

REFERENCES

- [1] Wilber, G.A., Batra, R., Savage, W.F. and Childs, W.J. The effects of thermal history and composition on the hot ductility of low carbon steels. Metallurgical Transactions, Vol.6A, September 1975, pp.1727-1735.
- [2] Suzuki, H.G., Nishimura, S. and Yamaguchi, S. Characteristics of hot ductility in steels subjected to the melting and solidification. Transaction ISIJ, Vol.22, 1982, pp.48-56.
- [3] Suzuki, H.G., Nishimura, S. and Nakamura, Y. Improvement of hot ductility of continuous cast carbon steels. Transaction ISIJ, Vol.24, 1984, pp.54-59.
- [4] Suzuki, H.G., Nishimura, S. and Yamaguchi, S. Physical simulation of the continuous casting. The symposium on physical simulation of welding, hot forming and continuous casting, May 2-4th, 1988, CANMET, Canada, pp.1-25.
- [5] Thomas, B.G., Brimacombe, J.K. and Samarasekera, I.V. The formation of panel cracks in steel ingots: A state-of-the-art review. ISS Transactions, Vol.7, 1986, pp.7-20.

- [6] Mintz, B., Yue, S. and Jonas, J.J. Hot ductility of steels and its relationship to the problem of transverse cracking during continuous casting. International Material Reviews, Vol.36 No.5, 1991, pp.187-217.
- [7] Schmidtman, E. and Merz, M. Effect of cooling conditions and strain rate on high temperature properties of structural steels in continuous casting. Steel research Vol.58 No.4, 1987, pp.191-196.
- [8] Yamanaka, A., Nakajima, K. and Okamura, K. Critical strain for internal crack formation in continuous casting. Ironmaking and Steelmaking, Vol.22 No.6, 1995, pp.508-512.
- [9] Schmidtman, E. and Pleugel, L. Influence of carbon content on high-temperature strength and ductility of low alloyed steels after solidification from the melt. Arch. Eisenhüttenwas. Vol.51 Nr.2, 1980, pp.49-54.
- [10] Schmidtman, E. and Rakoski, F. Influence of the carbon content of 0.015 to 1% and of the structure on the high-temperature strength and toughness behavior of structure steel after solidification from the melt. Arch. Eisenhüttenwesen, Vol.54 No.2, 1983, pp.357-362.

- [11] Thome, R. and Dahl, W. On the crack susceptibility of high alloyed tool steel during continuous casting and in the temperature region of hot working. Steel Research Vol.66 No.2, 1995, pp.63-71.
- [12] Brimacombe, J.K. and Samarasekera, I.V. Principles of solidification and materials processing. Vol.1 in proceeding of Indo-US Workshop, ed. By R. Trivedi et al., Trans. Tech. Pub., New Delhi, 1990, p.179.
- [13] Clyne, T.W., Wolf, M. and Kurz, W. The effect of melt composition on solidification cracking of steel, with particular reference to continuous casting. Metallurgical Transactions, Vol.13B, 1982, pp.259-266.
- [14] Matsubara, K. On the behaviors of the precipitated sulfide inclusions in solid steel. Transaction ISIJ, Vol.6, 1966, pp.29-49.
- [15] Kim, K., Yeo, T., Oh, K.H. and Lee, D.N. Effect of carbon and sulfur in continuously cast strand on longitudinal surface cracks. ISI International, Vol.36 No.36, 1996, pp.284-289.
- [16] Lankford, W.T. Some Considerations of Strength and Ductility in the Continuous-Casting Process. Metallurgical Transaction, Vol.3, 1972, pp.1331-1357.

- [17] Mintz, B. Importance of A_{r3} temperature in controlling ductility and width of ductility trough in steel, and its relationship to transverse cracking. Materials Science and Technology, Vol.12, 1996, pp.132-138.
- [18] Wilson, F.G. and Gladman, T. Aluminium nitride in steel. International Materials Reviews, Vol33 No.5, 1988, pp.221-286.
- [19] Yasumoto, K., Maehara, Y., Ura, S. and Ohmori, Y. Effect of sulfur on hot ductility of low-carbon steel austenite. Material Science and Technology, Vol.1, 1985, pp.111-116.
- [20] Sakai, T. and Ohashi, M. Physical Metallurgy of thermo-mechanical processing of steels and other metals. Thermec 88', Tokyo, The Iron and Steel Institute of Japan, Vol.1, 1988, p.162.
- [21] Deprez, P., Bricout, J.P. And Oudin, J. Tensile test on *in situ* solidified notched specimens: effect of temperature history and strain rate on the hot ductility of Nb and Nb-V microalloying steels. Materials Science and Engineering, A168, 1993, pp.17-22.
- [22] Revaux, T., Deprez, P., Bricout, J.P. and Oudin, J. *In situ* solidified hot tensile test and hot ductility of some plain carbon steels and

- microalloyed steels. ISIJ International, Vol.34 No.36, 1994, pp.528-535.
- [23] William, F.S. Structure and properties of engineering alloys. McGraw-Hill, Inc., 1993, p.387
- [24] Robert, G.A., Hamaker, J.C. and Johnson, A.R. Tool steels. American Society for Metals, Ohio, 1962.
- [25] Shinoda, T., Miyake, H., Matsuzaka, T., Matsumoto, T. and Kanai, H. Hot crack susceptibility of boron modified AISI 304 austenitic stainless steel welds. Materials Science and Technology, Vol.8, October 1992, pp.913-921.
- [26] Turkdogan, E.T. and Grange, R.A. Microsegregation in steel. Journal of The Iron and Steel Institute, May 1970, pp.482-494.
- [27] Turkdogan, E.T. Theoretical aspects of sulfide formation in steel, in Proceeding of an International Symposium "Sulfide Inclusion in Steel". 7-8 November 1974, port Chester, New York, pp.1-21.
- [28] Imagumbai, M. Behaviors of manganese-sulfide in aluminium-killed steel solidified uni-directionally state-dendrite structure and inclusions. ISIJ International, Vol.34 No.11, 1994, pp.896-905.
- [29] Ito, Y., Masumitsu, N. and Matsubara, K. Formation of manganese sulfides in steel. Transaction ISIJ, Vol.21, 1981, pp.477-484.

- [30] Baker, T.J. Use the scanning electron microscopy in studying sulfide morphology on fracture surface, in Proceeding of an International Symposium "Sulfide Inclusion in Steel". 7-8 November 1974, Port Chester, New York, pp.135-159.

APPENDIXES

APPENDIX I

DESCRIPTION OF DTA

The Differential Thermal Analysis (DTA) is applied to determine liquidus, solidus and phase transformations temperature during solidification of steel. It is a technique that is recording the temperature difference between a sample and a reference material. The equipment is comparing the temperature of the two specimens. Both are cooled down or heated up under the same condition. The reference material is Alumina (Al_2O_3) which makes no transformation of phases or changing of the inner energy due to lattice transformations or solidification. Therefore a change in the temperature is indicating a transformation due to the exothermic or endothermic effect during the phase transformation of the sample.

The major parts of the DTA, brand name is Netzsch 404s, are shown in Fig.A1-1. The equipment consists mainly of vacuum furnace, specimen carrier, temperature measurement system and controlling unit and power unit.

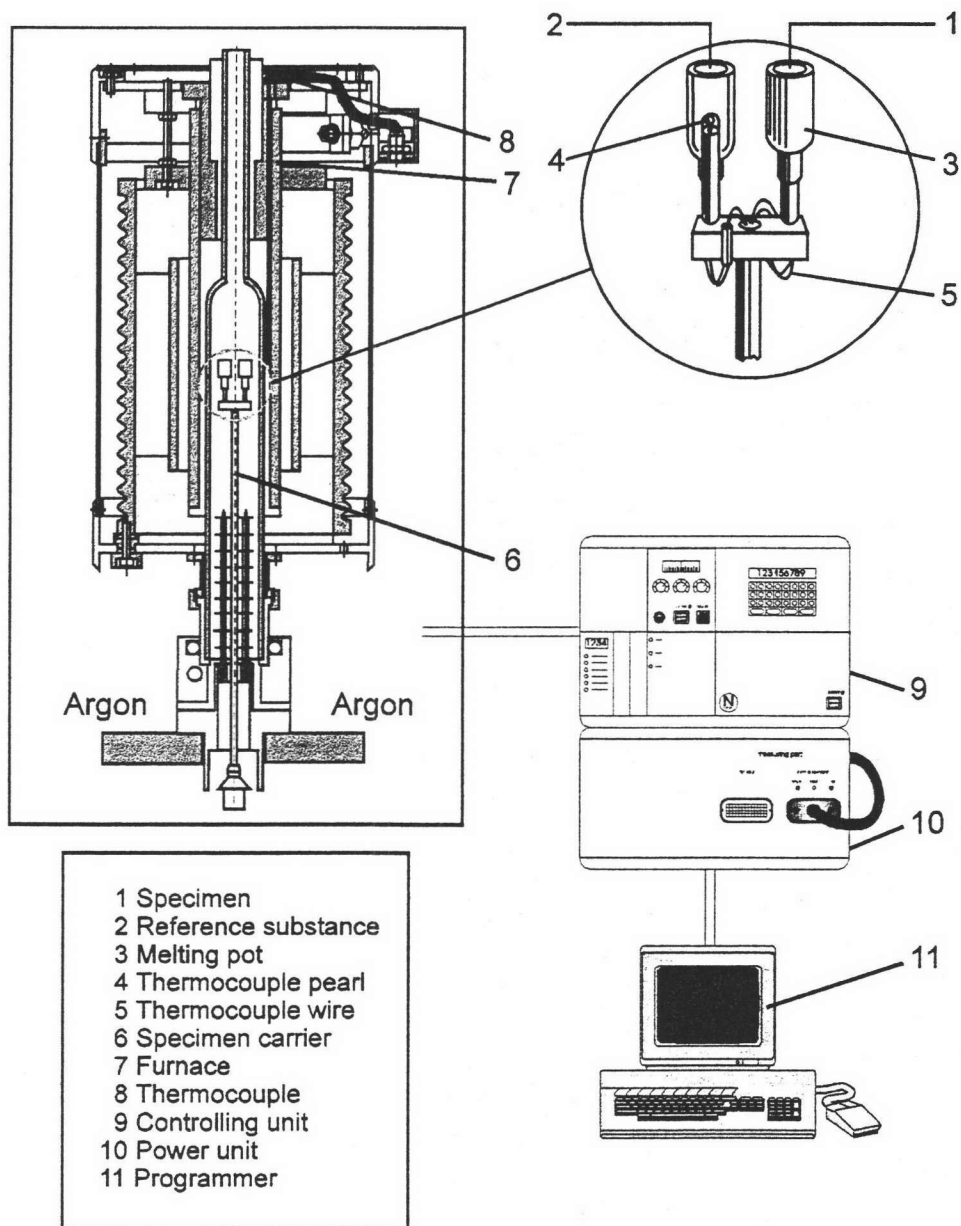


Fig.A1-1 Differential-Thermal Analysis (DTA) equipment.

The samples are heated up and cooled down with a certain cooling down or heating up velocity under argon atmosphere. During the tests the data are then transferred in a DTA-curve. The curve shows series of peaks that correspond to a phase transformation of the sample.

The sample (200 mg) was put in the sample holder inside the equipment. The operation is controlled by computer program. After closing the furnace the tests will be started in an inert atmosphere to minimize sample oxidation. The sample is heated up automatically with a heating rate of $10^{\circ}\text{C}/\text{min}$ and cooled down with the same rate. A specific recording device records the data of DTA.

A simplified curve of DTA is shown in Fig.A1-2. The figure displays the way to determine the solidus and liquidus temperature with the help of the DTA-curve. For the cooling curve the solidus temperature takes place at the point where the base line and incline line (solidification path) meet. The heating curve indicates the liquidus temperature at the peak of the curve.

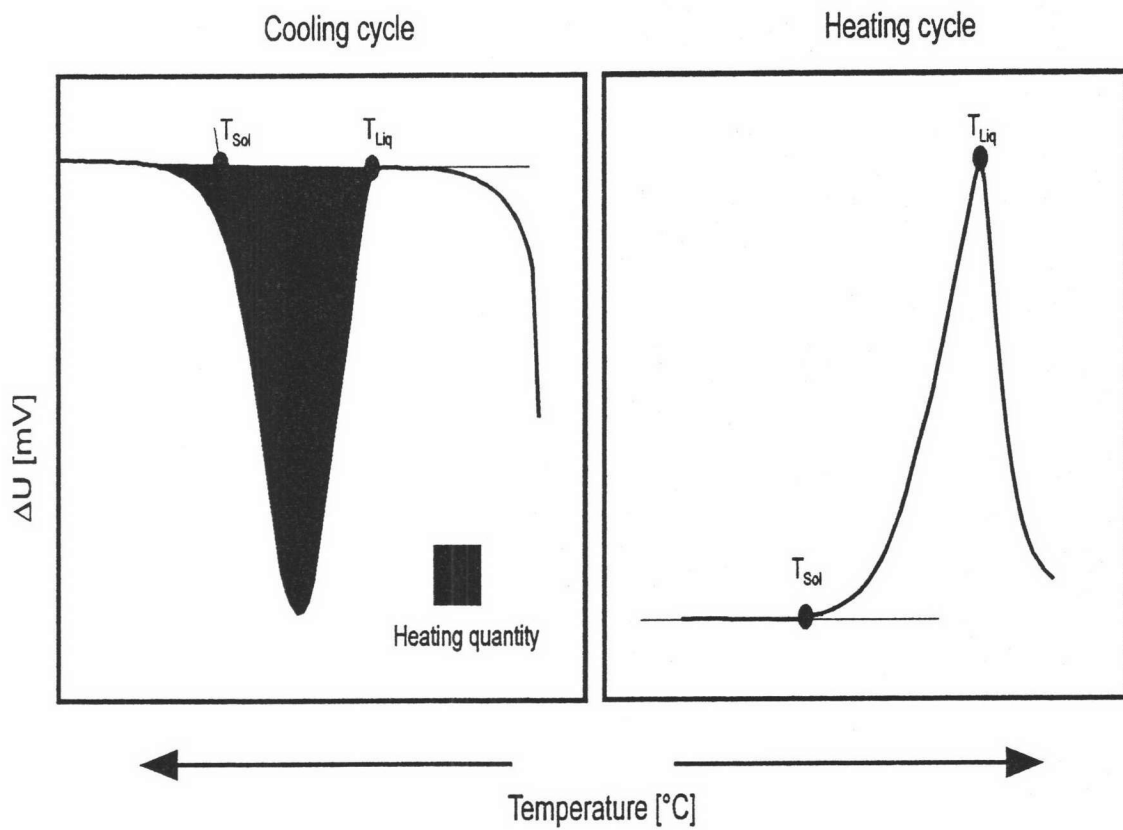


Fig.A1-2 Schematic diagram of a simple heating and cooling curve of DTA.

APPENDIX II

DATA OF HOT TENSILE TEST

Four groups of hot tensile test of steel grade AISI L3 are shown in Table A2-1 to A2-4, whereas the last four tables are the results of hot tensile test of steel grade AISI 01.

Table A2-1 Data of hot tensile test of steel grade AISI L3, group L3-1 (Strain rate: 2×10^{-3} /s, Cooling rate: 0.5°C/s)

Trial number	T _{test} (°C)	F _{max} (kN)	D _F (mm)	RA (%)	Remark
11/S1	897	14.24	4.7	95	
10/S1	1000	9.15	1.7	99	
9/S1	1096	5.96	0.0	100	
14/S1	1157	5.32	0.0	100	
1/S1	1198	4.14	12.5	63	
2/S1	1230	3.57	19.5	11	
3/S1	1245	2.84	20.1	5	
4/S1	1255	2.54	20.4	2	
12/S1	1263	2.53			ZDT
5/S1	1264	2.62			
13/S1	1271	2.92			
6/S1	1357	0.81			
8/S1	1382	0.29			
15/S1	1389	0.00			ZST
7/S1	1397	0.00			

Table A2-2 Data of hot tensile test of steel grade
 AISI L3, group L3-2 (Strain rate: $2 \times 10^{-3}/s$,
 Cooling rate: $3^{\circ}C/s$)

Trial number	T _{test} (°C)	F _{max} (kN)	D _F (mm)	RA (%)	Remark
H/S1	896	13.70	16.3	37	
G/S1	1000	8.04	15.7	42	
F/S1	1050	7.31	14.2	52	
E/S1	1129	5.64	12.9	61	
C/S1	1162	5.05	12.4	64	
A/S1	1203	4.21	14.1	53	
L/S1	1238	3.36	14.7	49	
I/S1	1253	3.53	14.1	53	
J/S1	1277	2.86	19.9	7	
K/S1	1284	2.82	20.2	4	
S/S1	1296	2.23			ZDT
Q/S1	1323	1.13			
R/S1	1343	0.82			
O/S1	1357	0.00			ZST

Table A2-3 Data of hot tensile test of steel grade
 AISI L3, group L3-3 (Strain rate: $2 \times 10^{-2}/s$,
 Cooling rate: $0.5^{\circ}C/s$)

Trial number	T _{test} (°C)	F _{max} (kN)	D _F (mm)	RA (%)	Remark
IV/S1	900	17.49	6.5	90	
III/S1	1000	10.77	15.0	47	
II/S1	1150	6.02	17.2	30	
IX/S1	1158	4.85			ZDT
VII/S1	1169	4.53			
VI/S1	1184	3.57			
V/S1	1203	3.93			
I/S1	1303	0.80			
XII/S1	1304	0.90			
XIV/S1	1320	1.19			
X/S1	1335	0.00			ZST
XI/S1	1344	0.00			

Table A2-4 Data of hot tensile test of steel grade
 AISI L3, group L3-4 (Strain rate: 2×10^{-2} /s,
 Cooling rate: 3°C/s)

Trial number	T _{test} (°C)	F _{max} (kN)	D _F (mm)	RA (%)	Remark
H1/S1	900	18.00	14.8	49	
I1/S1	902	17.77	14.7	48	
G1/S1	1002	9.51	13.5	57	
F1/S1	1100	7.60	14.9	48	
B1/S1	1203	5.47	14.7	49	
E1/S1	1238	3.74	20.0	6	
C1/S1	1256	3.49	20.3	2	
D1/S1	1266	3.00			ZDT
A1/S1	1308	2.45			
L1/S1	1324	1.71			
J1/S1	1335	0.00			ZST
K1/S1	1335	0.00			

Table A2-5 Data of hot tensile test of steel grade
 AISI O1, group O1-1 (Strain rate: 2×10^{-3} /s,
 Cooling rate: 0.5°C/s)

Trial number	T _{test} (°C)	F _{max} (kN)	D _F (mm)	RA (%)	Remark
7/S2	893	17.08	11.2	70	
4/S2	1000	10.13	3.5	97	
3/S2	1103	6.56	0.0	100	
2/S2	1204	4.24	0.0	100	
5 S2	1255	3.47	17.5	28	
6/S2	1278	2.92	20.0	6	
12/S2	1290	2.53			ZDT
1/S2	1306	2.43			
8/S2	1400	0.58			
9/S2	1408	0.38			
10/S2	1415	0.00			ZST
11/S2	1421	0.00			

Table A2-6 Data of hot tensile test of steel grade
 AISI O1, group O1-2 (Strain rate: $2 \times 10^{-3}/s$,
 Cooling rate: $3^{\circ}C/s$)

Trial number	T _{test} (°C)	F _{max} (kN)	D _F (mm)	RA (%)	Remark
E/S2	895	17.51	17.2	30	
D/S2	1007	9.98	15.6	43	
C/S2	1108	6.53	11.1	71	
B/S2	1203	4.75	14.0	54	
A/S2	1308	3.20	18.9	16	
H/S2	1312	2.63	20.0	6	
I/S2	1316	2.47			ZDT
G/S2	1325	2.35			
F/S2	1329	2.54			
J/S2	1355	1.24			
K/S2	1360	0.90			
L/S2	1380	0.86			
M/S2	1388	0.00			ZST

Table A2-7 Data of hot tensile test of steel grade
 AISI O1, group O1-3 (Strain rate: $2 \times 10^{-2}/s$,
 Cooling rate: $0.5^{\circ}C/s$)

Trial number	T _{test} (°C)	F _{max} (kN)	D _F (mm)	RA (%)	Remark
IV/S2	900	23.54	14.4	51	
III/S2	1003	12.66	9.2	80	
II/S2	1102	10.09	1.7	99	
I/S2	1207	6.15	18.3	21	
VI/S2	1224	5.37	20.3	3	
V/S2	1230	4.97			ZDT
VII/S2	1308	3.27			
IX/S2	1377	0.60			
X/S2	1388	0.48			
XI/S2	1400	0.39			
XII/S2	1405	0.00			ZST

Table A2-8 Data of hot tensile test of steel grade
 AISI 01, group 01-4 (Strain rate: $2 \times 10^{-2}/s$,
 Cooling rate : $3^{\circ}C/s$)

Trial number	T _{test} (°C)	F _{max} (kN)	D _F (mm)	RA (%)	Remark
B1/S2	894	19.50	17.4	29	
A1/S2	998	12.80	14.2	53	
C1/S2	1103	9.95	10.8	73	
D1/S2	1205	6.63	16.0	40	
F1/S2	1264	4.78	19.1	14	
G1/S2	1275	4.39			ZDT
E1/S2	1304	3.84			
H1/S2	1356	1.65			
I1/S2	1367	0.93			
K1/S2	1387	0.74			
J1/S2	1395	0.00			ZST

VITA

Mr. Sakhob Khumkoa was born in Khonkaen, Thailand on May 22, 1972. He received his certificate of high school in Namphong Suksa School, Khonkean, in 1990. He received his Bachelor Degree of Engineering in department of Metallurgical Engineering, faculty of Engineering, Chulalongkorn University in 1994. He was a student of Gradate School of Chulalongkorn University and began to study in the same department where he received Bachelor Degree of Engineering since academic year 1995.