## CHAPTER VI

## RESULTS

### 6.1 Results

### 6.1.1 The result of mixing the scrap and chemical composition received

According to implementation the plan in Chapter 4 during 2 January 2002 to 15 February 2003, the result of collecting the data from the record report can be sorted out into the heat day and month report. For the heat report, the example of mixing scrap result following 2-basket pattern can be shown in Table 6.1

Table 6.1 The example of mixing the scrap following 2-basket pattern in each heat to producing the molten steel MScode00001

| Scrap type | Basket 1 |  | Basket 2 |  | Total |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | (tons) | $m 3$ | (tons) | $m 3$ | (tons) | $m 3$ |
| S183 | 17.00 | 39.38 | 17.00 | 39.38 | 34.00 | 78.75 |
| S187 | 7.00 | 16.25 | 0.00 | 0.00 | 7.00 | 16.25 |
| S400 | 5.00 | 8.13 | 3.00 | 4.88 | 8.00 | 13.00 |
| S406 | 1.00 | 0.75 | 0.00 | 0.00 | 1.00 | 0.75 |
| S517 | 35.00 | 31.50 | 30.00 | 27.00 | 65.00 | 58.50 |
| S900 | 0.00 | 0.00 | 3.00 | 2.88 | 3.00 | 2.88 |
| S922 | 1.00 | 0.63 | 0.00 | 0.00 | 1.00 | 0.63 |
| S923 | 2.00 | 1.25 | 0.00 | 0.00 | 2.00 | 1.25 |
| F111 | 0.500 | 0.50 | 0.000 | 0.00 | 0.50 | 0.50 |
| I116 | 20 | 6.06 | 10 | 3.03 | 30.00 | 9.09 |
| Total | 88.50 | 104.44 | 63.00 | 77.16 | 151.50 | 181.59 |
| Density | 0.847412136 | 0.816526815 | 0.834289343 |  |  |  |

As can be seen in Table 6.1, there are mixing the scrap into 2 basket and there 9 types of scrap that are re-arranged from the original type to convenient for mixing the
scrap and receiving the chemical composition precision. According to mixing the scrap from this pattern in each heat, the density result of each heat is approximately 0.83 $t o n / \mathrm{m}^{3}$. At this density, melting the scraps is saved the energy as shown in Chapter 4. And then mixing the scrap from this patter can receive the chemical composition in Table 6.2

Table 6.2 The example chemical composition received from melting scrap 2-basket pattern in each heat

| Metallic Input |  | Input Ratio | c | P | S | Mn | Si | Weight |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| type |  | \% | \% | \% | \% | \% | \% | (tons) |
| S183 |  | 22.52 | 0.15 | 0.01 | 0.02 | 0.3 | 0.1 | 34.00 |
| S187 |  | 4.64 | 0.25 | 0.03 | 0.07 | 0.3 | 0.2 | 7.00 |
| S400 |  | 5.30 | 0.25 | 0.03 | 0.09 | 0.3 | 0.15 | 8.00 |
| S406 |  | 0.66 | 0.05 | 0.01 | 0.02 | 0.3 | 0.2 | 1.00 |
| S517 |  | 43.05 | 0.15 | 0.025 | 0.04 | 0.4 | 0.1 | 65.00 |
| S900 |  | 1.99 | 0.04 | 0.02 | 0.02 | 0.3 | 0.15 | 3.00 |
| S922 |  | 0.66 | 0.04 | 0.02 | 0.02 | 0.4 | 0.1 | 1.00 |
| S923 |  | $1.32$ | 0.04 | 0.02 | 0.02 | 0.3 | 0.1 | 2.00 |
| 1116 |  | 19.87 | 3.300 | 0.150 | 0.050 | 1.000 | 1.250 | 30.00 |
| Scrap Mix | ratio | 100.00 | 0.78 | 0.05 | 0.041 | 0.48 | 0.337 | 151.00 |
|  | (tons) | 151.00 | 1.18 | 0.07 | 0.06 | 0.73 | 0.51 |  |

According to Table 6.2, the chemical composition received from melting the scrap mix following the 2 -basket pattern are percent of carbon approximately 0.78 percent , percent of Phosphorous approximately 0.05 percent, percent of Sulpher about 0.04 percent, percent of Manganese around 0.48 percent, and percent of Silicon roughly 0.34 percent.

After mixing the scrap following this pattern, we can shown the example quantity of utilizing of the scraps each day in Table 6.3

Table 6.3 the example quantity of scrap mixing each day.

| $\begin{gathered} \text { Scrap } \\ \text { type } \end{gathered}$ | Bulk density | Scrap Mix |  |  |  |  |  |  |  | Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | (tons/m ${ }^{3}$ ) | 1st <br> heat | 2nd <br> heat | 3rd heat | 4th <br> heat | 5th <br> heat | $\begin{aligned} & \text { 6th } \\ & \text { heat } \end{aligned}$ | $\begin{aligned} & \text { 7th } \\ & \text { heat } \end{aligned}$ | $\begin{aligned} & \text { 8th } \\ & \text { heat } \end{aligned}$ |  |
| S183 | 0.432 | 34.00 | 34.05 | 34.02 | 34.01 | 34.00 | 34.02 | 33.98 | 34.02 | 272.10 |
| S187 | 0.431 | 7.00 | 7.02 | 7.03 | 7.00 | 6.98 | 7.00 | 7.03 | 6.95 | 56.01 |
| S400 | 0.615 | 8.00 | 8.03 | 8.05 | 7.95 | 7.98 | 7.98 | 8.02 | 8.01 | 64.02 |
| S406 | 1.333 | 1.00 | 1.02 | 1.03 | 1.02 | 1.00 | 0.98 | 0.95 | 1.02 | 8.02 |
| S517 | 1.111 | 65.00 | 64.80 | 64.90 | 65.10 | 65.20 | 64.80 | 65.10 | 65.10 | 520.00 |
| S900 | 1.043 | 3.00 | 2.95 | 3.02 | 3.02 | 2.98 | 3.02 | 3.02 | 3.00 | 24.01 |
| S922 | 1.600 | 1.00 | 0.95 | 0.95 | 1.00 | 1.03 | 1.02 | 1.02 | 1.04 | 8.01 |
| S923 | 1.600 | 2.00 | 2.02 | 2.02 | 1.98 | 2.03 | 1.95 | 2.05 | 1.98 | 16.03 |
| F111 | 1.000 | 0.50 | 0.50 | 0.50 | 0.50 | 0.50 | 0.50 | 0.50 | 0.50 | 4.00 |
| 1116 | 3.300 | 30.00 | 30.00 | 30.00 | 30.00 | 30.00 | 30.00 | 30.00 | 30.00 | 240.00 |
| Total(tons) |  | 151.50 | 151.34 | 151.52 | 151.58 | 151.70 | 151.27 | 151.67 | 151.62 | 1212.20 |
| Volume (m3) |  | 181.59 | 181.57 | 181.72 | 181.65 | 181.71 | 181.41 | 181.76 | 181.66 | 1453.07 |
| Avg. Density |  | 0.83 | 0.83 | 0.83 | 0.83 | 0.83 | 0.83 | 0.83 | 0.83 | 0.83 |

According to Table 6.3, this table is the example of mixing the scrap in each day by separating into 8 heats for each furnace in the work-day and the company has 2 Electric arc furnaces so the company can run 16 heats per day in the work-day. If it is the holiday (Saturday, Sunday, and so on), the company works 24 hour per day. For these days, the company can run melting the scrap about 19 heats per EAF furnace. So the total heat that the company can run in the holiday is about 38 heats per day.

The example chemical receiving melting the scrap in that day, can be shown in
Table 6.4

Table 6.4 The example chemical composition received from melting scrap 2-basket pattern in each day

| Heat No | $c$ |  | $p$ |  | $S$ |  | $M n$ |  | $S i$ |  |
| :---: | :---: | :--- | :---: | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  | (tons) | $\%$ | (tons) | $\%$ | (tons) | $\%$ | (tons) | $\%$ | (tons) | $\%$ |
| 1st heat | 1.179 | 0.778 | 0.070 | 0.046 | 0.061 | 0.040 | 0.729 | 0.481 | 0.510 | 0.336 |
| 2nd heat | 1.179 | 0.777 | 0.070 | 0.046 | 0.061 | 0.040 | 0.728 | 0.480 | 0.509 | 0.336 |
| 3rd heat | 1.179 | 0.777 | 0.070 | 0.046 | 0.061 | 0.040 | 0.729 | 0.480 | 0.510 | 0.336 |
| 4th heat | 1.179 | 0.778 | 0.070 | 0.046 | 0.061 | 0.040 | 0.729 | 0.481 | 0.510 | 0.336 |
| 5th heat | 1.179 | 0.778 | 0.070 | 0.047 | 0.061 | 0.040 | 0.730 | 0.481 | 0.510 | 0.336 |
| 6th heat | 1.179 | 0.777 | 0.070 | 0.046 | 0.061 | 0.040 | 0.728 | 0.480 | 0.509 | 0.336 |
| 7th heat | 1.179 | 0.778 | 0.071 | 0.046 | 0.061 | 0.040 | 0.730 | 0.481 | 0.510 | 0.336 |
| 8th heat | 1.179 | 0.778 | 0.070 | 0.046 | 0.061 | 0.040 | 0.730 | 0.481 | 0.510 | 0.336 |
| total | 9.431 | 0.778 | 0.564 | 0.046 | 0.490 | 0.040 | 5.833 | 0.481 | 4.076 | 0.336 |

According to Table 6.4, in this example day, the chemical composition that the company receives are carbon 9.42 tons ( $\sim 0.777-0.778$ percent), phosphorous 0.564 tons ( $\sim 0.46$ percent), Sulfur 0.49 tons ( $\sim 0.04$ percent), Manganese 5.8 tons ( $\sim 0.48$ percent) and Silicon 4.076 tons ( $\sim 0.336$ tons). It shown the chemical compositions received from mixing this scrap are rather constant so it is easy to adjust the chemical composition to be the specification required.

After seeing the example of mixing the scrap and the example result of chemical composition received, the next data demonstrated is the quantity of utilizing the scrap and the result of chemical composition following this pattern in January and February in the electric arc furnace 1 (EAF 1). It is shown in as shown in Table 6.5-6.8

Table 6.5 The production report of EAF1 in (2-31 January, 2003)
Raw Material Report Production Date 1-31 January 2002 EAF 1

| Date | S183 | S187 | S400 | S406 | S517 | S900 | S922 | S923 | F111 | 1116 | Total | Volume | Density | Production | Yield | Pro.Time | $T-T-T$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | (tons) | (tons) | (tons) | (tons) | (tons) | (tons) | (tons) | (tons) | (tons) | (tons) | (tons) | m3 | ton/m3 | (tons) | \% | (mins/day)) | (mins) |
| 2/1/02 | 272.10 | 56.01 | 64.02 | 8.02 | 520.00 | 24.01 | 8.01 | 16.03 | 4.00 | 240.00 | 1212.20 | 1453.07 | 0.83 | 1012.19 | 83.50 | 594.8 | 74.35 |
| 3/1/02 | 272.10 | 56.01 | 64.02 | 8.02 | 520.02 | 24.01 | 8.01 | 16.02 | 4.00 | 240.03 | 1212.24 | 1453.09 | 0.83 | 1012.46 | 83.52 | 594.64 | 74.33 |
| 4/1/02 | 646.24 | 133.02 | 152.05 | 19.05 | 1235.00 | 57.02 | 19.02 | 38.07 | 9.50 | 570.00 | 2878.98 | 3451.04 | 0.83 | 2425.54 | 84.25 | 1412.27 | 74.33 |
| 5/1/02 | 646.24 | 133.02 | 152.05 | 19.05 | 1235.05 | 57.02 | 19.02 | 38.05 | 9.50 | 570.07 | 2879.07 | 3451.09 | 0.83 | 2424.18 | 84.20 | 1412.08 | 74.32 |
| 6/1/02 | 272.12 | 56.02 | 64.03 | 8.02 | 520.03 | 24.02 | 8.02 | 16.02 | 4.00 | 240.02 | 1212.30 | 1453.20 | 0.83 | 1021.37 | 84.25 | 594.8 | 74.35 |
| 7/1/02 | 272.15 | 56.02 | 64.02 | 8.01 | 520.01 | 24.01 | 8.01 | 16.03 | 4.00 | 240.03 | 1212.29 | 1453.22 | 0.83 | 1020.75 | 84.20 | 594.8 | 74.35 |
| 8/1/02 | 272.10 | 56.01 | 64.03 | 8.00 | 520.00 | 24.02 | 8.02 | 16.03 | 4.00 | 240.02 | 1212.23 | 1453.09 | 0.83 | 1029.06 | 84.89 | 594.72 | 74.34 |
| 9/1/02 | 272.10 | 56.03 | 64.02 | 8.02 | 520.02 | 24.01 | 8.01 | 16.02 | 4.00 | 239.95 | 1212.18 | 1453.11 | 0.83 | 1029.14 | 84.90 | 594.8 | 74.35 |
| 10/1/02 | 272.12 | 56.03 | 64.02 | 8.03 | 520.03 | 24.02 | 8.02 | 16.00 | 4.00 | 240.02 | 1212.29 | 1453.20 | 0.83 | 1030.69 | 85.02 | 59¢. 56 | 74.32 |
| 11/1/02 | 646.24 | 133.07 | 152.05 | 19.05 | 1235.05 | 57.02 | 19.02 | 38.05 | 9.50 | 569.88 | 2878.93 | 3451.14 | 0.83 | 2447.38 | 85.01 | 1412.27 | 74.33 |
| 12/1/02 | 646.29 | 133.07 | 152.05 | 19.07 | 1235.07 | 57.05 | 19.05 | 38.00 | 9.50 | 570.05 | 2879.19 | 3451.35 | 0.83 | 2447.31 | 85.00 | 1412.27 | 74.33 |
| 13/1/02 | 272.10 | 56.01 | 64.02 | 8.01 | 520.03 | 24.02 | 8.01 | 16.01 | 4.00 | 240.03 | 1212.24 | 1453.10 | 0.83 | 1030.65 | 85.02 | 594.56 | 74.32 |

Table 6.5 The production report of EAF1 in (2-31 January, 2003) (Cont.)
Raw Material Report Production Date 1-31 January 2002 EAF 1

| Date | S183 | S187 | S400 | S406 | S517 | S900 | S922 | 5923 | F111 | 1116 | Total | Volume | Density | Production | Yield | Pro. Time | T-T-T |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | (tons) | (tons) | (tons) | (tons) | (tons) | (tons) | (tons) | (tons) | (tons) | (tons) | (tons) | m3 | ton/m3 | (tons) | \% | (mins/day)) | (mins) |
| 14/1/02 | 272.12 | 56.02 | 64.03 | 8.02 | 520.01 | 24.00 | 8.02 | 16.00 | 4.00 | 240.03 | 1212.25 | 1453.15 | 0.83 | 1030.53 | 85.01 | 594.4 | 74.3 |
| 15/1/02 | 272.13 | 56.02 | 64.01 | 8.02 | 520.00 | 24.01 | 8.00 | 16.02 | 4.00 | 240.00 | 1212.21 | 1453.13 | 0.83 | 1030.74 | 85.03 | 594.4 | 74.3 |
| 16/1/02 | 272.13 | 56.02 | 64.02 | 8.01 | 520.00 | 24.02 | 8.01 | 16.01 | 4.00 | 240.00 | 1212.22 | 1453.15 | 0.83 | 1030.63 | 85.02 | 594.48 | 74.31 |
| 17/1/02 | 272.12 | 56.01 | 64.03 | 8.01 | 520.05 | 24.03 | 8.02 | 16.01 | 4.00 | 240.05 | 1212.33 | 1453.20 | 0.83 | 1029.87 | 84.95 | 594.56 | 74.32 |
| 18/1/02 | 646.31 | 133.05 | 152.05 | 19.02 | 1235.00 | 57.05 | 19.02 | 38.02 | 9.50 | 570.00 | 2879.02 | 3451.24 | 0.83 | 2447.74 | 85.02 | 1411.89 | 74.31 |
| 19/1/02 | 646.29 | 133.05 | 152.04 | 19.05 | 1235.02 | 57.05 | 19.00 | 38.05 | 9.45 | 570.02 | 2879.02 | 3451.17 | 0.83 | 2447.45 | 85.01 | 1411.7 | 74.3 |
| 20/1/02 | 272.12 | 56.01 | 64.01 | 8.01 | 520.02 | 24.02 | 8.02 | 16.02 | 4.00 | 240.03 | 1212.26 | 1453.13 | 0.83 | 1030.78 | 85.03 | 594.4 | 74.3 |
| 21/1/02 | 272.12 | 56.01 | 64.01 | 8.02 | 520.02 | 24.01 | 8.01 | 16.00 | 4.00 | 240.00 | 1212.20 | 1453.10 | 0.83 | 1030.85 | 85.04 | 594.32 | 74.29 |
| 22/1/02 | 272.10 | 56.02 | 64.00 | 8.01 | 520.03 | 24.03 | 8.00 | 16.02 | 4.00 | 240.00 | 1212.21 | 1453.09 | 0.83 | 1030.62 | 85.02 | 594.32 | 74.29 |
| 23/1/02 | 272.09 | 56.01 | 64.02 | 8.00 | 520.04 | 24.02 | 8.00 | 16.03 | 4.00 | 240.02 | 1212.23 | 1453.08 | 0.83 | 1030.76 | 85.03 | 594.32 | 74.29 |
| 24/1/02 | 272.08 | 56.01 | 64.01 | 8.01 | 520.00 | 24.02 | 8.02 | 16.02 | 4.00 | 240.03 | 1212.20 | 1453.02 | 0.83 | 1030.85 | 85.04 | 594.24 | 74.28 |
| 25/1/02 | 646.21 | 133.02 | 152.05 | 19:00 | 1235.10 | 57.05 | 19.00 | 38.07 | 9.50 | 570.05 | 2879.05 | 3451.06 | 0.83 | 2447.77 | 85.02 | 1411.51 | 74.29 |

Table 6.5 The production report of EAF1 in (2-31 January, 2003) (Cont.)


Table 6.6 The production report of EAF1 in (1-15 February,2003)


Table 6.6 The production report of EAF1 in (1-15 February, 2003) Cont.


In compliance with Tables 6.5 and 6.6, we know the quantity of utilizing the scrap for each day in EAF 1, for example, there are utilizing the scrap about 1,212 tons on the working day and 3,450 tons on the holiday or festival day. It indicated that the utilizing the scrap for producing the product about 2424 tons per day and 6900 tons per day on working day and holiday respectively because the company has the 2 EAF (EAF1, EAF2) to run continuous process in each day. And then the densities of mixing the scrap into the buckets are approximately 0.83 tons $/ \mathrm{m}^{3}$ that it is in the range of saving energy (between 0.8-0.9 tons $/ \mathrm{m}^{3}$ ).

According to data from the table 6.5 and 6.6, we can shown in the graph of density, scrap utilization, production result, and yield in Figures 6.1-6.4


Figure 6.1 The density of mixing the scrap 4 baskets

In January and February, the scrap preparing worker provides the scrap to the basket at the 0.83 ton $/ \mathrm{m}^{3}$ as shown in Figure 4.6. According to Figure 6.4, the density that saving energy for melting scrap are about 0.8-0.9 ton $/ \mathrm{m}^{3}$ and the worker can provide the scrap density in the rage of saving energy range. So the company receiving
the benefit from saving energy for melting scrap and can reducing the time for melting due to saving energy too.


Figure 6.2 The quantity of the used scrap in November, and December

In the Figure 6.2, it shows the utilization of the scrap each day in January and February by collecting the data from Tables 6.5 and 6.6. As you can see in the graph, the average quantity of scrap utilization is about 2,424 tons per day on the working day and 5,758 tons per day on the holiday and festival day. If we average these data, the average of utilization of scrap is equal to 3376.95 tons per day.


Figure 6.3 The result of production in December and November

According to Figure 6.3, the company uses the scrap about 2,424 tons per day on the working day and 5,758 tons per day on the holiday and festival day. After passing the production process, it can produce the product about tons per day on the working day and 3,800 tons per day on the holiday and festival day. According to these data, they can be taken to calculate the yield received from this formula.

$$
\text { Yield }=\frac{\text { Output(production) }}{\text { Input(Scrap used) }} \times 100
$$

Following this formula, the yield of the company in November and December can be plotted into Figure 6.4


Figure 6.4 The result of Production yield in December and November

As you can see in Figure 6,4. Yield is quite low in the first period of implementing the new pattern of basket if comparing with in the next period. The cause of this are that the worker that preparing the pattern of the basket are not familiar with the new quantity of the each scrap type because the equipment of taking the scrap can not take the certain quantity of scrap and the type of scrap are different from the original. So the quantity of the scrap mixing in the basket pattern is not constant. However, when the worker know the how much weigh can be received from picking the each scrap to the basket one time, the element of the scrap in the basket are constant and then it makes yield can improve from about $83.5 \%$ to $85 \%$.

By the way, from using the scrap in table 6.5, and 6.6. the chemical compositions are received from melting process can be shown in Tables 6.7 and 6.8

Table 6.7 The chemical compositions received after passing the melting process in
January

| Date | C |  | $P$ |  | $s$ |  | Mn |  | Si |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | tons | \% | tons | \% | tons | \% | tons | \% | tons | \% |
| 2/1/2002 | 9.43 | ก 39 | 0.56 | 0.02 | 0.49 | 0.02 | 5.83 | 0.24 | 4.08 | 0.17 |
| 3/1/2002 | 9.43 | 0.39 | 0.56 | 0.02 | 0.49 | 0.02 | 5.83 | 0.24 | 4.08 | 0.17 |
| 4/1/2002 | 22.40 | 0.39 | 1.34 | 0.02 | 1.16 | 0.02 | 13.85 | 0.24 | 9.68 | 0.17 |
| 5/1/2002 | 22.40 | 0.39 | 1.34 | 0.02 | 1.16 | 0.02 | 13.85 | 0.24 | 9.68 | 0.17 |
| 6/1/2002 | 9.43 | 0.39 | 0.56 | 0.02 | 0.49 | 0.02 | 5.83 | 0.24 | 4.08 | 0.17 |
| 7/1/2002 | 9.43 | 0.39 | 0.56 | 0.02 | 0.49 | 0.02 | 5.83 | 0.24 | 4.08 | 0.17 |
| 8,1/2002 | 9.43 | 0.39 | 0.56 | 0.02 | 0.49 | 0.02 | 5.83 | 0.24 | 4.08 | 0.17 |
| 9/1/2002 | 9.43 | 0.39 | 0.56 | 0.02 | 0.49 | 0.02 | 5.83 | 0.24 | 4.08 | 0.17 |
| 10/1/2002 | 9.43 | 0.39 | 0.56 | 0.02 | 0.49 | 0.02 | 5.83 | 0.24 | 4.08 | 0.17 |
| 11/1/2002 | 22.40 | 0.39 | 1.34 | 0.02 | 1.16 | 0.02 | 13.85 | 0.24 | 9.68 | 0.17 |
| 12/1/2002 | 22.40 | 0.39 | 1.34 | 0.02 | 1.16 | 0.02 | 13.85 | 0.24 | 9.68 | 0.17 |
| 13/1/2002 | 9.43 | 0.39 | 0.56 | 0.02 | 0.49 | 0.02 | 5.83 | 0.24 | 4.08 | 0.17 |
| 14/1/2002 | 9.43 | 0.39 | 0.56 | 0.02 | 0.49 | 0.02 | 5.83 | 0.24 | 4.08 | 0.17 |
| 15/1/2002 | 9.43 | 0.39 | 0.56 | 0.02 | 0.49 | 0.02 | 5.83 | 0.24 | 4.08 | 0.17 |
| 16/1/2002 | 9.43 | 0.39 | 0.56 | 0.02 | 0.49 | 0.02 | 5.83 | 0.24 | 4.08 | 0.17 |
| 17/1/2002 | 9.43 | 0.39 | 0.56 | 0.02 | 0.49 | 0.02 | 5.83 | 0.24 | 4.08 | 0.17 |
| 18/1/2002 | 22.40 | 0.39 | 1.34 | 0.02 | 1.16 | 0.02 | 13.85 | 0.24 | 9.68 | 0.17 |
| 19/1/2002 | 22.40 | 0.39 | 1.34 | 0.02 | 1.16 | 0.02 | 13.85 | 0.24 | 9.68 | 0.17 |
| 20/1/2002 | 9.43 | 0.39 | 0.56 | 0.02 | 0.49 | 0.02 | 5.83 | 0:24 | 4.08 | 0.17 |
| 21/1/2002 | 9.43 | 0.39 | 0.56 | 0.02 | 0.49 | 0.02 | 5.83 | 0.24 | 4.08 | 0.17 |
| 22/1/2002 | 9.43 | 0.39 | 0.56 | 0.02 | 0.49 | 0.02 | 5.83 | 0.24 | 4.08 | 0.17 |
| 23/1/2002 | 9.43 | 0.39 | 0.56 | 0.02 | 0.49 | 0.02 | 5.83 | 0.24 | 4.08 | 0.17 |
| 24/1/2002 | 9.43 | 0.39 | 0.56 | 0.02 | 0.49 | 0.02 | 5.83 | 0.24 | 4.08 | 0.17 |
| 25/1/2002 | 22.40 | 0.39 | 1.34 | 0.02 | 1.16 | 0.02 | 13.85 | 0.24 | 9.68 | 0.17 |


| Date | $C$ |  | $P$ |  | $S$ |  | $M n$ |  | $S i$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | tons | $\%$ | tons | $\%$ | tons | $\%$ | tons | $\%$ | tons | $\%$ |
| 26/1/2002 | 22.40 | 0.39 | 1.34 | 0.02 | 1.16 | 0.02 | 13.85 | 0.24 | 9.68 | 0.17 |
| 27/1/2002 | 9.43 | 0.39 | 0.56 | 0.02 | 0.49 | 0.02 | 5.83 | 0.24 | 4.08 | 0.17 |
| 28/1/2002 | 9.43 | 0.39 | 0.56 | 0.02 | 0.49 | 0.02 | 5.83 | 0.24 | 4.08 | 0.17 |
| 29/1/2002 | 9.43 | 0.39 | 0.56 | 0.02 | 0.49 | 0.02 | 5.83 | 0.24 | 4.08 | 0.17 |
| 30/1/2002 | 9.43 | 0.39 | 0.56 | 0.02 | 0.49 | 0.02 | 5.83 | 0.24 | 4.08 | 0.17 |
| 31/1/2002 | 9.43 | 0.39 | 0.56 | 0.02 | 0.49 | 0.02 | 5.83 | 0.24 | 4.08 | 0.17 |
| Total | 386.70 | 0.39 | 23.11 | 0.02 | 20.11 | 0.02 | 239.14 | 0.24 | 167.13 | 0.17 |

Table 6.8 The chemical compositions received after passing the melting process in
February (1-15)

| Date | C |  | P |  | S |  | Mn |  | Si |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | tons | $\%$ | tons | $\%$ | tons | $\%$ | tons | $\%$ | tons | $\%$ |
| $1 / 2 / 2002$ | 22.40 | 0.39 | 1.34 | 0.02 | 1.16 | 0.02 | 13.85 | 0.24 | 9.68 | 0.17 |
| $2 / 2 / 2002$ | 22.40 | 0.39 | 1.34 | 0.02 | 1.16 | 0.02 | 13.85 | 0.24 | 9.68 | 0.17 |
| $3 / 2 / 2002$ | 9.43 | 0.39 | 0.56 | 0.02 | 0.49 | 0.02 | 5.83 | 0.24 | 4.08 | 0.17 |
| $4 / 2 / 2002$ | 9.43 | 0.39 | 0.56 | 0.02 | 0.49 | 0.02 | 5.83 | 0.24 | 4.08 | 0.17 |
| $5 / 2 / 2002$ | 9.43 | 0.39 | 0.56 | 0.02 | 0.49 | 0.02 | 5.83 | 0.24 | 4.08 | 0.17 |
| $6 / 2 / 2002$ | 9.43 | 0.39 | 0.56 | 0.02 | 0.49 | 0.02 | 5.83 | 0.24 | 4.08 | 0.17 |
| $7 / 2 / 2002$ | 9.43 | 0.39 | 0.56 | 0.02 | 0.49 | 0.02 | 5.83 | 0.24 | 4.08 | 0.17 |
| $8 / 2 / 2002$ | 22.40 | 0.39 | 1.34 | 0.02 | 1.16 | 0.02 | 13.85 | 0.24 | 9.68 | 0.17 |
| $9 / 2 / 2002$ | 22.40 | 0.39 | 1.34 | 0.02 | 1.16 | 0.02 | 13.85 | 0.24 | 9.68 | 0.17 |
| $10 / 2 / 2002$ | 9.43 | 0.39 | 0.56 | 0.02 | 0.49 | 0.02 | 5.83 | 0.24 | 4.08 | 0.17 |
| $11 / 2 / 2002$ | 9.43 | 0.39 | 0.56 | 0.02 | 0.49 | 0.02 | 5.83 | 0.24 | 4.08 | 0.17 |
| $12 / 2 / 2002$ | 9.43 | 0.39 | 0.56 | 0.02 | 0.49 | 0.02 | 5.83 | 0.24 | 4.08 | 0.17 |
| $13 / 2 / 2002$ | 9.43 | 0.39 | 0.56 | 0.02 | 0.49 | 0.02 | 5.83 | 0.24 | 4.08 | 0.17 |
| $14 / 2 / 2002$ | 9.43 | 0.39 | 0.56 | 0.02 | 0.49 | 0.02 | 5.83 | 0.24 | 4.08 | 0.17 |
| $15 / 2 / 2002$ | 22.40 | 0.39 | 1.34 | 0.02 | 1.16 | 0.02 | 13.85 | 0.24 | 9.68 | 0.17 |
| $T 0 t a 1$ | 206.32 | 0.39 | 12.33 | 0.02 | 10.73 | 0.02 | 127.59 | 0.24 | 89.17 | 0.17 |

After the scraps in Tables 6.5 and 6.6 are melted in the EAF1, the chemical composition received in January and February can be shown in Tables 6.7 and 6.8. The percent of carbon, sulfur, phosphorous, manganese and silicon are still about 0.39, $0.02,0.02,0.24$ and 0.17 respectively.
6.1.2 Time utilization of melting the scrap


Figure 6.5 Procedure of used energy for melting process

According to the procedure above, we found that

| On time | $=55.24 \mathrm{mins} /$ heat |
| :--- | :--- |
| Off time | $=19 \mathrm{mins} /$ heat |
| Iotal | $=74.24 \mathrm{mins} /$ heat |

On time 55.24 minutes can be separate into:

## On Ttime

From Scrap:

$$
\frac{151 t \times 331.4 \mathrm{Kwh} / t}{1000 \mathrm{Kwh} / \mathrm{min}}=50.04 \text { minute }
$$

$$
\frac{5.2 t \times 1000 K w h / t}{1000 K w h / \mathrm{min}}=5.2 \text { minutes }
$$

From Addition Lime: $\quad \frac{5.2 t \times 1000 \mathrm{Kwh} / \mathrm{t}}{1000 \mathrm{Kwh} / \mathrm{min}}=5.2$ minutes
Off time 25 minutes can be separate into:

## OFF Time



However, from the table 6.5 and 6.5 , we will see that T-T-T time is about 74.3 minutes in practical. It is slightly different from the calculation. So the result of melting time is the level acceptance.

### 6.1.3 Yield result



Scrap using


Production receiving
$=128.35$ tons
Yield
$=\frac{128.35}{151} \times 100$ percent
$=85$ percent

According to this result, if we take this result to compare with the calculation result at the same quantity of scrap(151 tons), the comparison of both can be shown in the table below:

Table 6.9 The comparison result between the current managing scrap and the calculating the result of managing the scrap to improvement at density 0.6 ton $/ \mathrm{m}^{3}$ and 0.85 ton $/ \mathrm{m}^{3}$ respectively

| Item | Current managing scrap | Calculating to Improving | Difference |
| :---: | :---: | :---: | :---: |
| Scrap | 151 tons/heat | 151 tons/heat | 0 |
| Production | 128.35 tons/heat | 132 tons/heat | 3.65 |
| Yield | 85\% | 87.42\% | 2.42\% |
| On-Time |  |  |  |
| -Scrap | 55.24 minutes | 55.24 minutes | 0 minutes |
| -Addition Flux | 5.2 minutes | 5.2 minutes | 0 minutes |
| Off-Time |  |  |  |
| -Charging | 6 minutes | 6 minutes | 0 minutes |
| -Tapping | 4 minutes | 4 minutes | 0 minutes |
| -Other | 9 minutes | 9 minutes | 0 minutes |
| T-T-T | 72.24 minutes | 72.2 minutes | (-.04) minutes |

### 6.1.4 Disadvantage managing the 4 -basket pattern

Disadvantages of managing the raw materials (scrap, pig iron, flux and so on) 2 baskets at density 0.83 tons $/ \mathrm{m}^{3}$ can be shown Table 6.10:

Table 6.10 Disadvantages of managing the raw materials 2 baskets comparing with standard at density 0.83 tons $/ \mathrm{m}^{3}$

| Disadvantage | Lose time/heat | Loss time/2months | $\%$ |
| :--- | :---: | :---: | :---: |
|  | (minutes) | (minutes) |  |
| Long time for <br> Melting scrap <br> time | 0 |  | 0 |
| Long time for <br> Melting Addition <br> time | 0 | 0 | 0 |
| Long time for <br> Charging the <br> baskets to EAF |  | 0 | 0 |
| Total |  | 0 |  |



Figure 6.6 The Pareto chart of lose time due to managing 2 baskets

According to the table 6.9 and 6.10, these data can be shown in the pareto chart demonstrate the lost time due to managing scrap 2 baskets in figure 6.6, scrap using,
production quantity, and yield in January and February in figure 6.7 and total scrap using, production quantity, and yield in 1.5 months in figure 6.8.


Figure 6.7 Scrap using, production quantity, and yield in January and February(1-15)


Figure 6.8 Total Scrap using, production quantity, and yield in 1.5 months

### 6.1.5 The utilizing of flux for 2 baskets

According to utilizing of flux for 2 baskets from calculation in Chapter 5, the company fixes the quantity of flux using following calculation. And the result of chemical is nearly the specification that require from this pattern. So the quantity of flux using can be shown in the process below:

Add material additive charging to the baskets

Table 6.11 Charging Flux in Scrap basket

| CaO <br> $(\mathrm{Kg})$ | Dolomite <br> $(\mathrm{Kg})$ |
| :---: | :---: |
| 500 | - |

## Add between melting by EAF Material Weighting/Charging

Table 6.12 EAF material Weighting/Charging

| Charge №. | $\operatorname{Bin}$ No. 2 <br> CaO | Bin No. 3 <br> B-Dolomite |
| :---: | :---: | :---: |
| 1st | Chill 1600 amorn | IVERSITY 700 |
| 2 nd | 700 | 440 |

Add before refining by Tapping Material Weighting/Charging

Table 6.13 Tapping Material weighting/Charging

| Charge | Bin No.2 | Bin No.5 |
| :---: | :---: | :---: |
| No. | CaO | B-Dolomite |
| 1st | 1200 | 60 |

According to utilizing the flux above, the total flux utilizes are equal to 5,200 $\mathrm{kg} / \mathrm{heat}$. The detail of utilizing can be show below:

Flux Utilization of 2 basket pattern


### 6.1.6 Comparing the result before and after improvement

## Comparison Density



Figure 6.9 Comparison density of before and after improvement

As you can see Figure 6.9, the density before improvement is 0.62 ton $/ \mathrm{m} 3$ and the density after improvement is 0.83 ton $/ \mathrm{m} 3$. It shows that the new pattern of the mixing makes the density increasing from the past. Increasing the density from 0.62 to 0.83 makes EAF saved the energy to melting the scraps. In addition, the quantity of basket reducing due to improve the density leads to the charging time reducing too. So the company should fix at this density that has more benefit from the past.

## Comparison the disadvantages



Figure 6.10 Comparison the disadvantage of before improvement and after improvement with the standard company.

As shown in Figure 6.10, it shows that the company before improvement the company has to loss time due comparison with the standard Japanese company to charging the basket 6 minute per heat, melting scrap 2.9 minutes per heat, and melting time 1.9 minutes. However, after improvement, the company can melt both scrap and addition following the standard pattern. It makes the company don't have the difference time between the standard company. In addition, the company can reduce the charging scrap time from 4 times for 4 -basket pattern to 2 times for 2-basket pattern like the standard company so there is no loss time happened due to charging the scrap.

## Comparison Scrap utilization/heat



Figure 6.11 Comparison scraps utilization of before and after improvement

Before improvement, the company used the scraps 149.5 tons per heat in 4 baskets for being the raw material to produce the steel. In the planning of improvement, the company tries to set the weight of the scrap (new categorizing the scrap) equal before improvement by calculation from the program mixing the scrap. However, in practical, the quantity of scrap taken from the crane is about 151 tons. So the company using this to consider the quantity of using the other raw material and the melting process. However, the quantity of before and after improvement are slightly different about 0.5 tons or 0.33 percent. So the company used this quantity of the scrap to be the standard of this product (MS code00001).

## Comparison Production received/heat



Figure 6.12 Comparison Production received of before and after improvement

According to Figure 6.12, the production per heat before improvement is 112.125 tons and after improvement is 128.35 tons. The difference production between before and after improvement is about 16 tons per heat or 12.64 percent. As you can see in Figures 6.10 and 6.12, the quantities of scrap used are slightly different ( $0.33 \%$ ) but the output of the melting these scraps are quite different (12.64\%). It shows that after improvement the company receiving the increasing output rate more than increasing the input rate. It means the yield after improvement is more than the yield before improvement. The comparisons between yield before improvement and after improvement can be shown in Figure 6.13. So if we consider at 1 month ( 28 days) that separate into 20 working days and 8 holidays, the quantity of heat before improvement is equal to 296 heats per month per furnace and the quantity of heat after improvement is equal to 312 heats per month per furnace. So the quantity of output per months that receives increasing from improvement is equal to:

$$
\begin{aligned}
\text { Increa sin g output } & =296 \times 16+(312-296) \times 128.35 \\
& =6792 \text { tons } / \text { furnace }
\end{aligned}
$$

As you can see, after improvement, the company can increase the production abut 6792 tons per furnace. Due to having 2 furnaces, the production increasing is equal to 13584 tons. This is the high benefit receiving from improvement. If comparison this into sale price, the company can sale increasing about 203,760,000 baht per month

## Comparison Yield



Figure 6.13 Comparison Yield of before and after improvement

Yield is the rate of output and input. As you can see from Figures 6.11 and 6.13., before improvement, the company uses the scraps 149.5 tons and received the output is 112.125 tons so yield before improvement are equal to :

$$
\text { Yield }_{\text {before inrovement }}=\frac{149.5-112.125}{149.5} \times 100=75 \%
$$

After improvement, the company uses the scrap 151 tons and receiving the output is 128.35 tons so yield after improvement are equal to:

$$
\text { Yield }_{\text {afteri improvement }}=\frac{151-128.35}{151}, \times 100=85 \%
$$

So yield after improvement are increased by $10 \%$ from before improvement. It leads to the company can receiving the product.

## Comparison flux utilization/heat



Figure 6.14 Comparison flux used of before and after improvement

The total flux used before improvement is equal to 7200 kilograms and the flux used after improvement is equal to 5200 kilograms. The difference of flux used before and after improvement is equal to 2000 kilogram. So if we consider at 1 month ( 28 days) that separate into 20 working days and 8 holidays, the quantity of heat before improvement is equal to 296 heats per month and the quantity of heat after improvement
is equal to 312 heats per month. However, if we consider at the same quantity of heat at 312 heats, the quantity of flux reduce by:

$$
\begin{aligned}
\text { Flux Reducing } & =312 \times 2 \\
& =624 \text { tons/furnace }
\end{aligned}
$$

However, the company has two furnaces so the reducing of flux used are equal to $624 \times 2=1248$ kilograms. Flux reduces 1248 tons per month consider at the same quantity of heat at 312 heats per furnace. It makes the company can reducing the cost of flux (about 5 bath/kg).. In addition, the company saves the time from reducing melting the flux about 1248 minutes.

## Comparison T-T-T/heat



Figure 6.15 Comparison Tap-To-Tap between before and after improvement

As you can see in Figure 6.15, the company reduces the T-T-T time about 8.76 minutes per heat. As we consider the time used in 1 month ( 28 day). The company can reduce the time equal to :

$$
\begin{aligned}
T-T-T \text { reducing } \quad & =8.7 \mathrm{~min} \times 312 \text { heat } \\
& =2714 \mathrm{~min} \text { ute }
\end{aligned}
$$

However, if we consider at time used in the 1 month ( 28 days) by separating into working day (11 hours, 20days) and holiday ( 24 hours, 8 days), the company can run the production 8 heat/day on the working day and 17 heat/day on the holiday. So , in 1 month (28days), the company can run the quantity of heat equal to:

Quantity of heatbefore improvement $\quad=\frac{11 \times 60}{83} \times 20+\frac{(24 \times 60)}{83} \times 8$
$=8 \times 20+17 \times 8$
$=160+136=296$ heats

And the quantity of heat after improvement can be show below:
Quantity of heataferimporvement $=\frac{11 \times 60}{74.3} \times 20+\frac{(24 \times 60)}{74.3} \times 8$

$$
=8 \times 20+19 \times 8
$$

$$
=160+152=312 \text { heats }
$$

As comparing the two quantity, the company receive the quantity of heat increasing $=312-296=16$ heat per month for 1 furnace. However the company has two furnaces. So the company can increase the quantity of heat by 32 heats per month

### 6.2 Analyzing Operating cost, Sale price and Profit per Month before and

 after ImprovementFor this improvement, the company has changed the new scrap types, change the addition flux, and so on but no increasing investment and labor cost. Therefore, the detail of the cost per ton ${ }_{\text {product }}$ before and after improvement can be shown in Table 6.15 and Table 6.17 respectively.

## Before improvement

Table 6.14 The scrap price in November and December

| Type | Unit Cost <br> Baht/t $t_{s}$ | Quantity <br> $t_{s}$ | Cost <br> Baht |
| :---: | ---: | ---: | ---: |
| Po(ex) | $6,300.0$ | 9.0 | $56,700.0$ |
| Po | $6,000.0$ | 17.0 | $102,000.0$ |
| A | $5,400.0$ | 33.0 | $178,200.0$ |
| B | $5,000.0$ | 65.5 | $327,500.0$ |
| I | $7,000.0$ | 25.0 | $175,000.0$ |
| Total |  |  |  |
| Average (Baht $\left./ t_{\mathrm{s}}\right)$ |  |  |  |

Table 6.14 showed the price of each scrap that the company can find in November and December and the quantity of each scrap used in each heat. From this price and quantity, it can be calculated the average cost per ton scrap equal to 5614.7 baht at density 0.62 ton $/ \mathrm{m}^{3}$. After calculating the cost per ton of the scrap, it can be calculating the production cost per ton product as shown in Table $6.15 ~_{\text {Pr }}$

In Table 6.15, It shows the production cost per ton $n_{\text {product }}$ by calculating cost from the scrap used to produce the product 1 tons, Energy used, Addition used, Ferro-alloys used, Maintenance cost, Refractory cost, Labor cost, Roiling mill cost, and the other cost.

Table 6.15 Production Cost per ton product of the product before improvement

| Description | Unit Cost | Quantity | Cost |
| :---: | :---: | :---: | :---: |
|  | (Baht/Unit) | (Unit/t ${ }_{\text {product }}$ ) | (Baht/t product ) |
| Scrap | 5,614.72 | 1.33 | 7,486.27 |
| Energy |  |  |  |
| -Electrical | 1.75 | 517.30 | 905.28 |
| -Oxygen | 4.00 | 35.00 | 140.00 |
| -Natural gas | 5.50 | 3.00 | 16.50 |
| -Electrode | 150.00 | 2.00 | 300.00 |
| Addition |  |  |  |
| -Flux | 4.00 | 64.00 | 256.00 |
| -Coke | 6.00 | 46.00 | 276.00 |
| - $\mathrm{CaF}_{2}$ | 6.00 | 3.74 | 22.44 |
| Ferro-Allovs |  |  |  |
| -Fe-Si | 40.00 | 4.00 | 160.00 |
| -Fe-Mn | 25.00 | 10.00 | 250.00 |
| -Al ash | 10.00 | 1.60 | 16.00 |
| -SiC | 30.00 | 2.00 | 60.00 |
| Maintenance Cost | 180.00 | P $\quad 1.00$ | 180.00 |
| Refractory Cost | 320.00 | $\checkmark 1.00$ | 320.00 |
| Labour Cost | 30.00 | -1.00 | 30.00 |
| Other | 120.00 | $y)=1.00$ | 120.00 |
| Roll Mill Cost | 895.00 | 1.00 | 895.00 |
|  |  | Total Cost | 11,433.48 |

So for the product 1 tons, the cost of production is equal to 11433.48 baht per ton $_{\text {product }}$



Figure 6.16 Average Sale, Cost and Profit per Month before Improvement

## After Improvement

Table 6.16 The scrap price in January and February

| Type | Unit Cost | Quantity | Cost |
| :---: | :---: | :---: | :---: |
|  | Baht/t ${ }_{\text {s }}$ | $t_{s}$ | Baht |
| S183 | 6,090.0 | 34.0 | 207,060.0 |
| S187 | 6,525.0 | 7.0 | 45,675.0 |
| S517 | 6,960.0 | 65.0 | 452,400.0 |
| S400 | 7,100.0 | 8.0 | 56,800.0 |
| S406 | 7,400.0 | 1.0 | 7,400.0 |
| S922 | 6000 | 3.0 | 18,000.0 |
| S923 | 6,000.0 | 2 | 12,000.0 |
| S900 | 6,000.0 | 1.0 | 6,000.0 |
| 1116 | 7,000.0 | 30.0 | 210,000.0 |
| Total |  | 151.0 | 1,015,335.0 |
|  | Average (Baht/ts) |  | 6,724.1 |

Table 6.16 showed the unit cost per ton $n_{\text {scrap }}$ of each scrap type, quantity of scrap used in 1 heat, and the cost from each scrap type per heat. All of these can be
calculated the average cost per ton scrap equal 6724.1 baht per ton scrap . However, 1 ton product has to used 1.18 ton scrap. So the production cost of producing the product 1 ton can be shown in the figure 6.17

Table 6.17 Production Cost per ton product of the product after improvement

| Description | Unit Cost | Quantity | Cost |
| :---: | :---: | :---: | :---: |
|  | (Baht/Unit) | (Unit/t product ) | (Baht/t product ) |
| Scrap | 6,724.07 | 1.18 | 7,910.87 |
| Energy |  |  |  |
| -Electrical | 1.75 | 430.39 | 753.18 |
| -Oxygen | 4.00 | 35.00 | 140.00 |
| -Natural gas | 5.50 | 3.00 | 16.50 |
| -Electrode | 150.00 | 2.00 | 300.00 |
| Addition |  |  |  |
| -Flux | 4.00 | 40.50 | 162.00 |
| -Coke | 6.00 | 30.00 | 180.00 |
| - $\mathrm{CaF}_{2}$ | 6.00 | 3.74 | 22.44 |
| Ferro-Allovs |  |  |  |
| -Fe-Si | 40.00 | 4.00 | 160.00 |
| -Fe-Mn | 25.00 | 10.00 | 250.00 |
| -Al ash | 10.00 | 1.60 | 16.00 |
| - SiC | 30.00 | 2.200 | 60.00 |
| Maintenance Cost | 160.00 | (3) 1.00 | 160.00 |
| Refractorv Cost | 280.00 | (6) 1.00 | 280.00 |
| Labour Cost | 23.00 | 1.00 | 23.00 |
| Other | 100.00 | 1.00 | 100.00 |
| Roll Mill Cost | 890.00 | 1.00 | 890.00 |
|  |  | Total Cost | 11,423.99 |

So for the product 1 tons, the cost of production is equal to 11423.99 baht per ton product
In 1 month: Average production/month $=88,232$ ton $_{\text {product }}$
Average Cost/month รณมหาวทย $88,232 \times 11433.48$
CHULALONGKORN $=$ NIV/ 1007961561.11 Baht/month

Sale price $=15,000 \mathrm{baht} /$ ton $_{\text {product }}$
Average Total Sale $=15000 \times 88,232$
$=132,480,000$ Baht/month
therefore: Average Profit $=1,323,480,000-1,007,961,561.11$
$=315,518,438.88$ Baht/month


Figure 6.17 Average Sale, Cost and Profit per Month after Improvement

Comparison Profit before and after improvement
From Figure 6.16 and Figure 6.18, the sale after improvement increase from $1,099.079$ million Baht to $1,324.8$ million Baht so the sale increases by 20.53 percent. The cost after improvement increases from 837.748 million Baht to $1,007.96$ million baht. The difference is about 20.31 percent. From the sale and cost, the profit after improvement increase from 261.32 million baht to 315.518 million baht. The increasing profit is equal to 54.198 million baht (about 20.\%) as shown in figure 6.18


Figure 6.18 Comparison average profit per month between before and after improvement

### 6.3 Conclusion Result



Managing of the suitable plan and method for improvement about the scrap and chemical composition received lead to improve yield in the melting process.

New Pattern of melting the scrap in the EAF makes reducing the cost due to using the electrical energy reducing and using indirect raw material reducing as shown in the table 6.18

Table 6.18 Comparing using energy, lime, production, and yield before and after improvement.

| Items | Before Improvement | After improvement |
| :--- | :--- | :--- |
| Energy | $387.96 \mathrm{KwH} / T_{\text {scrap }}$ | $365.82 \mathrm{KwH} / T_{\text {scrap }}$ |
| Lime | $7200 \mathrm{kgs} / T_{\text {scrap }}$ | $5200 \mathrm{kgs} / T_{\text {scrap }}$ |
| Production | $750 \mathrm{kgs} / T_{\text {scrap }}$ | $870 \mathrm{kgs} / T_{\text {scrap }}$ |
| Yield | $75 \%$ | $85 \%$ |

Time using for melting the scrap reduce from the past. It lead to the more time for producing from T-T-T $=83$ minutes/heat to 74.24 minutes $/$ heat

According to efficiency increasing from the improvement, it makes all functions, departments, top management and so on are awareness and unique to improvement in the next project improvement.
> It makes the company can sent more products to support market requirement by profit after improvement increasing by 54.2 million baht per month from before improvement.

