

CHAPTER IV PVDF/ANTIMONY MODIFIED TITANIUM DIOXIDE (Sb-TiO₂) MEMBRANE FOR PEMFC APPLICATIONS

4.1 Abstract

PVDF/5 mol% Sb-TiO₂ composite film was prepared by solvent casting. By adding 5 mol% Sb-TiO₂ ceramic powder into the polyvinylidene fluoride (PVDF) matrix, the membrane was aimed to increase the hydrophilicity and proton conductivity at high temperature. Antimony modified titanium dioxide (Sb-TiO₂) was prepared via sol-gel method. The anatase structure of calcined Sb-TiO₂ at 500 °C was investigated by XRD. The presence of antimony in titania provides higher porosity and higher specific surface area. The composite films of 10%, 20%, 30%, 40%, and 50% by weight ceramic were fabricated by solvent casting using DMF as a solvent. TGA thermograms indicated the higher thermal stability with higher ceramic content. The microstructure of the composite was observed using SEM. The impedance of composites at different contents of ceramic was measured as a function of frequency using Hewlett-Packard 4194A impedance/gain phase analyzer. With increasing 5 mol%Sb-TiO₂ contents, a percentage of water uptake and the proton conductivity were increased.

Keywords: PVDF/5 mol% Sb-TiO₂ composite; Proton exchange membrane fuel cell

4.2 Introduction

Nowadays, fuel cell is very interesting as power sources for electric vehicles, stationary applications, and portable electronics. Among the several kinds, proton exchange membrane fuel cell (PEMFC) is the most popular choice because of its potential high efficiency, low operating temperature and usage safety. An important part of PEMFC is the polymer membrane which works as an efficient

polymer electrolyte, *i.e.*, conduct by protons whereas hindering electronic transport and penetration of fuel [1, 2].

Generally, perfluorinated membrane, Nafion, is used in practical cells, showing good ionic conductivity and chemical stability. Despite these good qualities, perfluorinated membranes still have few disadvantages, such as high cost, unstable mechanical properties at temperatures above 100 °C, and conductive only when soaked in water, which limits fuel cell operating temperatures to 80 °C. The operation of fuel cells at higher temperature own many advantages such as lower heat exchangers, and easier to integrate with reformers. Consequently, the development of membranes which are mechanically and chemically stable at higher temperatures (above 100 °C) is very interesting for studying fuel cells [3, 4].

Polymer matrix composite providing various advantages such as low cost, lightweight, and easier to manufacture than other materials, is one of the choices to improve high-temperature performance. The membrane is made with organic polymers containing ceramic fillers. Inorganic materials can have high proton conductivity with hydrophilicity, good chemical and thermal stability, high porosity, and high specific surface areas. Organic materials can make membranes elastic and have good mechanical properties with hydrophobicity. Thus, the composite film is applicable at higher temperature and moderate water vapor pressures [5-7].

In 2005, Colomer [15] prepared nanoporous anatase ceramic membranes with a BET surface area of $121 \text{ m}^2/\text{g}$, an average pore diameter of 5.8 nm and a pore volume of 0.236 cm³/g. Proton conductivity of the membranes was measured as a function of temperature and relative humidity, R.H. When anatase membranes are treated at pH 1.5, the proton conductivity increased in the whole range of temperature and R.H. from room temperature to 90 °C. The highest value of proton conductivity was found to be 0.015 S/cm at 90 °C and 81% R.H. The similar values of proton conductivity, lower cost and higher hydrophilicity of these membranes in proton exchange membrane fuel cells (PEMFCs).

In Tanita's work [6], niobium-modified titania and antimony/niobiummodified titania ceramic were prepared via the sol-gel technique. Inorganic membranes were fabricated by using the spin-coating technique using epoxy resin as a binder. The proton conductivity value of TiO₂/epoxy membrane was enhanced by doping niobium and antimony into TiO₂ matrix and all of the nano-composite films present good thermal and mechanical properties.

In this study, the 5 mol% Sb-TiO₂ was prepared based on the sol-gel method. The PVDF/5 mol% Sb-TiO₂ composite films were prepared using solvent casting. Microstructure and distribution of ceramic power were observed by SEM and EDX. Higher proton conductivity and higher a percentage of water uptake were observed in composite films at higher ceramic contents.

4.3 Experiment

4.3.1 Materials

Titanium (IV) butoxide, glacial acetic acid and methyl alcohol were purchased from Italmar. The Poly(vinylidene fluoride) (PVDF) pellets were given by Solvay ([#]1008). *N*,*N*-Dimetyl formamide (DMF) was purchased from Lab Scan. Antimony (V) chloride was purchased from S.M. Chemical.

4.3.2 PVDF Film Preparation

Poly(vinylidene fluoride) pellets manufactured from Solvay Company (Belgium) (Solef 1008) were used. The fabrications of PVDF film was the solution casting which PVDF pellets were dissolved in DMF solution. The viscous solution was then casted on glass substrate. After the solvent evaporation in a vacuum oven at 60°C for 3 hours, the precursor membranes were washed in distilled water and dried in vacuum to assure the elimination of the solvent.

4.3.3 Sol-gel Processing of Antimony-modified Titania ceramics

Titanium (IV) butoxide (Ti $(OC_4H_9)_4$) was dissolved in the mixture between methanol/acetic acid ratio at room temperature with continuous stirring. The ratio of methanol/acetic acid was 1:1. In a different beaker, antimony (V) chloride (SbCl₅) was dissolved in methanol and gradually mixed with TiO₂ sol. After that, the gel was calcined at temperature about 500 °C for 3 hours. Antimony-modified titania particles was grounded into powder. TiO₂ powder was also prepared as a reference. The ceramic powder was characterized using XRD, SEM, and EDX. The surface area and pore size distribution were also measured using Nitrogen sorption.

4.3.4 PVDF/ Antimony-modified Titania composite Preparation

PVDF powder supplied by Solvay (Solef 1008) was dissolved in dimethyl formamide (DMF) at 60°C. For composite preparation, the ratio of polymer and solvent was 1:10 w/v. Proportionate quantity of Antimony-modified Titania ceramics powder was added in the polymer solution. It was homogenized by magnetic stirrer. The solution was then cast on a glass substrate. After that, the solvent was evaporated at 60°C for 3 hour under vacuum. Following this method, the composite films of 10%, 20%, 30%, 40%, and 50% by weight ceramic were fabricated. The precursor membranes were washed with distilled water and dried in vacuum. The dispersion of ceramic particles was observed by using SEM and EDXmapping. The composite membranes were tested in order to evaluate the potential use as electrolyte in PEMFCs at high temperature by using TGA, Impedance spectroscopy and Water uptake. Lloyd Universal Testing machine were carried out to measure the mechanical properties of the thin films.

4.3.5 Characterization

Crystal structure of ceramic was characterized by X-ray diffraction (Rigaku, model Dmax 2002). The specific surface area and the pore size distribution were measured by using Thermo Finnigan, Autosorb-1 from Quantachrome Company. The distribution of ceramic powders in composites was observed using a Hitachi/S-4800 field emission scanning electron microscope and the doped Sb species were identified by LINK ISIS series 300 for Energy dispersive X-ray (EDX) analysis. Thermal stabilities of composite film were investigated by Thermal gravimetric Analyzer, Perkin-Elmer TG-DTA pyres diamond. Mechanical properties of the thin films were investigated by using a Model LRX Lloyd Universal Testing machine following ASTM D882. The water uptake (%W) was measured by soaking the samples in the water. The impedance of the samples was measured by using impedance analyzer (Hewlett Packard., model 4194A) in impedance (Z) mode, with frequency from 1 kHz to 10 MHz.

4.4 Results and Discussion

4.4.1 Antimony Modified Titanium Dioxide (Sb-TiO₂) in Various Amounts of Antimony

4.4.1.1 XRD Analysis of Pure and Sb Doped TiO₂ Particles

The crystal structure of pure and Sb doped TiO_2 particles were examined by XRD. All of the samples were calcined at 500 °C for 3 h in a furnace and the diffractograms shown in Fig.4.1 indicate that all of the samples possess an anatase phase and no peaks of rutile and mixed phases were found.

Sample	Crystal Size (nm)	20 Position of 1 0 1 Peak	d _(h k l) (nm)	Lattice Parameter	
				a (Å)	c (Å)
TiO ₂	14.64568	25.367	0.35083	3.776	9.486
5mol%Sb-TiO ₂	11.50039	25.322	0.351443	3.783	9.497
10mol%Sb-TiO ₂	11.2463	25.325	0.351402	3.7822	9.5023
20mol%Sb-TiO2	11.48518	25.367	0.35083	3.776	9.486

Table 4.1 Summary of physical properties of TiO₂ and Sb doped TiO₂ samples

The anatase peaks were indexed as (101), (004), (200), (105),

(211), (204), (116), (220) and (215) in the order of increasing diffraction angles, indicating a body centered tetragonal crystalline structure of TiO_2 crystal [9]. It also shows that the increase of the full width at half-maximum (FWHM) of the XRD peaks with doping antimony exhibits the decrease of grain size, as reported in Table 4.1.

The grain size of the TiO_2 and $Sb-TiO_2$ powders were calculated using the Scherrer equation [10]. It is worth noting that the crystal size of doped particles decreased by an introduction of Sb dopant into TiO_2 crystal [11].



Figure 4.1 XRD patterns for (a) TiO₂, (b) 5 mol%Sb-TiO₂, (c) 10 mol%Sb-TiO₂, (d) 20 mol%Sb-TiO₂ which all of these were calcined at 500 ° C.

The doping of antimony atoms into the TiO₂ lattice did not give any significant changes in the diffractograms. The lattice parameters a and c, as listed in Table 4.1, were calculated based on Bragg's law (2d sin $\theta = \lambda$) and a formula for a tetragonal system [12],

$$\frac{l}{d^2} = \frac{h^2 + k^2}{a^2} + \frac{l^2}{c^2}$$

There is no considerable difference in the lattice parameters of doped materials, this suggests that the structure of doped TiO_2 samples was not changed or distorted from anatase structure of pure TiO_2 .

4.4.1.2 Surface Area and Pore Size Analysis of TiO₂ and Sb Doped TiO₂ Particles

The results from the surface area, pore size and pore volume measurement of TiO_2 after calcinations at 500 °C were summarized in Table 4.2. The materials present type IV of N₂ adsorption-desorption isotherms with hysteresis loops in Fig. 4.2, clearly indicating the mesoporous nature of TiO_2 and Sb doped TiO_2 samples. The volume adsorbed for all isotherms sharply increased at high relative pressure (P/P₀), representing capillary condensation of nitrogen within the irregular mesopore structure.

Table 4.2 Physicochemical properties of TiO_2 and Sb doped TiO_2 samples calcined at 500 °C

Samples	S _{BET} (m ² g ⁻¹)	D _{Pore} (nm)	V _{Pore} (cc g ⁻¹)
TiO ₂	61.09	7.06	0.1078
5 mol% Sb-TiO ₂	92.9	11.4	0.2647
10 mol% Sb-TiO2	93.48	16.09	0.2956
20 mol% Sb-TiO2	92.34	14.68	0.2655

As shown in Table 4.2, the surface area of Sb doped TiO_2 were higher than that of pure TiO_2 . This increasing was due to the presence of Sb^{5+} on the surface of TiO_2 which inhibits densification and crystalline growth of TiO_2 nanoparticles by providing dissimilar boundaries [13].



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Figure 4.2 N₂ adsorption-desorption isoterms of (a) TiO₂, (b) 5 mol%Sb-TiO₂, (c) 10 mol%Sb-TiO₂, (d) 20 mol%Sb-TiO₂ samples calcined at 500 ° C.

4.4.1.3 SEM/EDX Analysis of TiO₂ and Sb Doped TiO₂ Particles

SEM photographs of particles obtained present spherical morphology of pure and doped TiO_2 nanoparicles and it was not significantly changed according to the introduction of Sb dopant as shown in Fig. 4.3.



Figure 4.3 SEM images of (a) TiO₂, (b) 5 mol%Sb-TiO₂, (c) 10 mol%Sb-TiO₂,
(d) 20 mol%Sb-TiO₂ samples calcined at 500 ° C.

In order to identify the presence of Sb^{5+} ions in the TiO₂ matrix, EDX spectrum was carried out. The EDX spectrum shown in Fig. 4.4 confirmed that most of Sb^{5+} ions incorporated into the framework of TiO₂ and substitute for the Ti⁴⁺ sites. Moreover, the results suggested that Sb was incorporated into the TiO₂ crystal because any peak corresponding to Sb-related compounds was not detected by X-ray diffraction patterns.









Figure 4.4 EDX graphs of (a) TiO_2 , (b) 5 mol%Sb-TiO₂, (c) 10 mol%Sb-TiO₂, (d) 20 mol%Sb-TiO₂ samples calcined at 500 ° C.

4.4.2 <u>PVDF-10%wt of Antimony Modified Titanium Dioxide (Sb-TiO₂)</u> <u>Composite Film at Various Amounts of Antimony</u> *4.4.2.1 SEM/EDX Analysis of PVDF-10%wt of Sb Doped TiO₂ Films* SEM micrograph of the composites containing 10%wt of Sb doped TiO₂ filler in various amounts of Sb which fine powder was dispersed in a PVDF matrix were shown in Figures 4.5.





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Figure 4.5 SEM images of (a) PVDF cast film, (b) PVDF-10%wt of TiO₂, (c) PVDF-10%wt of 5 mol%Sb-TiO₂, (d) PVDF-10%wt of 10 mol%Sb-TiO₂, (e) PVDF-10%wt of 20 mol%Sb-TiO₂.

In addition, EDX analysis was used to observe the distribution and dispersion of ceramic powder in the PVDF matrix. EDX Sb and Timapping photographs show the homogeneous and uniform distribution of Sb-TiO₂ ceramic in PVDF matrix as presented in Fig. 4.6, 4.7, 4.8 and 4.9.



Figure 4.6 (a) SEM image (scale bar = $10 \mu m$), (b) EDX Ti-mapping photograph of PVDF-10%wt of TiO₂.



Figure 4.7 (a) SEM image (scale bar = $10 \mu m$), (b) EDX Ti-mapping photograph, (c) EDX Sb-mapping photograph of PVDF-10%wt of 5 mol%Sb-TiO₂.



Figure 4.8 (a) SEM image (scale bar = $10 \mu m$), (b) EDX Ti-mapping photograph, (c) EDX Sb-mapping photograph of PVDF-10%wt of 10 mol%Sb-TiO₂.



Figure 4.9 (a) SEM image (scale bar = $10 \mu m$), (b) EDX Ti-mapping photograph, (c) EDX Sb-mapping photograph of PVDF-10%wt of 20 mol%Sb-TiO₂.

4.4.2.2 TGA Analysis of PVDF-10%wt of Sb Doped TiO₂ Cast Films

The hydration effect and thermal stability of thin films were also examined using TGA analysis. As shown in Fig.4.10, the mass loss for all of the samples occurs in 2 steps in a wide temperature range from room temperature to 900 °C. It can be observed that the relative mass decayed at temperature below 150 °C and another mass loss is at approximately near 400 °C. The first mass loss indicates the presence of water, while the second one presents the decomposition of PVDF. Moreover, there was no significant shift of TGA thermographs among PVDF/Sb-TiO₂ thin films. Therefore, this suggested that the amounts of Sb dopant does not influence the degradation of thin films.



Figure 4.10 TGA thermograms of PVDF cast film and PVDF-10%wt of Sb doped TiO_2 cast films.

4.4.2.3 Mechanical Properties of PVDF-10%wt of Sb Doped TiO₂ Cast Films

Tensile properties were measured in order to evaluate the stiffness and strength of the thin films. As it can be seen in the Table 4.3, the PVDF/10%wt of Sb doped TiO_2 cast films have Young's Modulus better than that of PVDF film. This may be contributed the high modulus of ceramic. On the other hand, the percentage strain at break and the stress at break of PVDF film are better than those of composite films because the chain flexibility of the polymer in composite was restricted [14] and the interfacial interaction between polymer and ceramic was weak.

	Young's	Stress at	Percentage
Samples	Modulus	Break (MPa)	Strain at Break
	(MPa)		
PVDF Cast Film	272.42 ± 2.45	24.66 ± 3.38	17.00 ± 1.26
PVDF/10%wt of TiO ₂	395.26±3.58	16.59 ± 2.41	13.58 ± 2.55
PVDF/10%wt of 5 mol%Sb-TiO ₂	432.02 ± 3.35	17.17 ± 3.78	12.75 ± 3.05
PVDF/10%wt of 10 mol%Sb-TiO ₂	383.19±4.14	16.80 ± 4.56	13.08 ± 2.61
PVDF/10%wt of 20 mol%Sb-TiO ₂	408.32 ± 2.96	16.73 ± 2.74	11.87 ± 2.84

Table 4.3 Mechanical properties of PVDF cast film and PVDF/10%wt of Sb dopedTiO2 cast films

4.4.2.4 Water Uptake Testing of PVDF-10%wt of Sb Doped TiO₂ Cast Films

The results of water uptake testing at room temperature exhibit that composite films have higher percentage of water uptake than PVDF film because of the hydrophilicity of the ceramics and the PVDF/Sb doped TiO₂ films possess higher percentage of water uptake than PVDF/TiO₂ film, as shown in Table 4.4. This increase may be due to the higher specific surface areas of doped TiO₂ ceramics than pure TiO₂ ceramics, according to the results from surface area measurement.

Table 4.4 Water uptake of PVDF cast film and PVDF/10%wt of Sb doped TiO_2 cast films

Samples	Percentage of Water Uptake
PVDF Cast Film	4.66
PVDF/10%wt of TiO ₂	8.74
PVDF/10%wt of 5 mol%Sb-TiO ₂	11.20
PVDF/10%wt of 10 mol%Sb-TiO ₂	10.60
PVDF/10%wt of 20 mol%Sb-TiO ₂	11.68

4.4.2.5 Proton Conductivity Measurement of PVDF-10%wt of Sb Doped TiO₂ Cast Films

The results of resistance and proton conductivity of all membranes at room temperature after soaking in 6M H_2SO_4 aqueous solution were demonstrated in Table 4.5. The proton conductivity value of PVDF/Sb doped TiO₂ films were enhanced by doping antimony into TiO₂ matrix because the doped TiO₂ showed higher specific surface areas, leading to obtain higher water adsorption ability, and the porous surface condition of the TiO₂ ceramic particles was improved by doping antimony. High surface areas and the acidic porous surface condition of the ceramic particles cause easier proton hoping, resulting in an increase of proton conductivity value.

Table 4.5	Resistance and proton conductivity at 25 ° C of PVDF of	cast film	and
PVDF/10%	6wt of Sb doped TiO ₂ cast films		

Samples	Resistance	Proton Conductivity
	(Ohms)	(S/cm)
PVDF Cast Film	1183.74	9.04×10 ⁻⁶
PVDF/10%wt of TiO ₂	813.89	1.92×10 ⁻⁵
PVDF/10%wt of 5 mol%Sb-TiO ₂	412.56	3.78×10 ⁻⁵
PVDF/10%wt of 10 mol%Sb-TiO ₂	435.88	3.67×10 ⁻⁵
PVDF/10%wt of 20 mol%Sb-TiO ₂	421.65	3.77×10 ⁻⁵

4.4.3 PVDF-5 mol% Antimony Modified Titanium Dioxide (5 mol%Sb-TiO₂) Composite Film in Various Amounts of Ceramic Powder 4.4.3.1 SEM/EDX Analysis of PVDF-5 mol%Sb Doped TiO₂ Thin Films

SEM micrograph of the composites containing 10, 20, 30, 40, and 50 wt% ceramic filler which fine powder was dispersed in a PVDF matrix were shown in Figures 4.11. The composites displayed the microstructure of larger agglomeration in PVDF matrix when amount of ceramic increased. However, at higher ceramic content, the flexibilities of composite films were reduced due to the high stiffness of ceramic powder.





Figure 4.11 SEM images of (a) PVDF cast film, (b) PVDF-10%wt of 5 mol%Sb-TiO₂, (c) PVDF-20%wt of 5 mol%Sb-TiO₂, (d) PVDF-30%wt of 5 mol%Sb-TiO₂, (e) PVDF-40%wt of 5 mol%Sb-TiO₂, (f) PVDF-50%wt of 5 mol%Sb-TiO₂.

In addition, EDX analysis was used to observe the distribution and dispersion of ceramic powder in the PVDF matrix. EDX Sb and Timapping photographs show the homogeneous and uniform distribution of Sb-TiO₂ ceramic in PVDF matrix as presented in Fig. 4.12, 4.13, 4.14, 4.15 and 4.16.



Figure 4.12 (a) SEM image (scale bar = $10 \mu m$), (b) EDX Ti-mapping photograph, (c) EDX Sb-mapping photograph of PVDF-10%wt of 5 mol%Sb-TiO₂.



Figure 4.13 (a) SEM image (scale bar = $10 \mu m$), (b) EDX Ti-mapping photograph, (c) EDX Sb-mapping photograph of PVDF-20%wt of 5 mol%Sb-TiO₂.

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Figure 4.14 (a) SEM image (scale bar = $10 \mu m$), (b) EDX Ti-mapping photograph, (c) EDX Sb-mapping photograph of PVDF-30%wt of 5 mol%Sb-TiO₂.



Figure 4.15 (a) SEM image (scale bar = $10 \mu m$), (b) EDX Ti-mapping photograph, (c) EDX Sb-mapping photograph of PVDF-40%wt of 5 mol%Sb-TiO₂.



Figure 4.16 (a) SEM image (scale bar = $10 \mu m$), (b) EDX Ti-mapping photograph, (c) EDX Sb-mapping photograph of PVDF-50%wt of 5 mol%Sb-TiO₂.

4.4.3.2 TGA Analysis of PVDF-5 mol%Sb Doped TiO₂ Thin Films

The graphic of weight loss versus temperature for PVDF and PVDF/5 mol%Sb-TiO₂ composite as shown in Figure 4.17. It can be observed that the relative mass decayed at temperature below 150 ° C and another mass loss is at approximately near 400 ° C. The first mass loss indicates the presence of water, while the second one presents the decomposition of PVDF. TGA thermograms showed that the incorporation of 5mol%Sb-TiO₂ ceramic in the PVDF films enhances the higher residue of composite when compared to the pure PVDF.



Figure 4.17 TGA thermograms of PVDF cast film and PVDF-5 mol%Sb doped TiO_2 cast films.

4.4.3.3 Mechanical Properties of PVDF/5 mol%Sb-TiO₂ Thin Films

Tensile properties were measured in order to evaluate the stiffness and strength of the thin films. With increasing 5 mol%Sb-TiO₂ contents, the Young's Modulus of composite films increased while the percentage strain at break and the stress at break decreased as it can be seen in the Table 4.6. This may be contributed the high modulus of ceramic and the poor interaction between polymer and ceramic.

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	Young's	Stress at	Percentage
Samples	Modulus	Break (MPa)	Strain at Break
	(MPa)		
PVDF Cast Film	272.42 ± 2.45	24.66 ± 3.38	17.00 ± 1.26
PVDF/10%wt of 5 mol%Sb-TiO ₂	432.02 ± 3.35	17.17±3.78	12.75 ± 3.05
PVDF/20%wt of 5 mol%Sb-TiO ₂	463.40±3.96	8.10±1.58	9.66±2.49
PVDF/30%wt of 5 mol%Sb-TiO ₂	556.78 ± 2.07	7.03±1.33	5.26±1.87
PVDF/40%wt of 5 mol%Sb-TiO ₂	633.13±3.19	5.90 ± 1.43	3.04±0.91
PVDF/50%wt of 5 mol%Sb-TiO ₂	729.62 ± 2.85	4.87±1.22	1.63 ± 0.45

Table 4.6 Mechanical properties of PVDF cast film and PVDF/5 mol%Sb-TiO₂ thin films

4.4.3.4 Water Uptake Testing of PVDF-5 mol%Sb-TiO₂ Thin Films

The results of water uptake testing at room temperature exhibit that percentage of water uptake of composite films increased with the 5 mol%Sb-TiO₂ contents because of the hydrophilicity of the ceramics, as shown in Table 4.7. This increase may be due to the high specific surface areas of 5 mol%Sb-TiO₂ ceramics, according to the results from surface area measurement.

Table 4.7 Water uptake of PVDF cast film and PVDF/5 mol%Sb-TiO₂ thin films

Samples	Percentage of Water Uptake	
PVDF Cast Film	4.66	
PVDF/10%wt of 5 mol%Sb-TiO2	11.20	
PVDF/20%wt of 5 mol%Sb-TiO2	11.91	
PVDF/30%wt of 5 mol%Sb-TiO2	13.06	
PVDF/40%wt of 5 mol%Sb-TiO ₂	15.32	
PVDF/50%wt of 5 mol%Sb-TiO2	17.63	

4.4.3.5 Proton Conductivity Measurement of PVDF-5 mol%Sb Doped TiO₂ Thin Films

The results of resistance and proton conductivity of all membranes at room temperature after soaking in $6M H_2SO_4$ aqueous solution for 24 hours were demonstrated in Table 4.8. The proton conductivity value of composite membranes were enhanced by increasing 5 mol%Sb-TiO₂ particles because this ceramic showed higher specific surface areas, leading to obtain higher water adsorption ability. High surface areas and the acidic porous surface condition of this particles cause easier proton hoping, resulting in an increase of proton conductivity value.

Table 4.8 Resistance and conductivity at 25 °C of PVDF cast film and PVDF/5 mol%Sb-TiO₂ thin films

Samples	Resistance	Proton Conductivity
	(Ohms)	(S/cm)
PVDF Cast Film	1183.74	9.04×10 ⁻⁶
PVDF/10%wt of 5 mol%Sb-TiO ₂	412.56	3.78×10 ⁻⁵
PVDF/20%wt of 5 mol%Sb-TiO ₂	115.67	2.20×10 ⁻⁴
PVDF/30%wt of 5 mol%Sb-TiO ₂	54.17	6.15×10 ⁻⁴
PVDF/40%wt of 5 mol%Sb-TiO ₂	20.41	1.63×10 ⁻³
PVDF/50%wt of 5 mol%Sb-TiO ₂	0.86	4.63×10 ⁻²

From all of these results, the optimum %wt of ceramic in PVDF matrix should be 40%wt due to the high percentage of water uptake, high proton conductivity and good flexibility of this film. The temperature dependence of proton conductivity of PVDF film and PVDF/40%wt of 5 mol%Sb-TiO₂ composite were investigated from -40 °C to 140 °C in Figure 4.18. From these graphs, it should be observed that the proton conductivity of PVDF composite increased rapidly (~ 10^{-4}

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S/cm to ~ 10^{-1} S/cm) in the long range of temperature (-40 °C to 90 °C) before decreased rapidly (~ 10^{-1} S/cm to ~ 5×10^{-3} S/cm) in the short range of temperature (90 °C to 140 °C). The behavior of conductivity decreasing above 100 °C suggests the higher dehydration of the membrane with higher temperature. However, the composite film can keep the proton better than pure PVDF film due to the pore structure of ceramic powder. At 90 °C, the proton conductivity for the PVDF/40%wt of 5 mol%Sb-TiO₂ composite film is 0.0856 S/cm, which is the maximum conductivity value.



Figure 4.18 The temperature dependence of proton conductivity of PVDF film and PVDF/40%wt of 5 mol%Sb-TiO₂ films.

4.5 Conclusion

The PVDF/5 mol% Sb-TiO₂ composites were successfully fabricated. By doping Sb in TiO₂, the pore structure of ceramic was improved. The high contents of 5 mol% Sb-TiO₂ in the composite show enhancement of a percentage of water uptake

and proton conductivity compared to pure PVDF film. However, more agglomeration of ceramic powder were found in composites at higher 5 mol% Sb- TiO_2 content which made them opaque, stiff and easy to break. The optimum % wt of ceramic in PVDF composite is 40 % wt due to the good flexible film and 3 orders of magnitude higher than the pure PVDF film.

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4.7 References

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