 0.
        SUMSYX = 0.
        SUMSYY = 0.
        DO 290 J=1,6
            DO 290 K=1,6
                SUMKX = SUMKX + AKX(I,J,K)*UELE(J)*VELE(K)
                SUMKY = SUMKY + AKY(I,J,K)*VELE(J)*UELE(K)
290 CONTINUE
            DO 300 J=1,3
                SUMHY = SUMHY + HY(I,J)*PELE(J)
300 CONTINUE

```

```

DO 310 J=1,6
SUMSYX = SUMSYX + SYX(I,J)*UELE(J)
SUMSYY = SUMSYY + SYY(I,J)*VELE(J)
310 CONTINUE
FY(I) = SUMKX + SUMKY - SUMHY + SUMSYX + SUMSYY
280 CONTINUE
C
C COMPUTE [FI] MATRIX
C
DO 320 I=1,3
FI(I) = 0.
DO 330 J=1,6
FI(I) = FI(I) + HXT(I,J)*UELE(J) + HYT(I,J)*VELE(J)
330 CONTINUE
320 CONTINUE
C
C THUS THE RESIDUAL VECTOR ON RHS OF ELEMENT EQS. IS
C
DO 340 I=1,6
RELE(I) = -1.*FX(I)
RELE(I+6) = -1.*FY(I)
340 CONTINUE
DO 350 I=1,3
RELE(I+12) = -1.*FI(I)
350 CONTINUE
C
C ASSEMBLE THESE ELEMENT MATRICES TO FORM SYSTEM EQUATIONS
C
CALL ASSMBLE(IE, INTMAT, AKELE, RELE, SYSK, SYSR,
*           NPOIV, MXNEQ, MXELE )
C
500 CONTINUE
C
RETURN
END

```

ศูนย์วิทยทรัพยากร
จุฬาลงกรณ์มหาวิทยาลัย

ประวัติผู้เขียนวิทยานิพนธ์

นายอาชวี ปวีณวัฒน์ เกิดเมื่อวันที่ 24 เดือนกันยายน พุทธศักราช 2521 จังหวัด กรุงเทพมหานคร สำเร็จการศึกษาปริญญาวิศวกรรมศาสตรบัณฑิตจากภาควิชาวิศวกรรมเครื่องกล คณะวิศวกรรมศาสตร์ จุฬาลงกรณ์มหาวิทยาลัย เมื่อปีการศึกษา 2542 เข้าศึกษาต่อในหลักสูตร วิศวกรรมศาสตรมหาบัณฑิต ภาควิชาวิศวกรรมเครื่องกล คณะวิศวกรรมศาสตร์ จุฬาลงกรณ์มหาวิทยาลัย เมื่อปีการศึกษา 2543



ศูนย์วิทยทรัพยากร
จุฬาลงกรณ์มหาวิทยาลัย