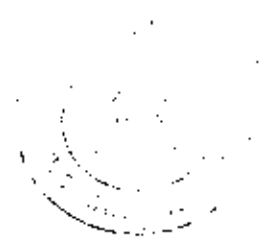


CHAPTER IV

VIBRATIONS AND MODE ANALYSIS



We shall now use the vibration theory to compute the normal frequencies of the system with 5 masses.

Normal frequency calculations for systems with 5 masses

For the system which belongs to the group  $D_{4h}$  in Example 1., we have the following set of Lagrange's equations of motion for the system:

$$m \ddot{x}_{1,3} + k (x_{1,3} - x_0) = 0 \dots\dots\dots(4.1)$$

$$m \ddot{y}_{2,4} + k (y_{2,4} - y_0) = 0 \dots\dots\dots(4.2)$$

$$m \ddot{z}_{1,3} + k_B (z_{1,3} - z_0 \pm 1\theta) = 0 \dots\dots\dots(4.3)$$

$$m \ddot{z}_{2,4} + k_B (z_{2,4} - z_0 \mp 1\phi) = 0 \dots\dots\dots(4.4)$$

$$m \ddot{y}_{1,3} + k_B (y_{1,3} - y_0 \pm 1\psi) = 0 \dots\dots\dots(4.5)$$

$$m \ddot{x}_{2,4} + k_B (x_{2,4} - x_0 \pm 1\psi) = 0, \dots\dots\dots(4.6)$$

$$m \ddot{x}_0 + m(\ddot{x}_1 + \ddot{x}_2 + \ddot{x}_3 + \ddot{x}_4) = 0, \dots\dots\dots(4.6a)$$

where  $k, k_B$  are force constants and  $\ddot{\phantom{x}}$  denotes a second

derivative with respect to time  $t$ .

From (4.1),

$$m \ddot{x}_1 + k (x_1 - x_0) = 0 \dots\dots\dots(4.7)$$

$$m \ddot{x}_3 + k (x_3 - x_0) = 0. \dots\dots\dots(4.8)$$

Subtracting (4.8) from (4.7), we have

$$m(x_1 - x_3)'' + k(x_1 - x_3) = 0 \dots\dots\dots(4.9)$$

Similarly, from (4.2)

$$m(y_2 - y_4)'' + k(y_2 - y_4) = 0 \dots\dots\dots(4.10)$$

$$\text{Let } x_1 = x_{10} \cos \sqrt{\lambda} t$$

$$x_3 = x_{30} \cos \sqrt{\lambda} t$$

where  $x_{10}$  and  $x_{30}$  are amplitudes of the displacement and substituting into (4.9), we have

$$\lambda_1 = \frac{k}{m} \dots\dots\dots(4.11)$$

From (4.1), adding together

$$m(x_1 + x_3)'' + k(x_1 + x_3) - 2k x_0 = 0$$

differentiating two times with respect to  $t$ ,

$$m(x_1 + x_3)'''' + k(x_1 + x_3)'' - 2k \ddot{x}_0 = 0 \dots\dots(4.12)$$

$$\text{Since } M \ddot{x}_0 + m(\ddot{x}_1 + \ddot{x}_2 + \ddot{x}_3 + \ddot{x}_4) = 0,$$

$$\text{hence } \ddot{x}_0 = -\frac{m}{M}(\ddot{x}_1 + \ddot{x}_2 + \ddot{x}_3 + \ddot{x}_4).$$

Setting  $\ddot{x}_2 = \ddot{x}_4 = 0$  and substituting into (4.12) which gives

$$m(x_1 + x_3)'''' + k(x_1 + x_3)'' \left(1 + \frac{2m}{M}\right) = 0, \text{ we obtain}$$

$$\lambda = 0 \text{ and } \lambda_2 = \frac{k}{m} \left(1 + \frac{2m}{M}\right) \dots\dots\dots(4.13)$$

where  $\lambda = 0$  corresponds to the rigid mode motion of the system.

Similarly, from (4.2), we have the similar result

$$\lambda_3 = \frac{k_B}{m} \left(1 + \frac{2m}{M}\right) \dots \dots \dots (4.14)$$

From (4.5) and (4.6), we have

$$m(y_1 - y_3)'' + k_B(y_1 - y_3) - 2lk_B \psi = 0$$

$$m(x_2 - x_4)'' + k_B(x_2 - x_4) + 2lk_B \psi = 0$$

dividing the two equations by  $lk_B$ ,

$$\frac{m}{lk_B} (y_1 - y_3)'' + \frac{1}{l} (y_1 - y_3) - 2\psi = 0$$

$$\frac{m}{lk_B} (x_2 - x_4)'' + \frac{1}{l} (x_2 - x_4) + 2\psi = 0.$$

Let  $\frac{y_1 - y_3}{2l} = \alpha_1$ ,  $\frac{x_2 - x_4}{2l} = \alpha_2$ , therefore the

equations become

$$\frac{2m}{k_B} \ddot{\alpha}_1 + 2\alpha_1 - 2\psi = 0$$

$$\frac{2m}{k_B} \ddot{\alpha}_2 + 2\alpha_2 + 2\psi = 0.$$

$$\text{Let } \psi = \frac{\alpha_1 - \alpha_2}{2},$$

$$\frac{2m}{k_B} \ddot{\alpha}_1 + \alpha_1 + \alpha_2 = 0,$$

$$\frac{2m}{k_B} \ddot{\alpha}_2 + \alpha_1 + \alpha_2 = 0,$$

the determinant of the coefficients is

$$\begin{vmatrix} 1 - \frac{2m\lambda}{k_B} & 1 \\ 1 & 1 - \frac{2m\lambda}{k_B} \end{vmatrix} = 0,$$

the root of the determinant is

$$\lambda_4 = \frac{k_B}{m} \dots \dots \dots (4.15)$$

From (4.3),

$$m(z_1+z_3)'' + k_B (z_1+z_3 - 2z_0) = 0$$

or  $m(z_1+z_3)^{IV} + k_B(z_1+z_3)'' - 2k_B\ddot{z}_0 = 0 \dots \dots \dots (4.16)$

since  $M\ddot{z}_0 + m(\ddot{z}_1 + \ddot{z}_2 + \ddot{z}_3 + \ddot{z}_4) = 0$ ,

substituting  $\ddot{z}_0 = -\frac{m}{M}(\ddot{z}_1 + \ddot{z}_2 + \ddot{z}_3 + \ddot{z}_4)$  into (4.16), and rearranging its terms, we have

$$m(z_1+z_3)^{IV} + k_B \left(1 + \frac{2m}{M}\right) (z_1+z_3)'' + 2k_B \frac{m}{M} (z_2+z_4)'' = 0 \dots \dots \dots (4.17)$$

Similarly, from (4.4), we have

$$m(z_2+z_4)^{IV} + k_B \left(1 + \frac{2m}{M}\right) (z_2+z_4)'' + 2k_B \frac{m}{M} (z_1+z_3)'' = 0. \dots \dots \dots (4.18)$$

Equations (4.17) and (4.18) can be combined together and expressed in the matrix form as

$$m \begin{Bmatrix} z_1 + z_3 \\ z_2 + z_4 \end{Bmatrix}^{IV} + \begin{bmatrix} k_B \left(1 + \frac{2m}{M}\right) & 2k_B \frac{m}{M} \\ 2k_B \frac{m}{M} & k_B \left(1 + \frac{2m}{M}\right) \end{bmatrix} \begin{Bmatrix} z_1 + z_3 \\ z_2 + z_4 \end{Bmatrix}'' = 0$$

There will be a non-trivial solution only if

$$\begin{vmatrix} k_B \left(1 + \frac{2m}{M}\right) - m\lambda & 2k_B \frac{m}{M} \\ 2k_B \frac{m}{M} & k_B \left(1 + \frac{2m}{M}\right) - m\lambda \end{vmatrix} = 0,$$

The roots of this determinant are

$$\lambda_5 = \frac{k_B (M + 4m)}{mM} \dots \dots \dots (4.19)$$

and  $\lambda = \frac{k_B}{m}$  which is the same as  $\lambda_4$ .

From (4.3),

$$m(z_1 + z_3)'' + k_B(z_1 + z_3 - 2z_0) = 0$$

which also yields

$\lambda = \frac{k_B}{m} (1 + \frac{2m}{M})$  which is the same as  $\lambda_3$ . By solving (4.1), and (4.6) simultaneously, we have

$$\lambda_{6,7} = \frac{(k+k_B)(1+\frac{2m}{M}) \pm \sqrt{(k+k_B)^2(1+\frac{2m}{M})^2 - 4kk_B(1+\frac{4m}{M})}}{2m} \dots \dots \dots (4.20)$$

Therefore, we obtain seven normal frequencies

( $\nu_1 = \frac{\lambda_1}{2\pi}$ ) for the system, of which two are doubly degenerate

and five are non-degenerate. **These seven normal frequencies are agreeable with the equation (3.5) in Chapter III.**

For the system which belongs to the group  $D_{2h}$  in

Example 2, we have the following set of Lagrange's equations of motion:

$$m \ddot{x}_{1,3} + k_1(x_{1,3} - x_0) = 0 \dots \dots \dots (4.21)$$

$$m \ddot{y}_{2,4} + k_2(y_{2,4} - y_0) = 0 \dots \dots \dots (4.22)$$

$$m \ddot{z}_{1,3} + k'_1(z_{1,3} - z_0 \pm l_1\theta) = 0 \dots \dots \dots (4.23)$$

$$m \ddot{z}_{2,4} + k'_2(z_{2,4} - z_0 \pm l_2\theta) = 0 \dots \dots \dots (4.24)$$

$$m \ddot{y}_{1,3} + k'_1(y_{1,3} - y_0 \mp l_1\theta) = 0 \dots \dots \dots (4.25)$$

$$m \ddot{x}_{2,4} + k_2' (x_{2,4} - x_0 \pm l_2 \psi) = 0, \dots (4.26)$$

where  $k_1$ ,  $k_2$ ,  $k_1'$  and  $k_2'$  are force constants.

The process used to solve the set of these equations is the same as in the group  $D_{4h}$  above. We obtain the following values of  $\lambda_i$  :

$$\lambda_1 = \frac{k_1}{m} \left( 1 + \frac{2m}{M} \right) \dots (4.27)$$

$$\lambda_2 = \frac{k_2}{m} \left( 1 + \frac{2m}{M} \right) \dots (4.28)$$

$$\lambda_3 = \frac{k_1}{m} \dots (4.29)$$

$$\lambda_4 = \frac{k_2}{m} \dots (4.30)$$

$$\lambda_5 = \frac{k_1'}{m} \left( 1 + \frac{2m}{M} \right) \dots (4.31)$$

$$\lambda_6 = \frac{k_2'}{m} \left( 1 + \frac{2m}{M} \right) \dots (4.32)$$

$$\lambda_{7,8} = \frac{\left(1 + \frac{2m}{M}\right) (k_1' + k_2') \pm \sqrt{\left(1 + \frac{2m}{M}\right)^2 (k_1' + k_2')^2 - 4k_1'k_2' \left(1 + \frac{2m}{M}\right)}}{2m} \dots (4.33)$$

$$\lambda_9 = \frac{k_1' + k_2'}{2m} \dots (4.34)$$

There are 9 vibrational degrees of freedom for this system. We, therefore, have 9 normal frequencies and all of them are non-degenerate.

Schematic representations

We shall present the schematic representations of possible coordinates having the required symmetry as in Figure 10, and 11.

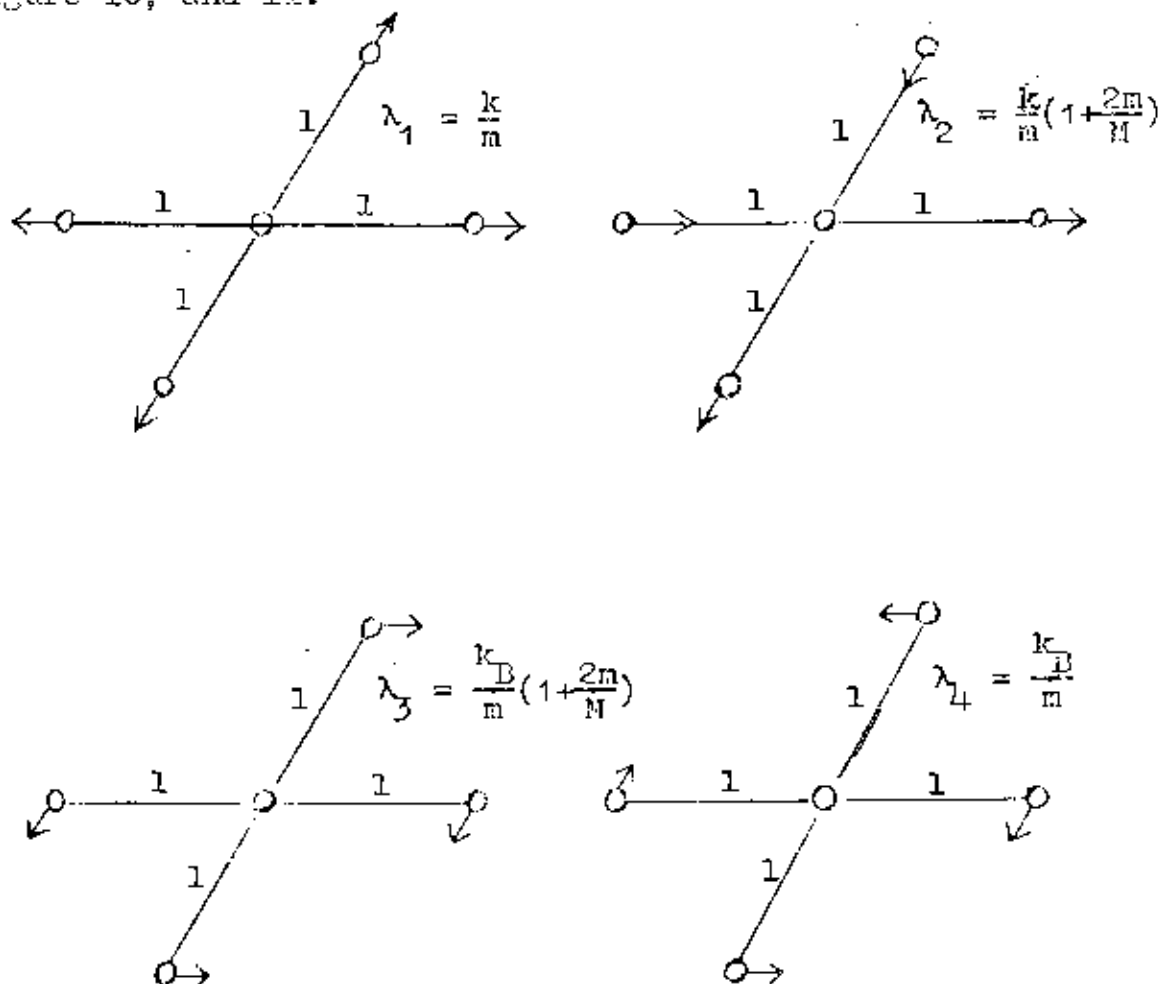


Figure 10(a) Normal modes of vibration of the system belonging to the group  $D_{4h}$ .

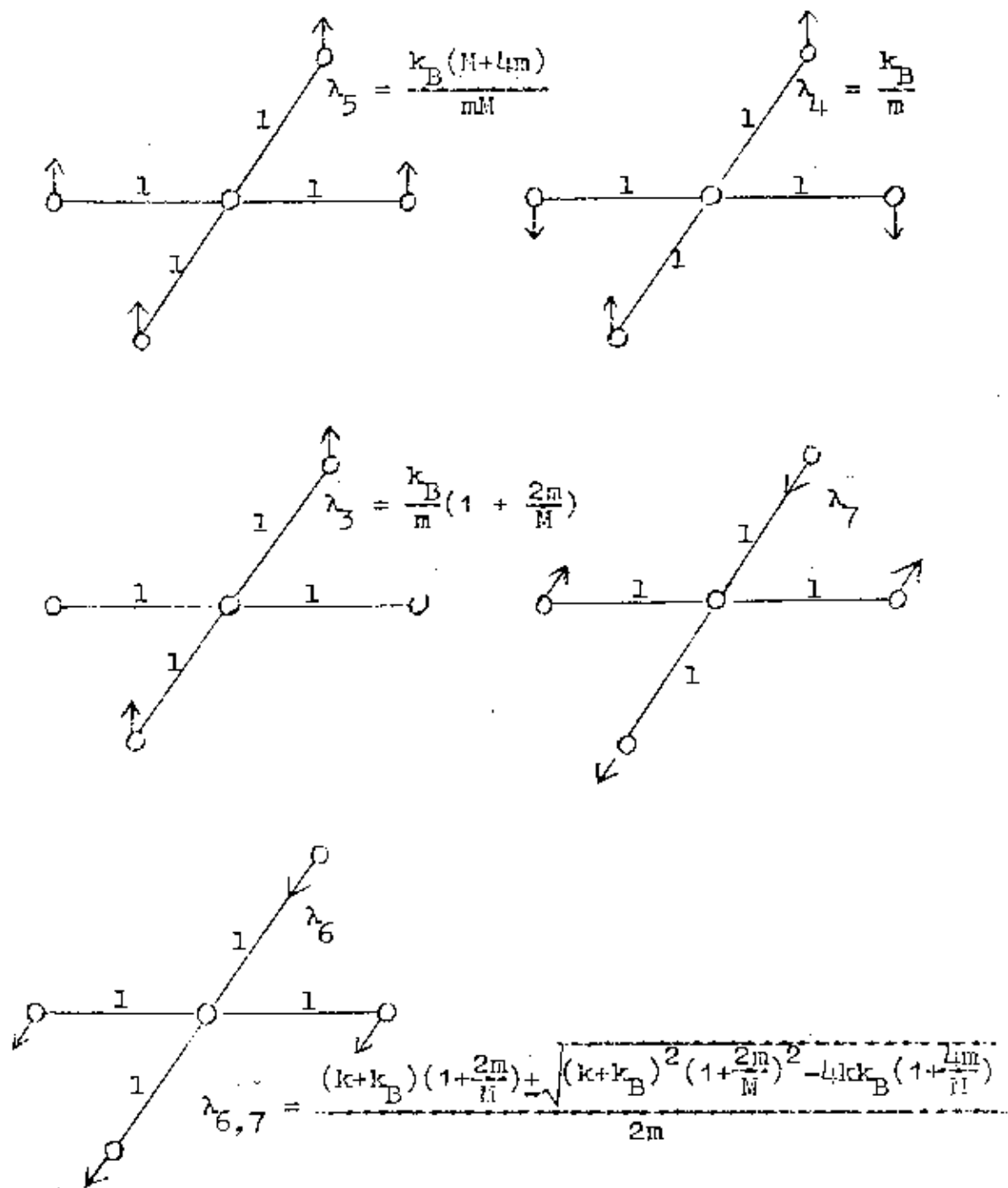


Figure 10(b) Normal modes of vibration of the system belonging to the group  $D_{4h}$ .



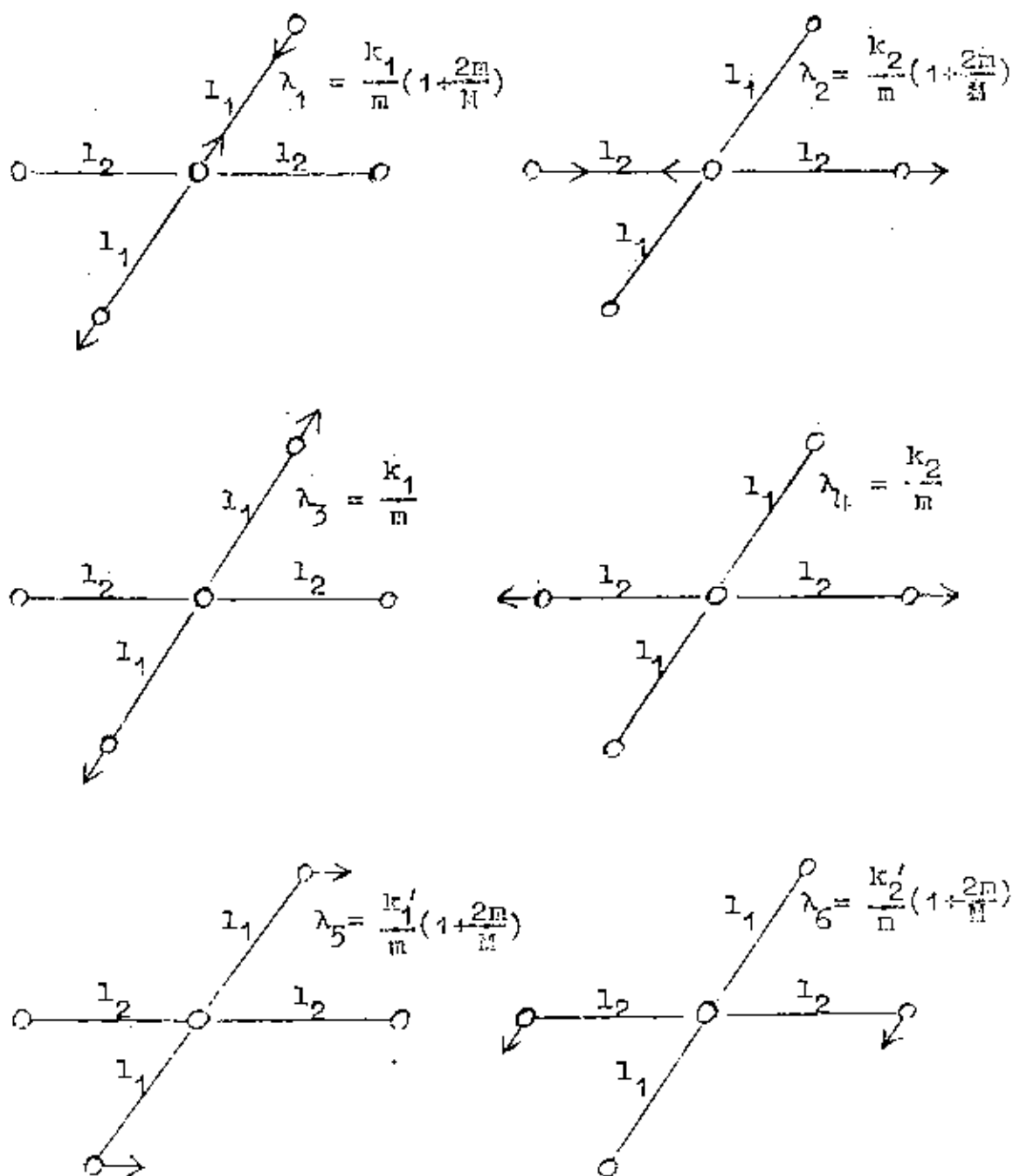
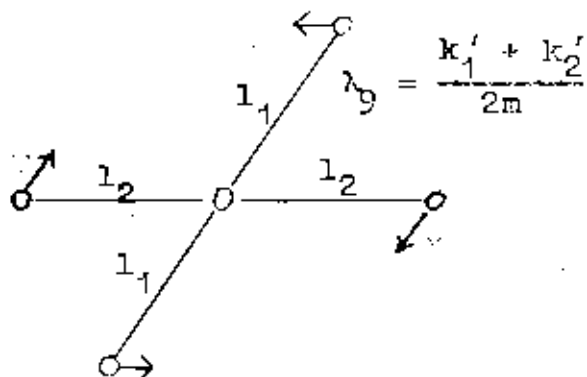
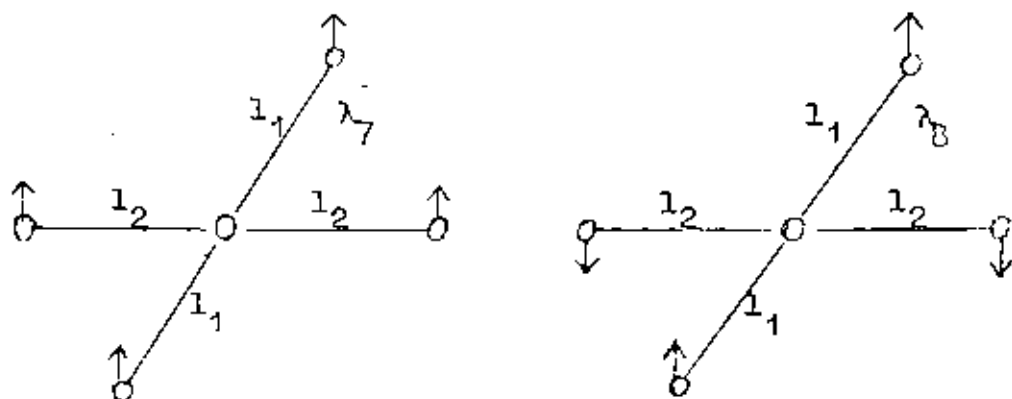


Figure 11(a) Normal modes of vibration of the system belonging to the group  $D_{2h}$ .



$$\lambda_{7,8} = \frac{(1 + \frac{2m}{N})(k_1' + k_2') \pm \sqrt{(1 + \frac{2m}{N})^2 (k_1' + k_2')^2 - 4k_1'k_2'(1 + \frac{4m}{N})}}{2m}$$

Figure 11(b) Normal modes of vibration of the system belonging to the group  $D_{2h}$ .