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APPENDICES

APPENDIX A EXPERIMENTAL DATA

Table A.1 Effect of oxygen partial pressure at total flow rate = 100 ml/minand applied voltage = 5,000 V

	%CH4 conv.	% O ₂ conv.	% Selectivity							
CH4:O2			СО	H_2	НСОН	CH ₃ OH	C ₂ -	C ²	C_2^{\blacksquare}	CO ₂
2:1	19.8	68.5	4.0	0	4.6	0	0	7.4	0	85.9
4:1	15.6	94.5	16.0	10.8	7.8	0	0	19.0	0	68.0
8:1	8.9	88.2	19.3	33.6	13.5	0.02	0	31.9	0	42.0

Table A.2 Effect of applied voltage at total flow rate = 100 ml/min and $CH_4:O_2 = 4:1$

			% Selectivity							
Applied Voltage (V)	%CH4 con	% O ₂ conv	CO	H_2	НСОН	СН ₃ ОН	C2	C ⁼	C₂ ≡	CO ₂
5000	15.6	94.5	16.0	10.8	7.8	0	0	19.0	0	68.0
6000	22.6	97.2	13.0	22.4	6.9	0.02	13.4	20.1	0	47.9
8000	22.7	93.9	12.4	22.5	6.6	0.01	13.7	22.1	0	43.5
10000	23.4	84.8	11.1	29.8	5.5	0.02	10.0	19.7	0	40.8

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Table A.3 Effect of total flow rate at $CH_4:O_2 = 4:1$ and applied voltage = 5,000 V

				% Selectivity								
Total	nv.	V.										
Flow	4 CO	2 COI			H	HC				2		
Rate	6CH	0%	CC	H_2	HCC	CH ₃ (C ₂	C ¹	C ³	CO		
(ml/min)	0	0.			H							
50	16.6	91.4	17.0	33.9	10.9	0.01	7.2	26.3	0	52.5		
100	15.6	94.5	16.0	10.8	7.8	0	0	19.0	0	68.0		
150	12.1	69.6	13.0	6.8	7.4	0	0	18.0	0	60.2		
200	11.5	76.2	5.2	0	5.6	0	0	10.3	0	73.8		

Table A.4 Effect of oxygen partial pressure on non-catalytic system at totalflow rate = 100 ml/min and applied voltage = 5,000 V

-	%CH ₄ conv.	% O ₂ conv.	% Selectivity							
CH ₄ :O ₂			СО	H_2	НСОН	CH ₃ OH	C2 ⁻	C. =	C ²	CO2
2:1	48.6	46.9	34.5	52.6	2.2	0	12.0	37.2	9.1	9.9
4:1	35.4	56.6	26.6	59.0	4.6	0.01	18.7	30.8	10.4	9.9
8:1	27.3	53.0	11.2	55.1	5.9	0.01	22.5	19.3	12.2	12.4

APPENDIX B

ASSUMPTIONS, DEFINITIONS AND CALCULATIONS

To facilitate the calculations, some valid assumptions were made as follows:

- 1. All the gaseous behaviors obey the ideal gas law.
- 2. Pressure drop across the system is very small and can be negligible.
- 3. The pressure in the system equals atmospheric pressure (1 atm).
- 4. The flow rate change across the reactor due to the variation in the gaseous compositions during the reaction time is very small and can be negligible.

The total molar flow rate of the gaseous stream can be determined from the following equation:

$$N = q \times (P/RT) \tag{B.1}$$

where

q = total volumetric flow rate

P = total pressure of the system

R = gas constant (82.051 atm·ml·mol⁻¹·min⁻¹·K⁻¹)

T = absolute ambient temperature (K)

The molar flow rate of each component can be obtained by multiplying its fraction derived from the gas chromatography analysis with the total molar flow rate.

The conversion is defined as:

% Conversion = (Mole reactant in – Mole reactant out) \times 100 (B.2)

Mole reactant in

The selectivity of each product is defined on the basis of the amount of carbon converted from the reactant into the specified products. The product selectivity is defined as follows:

% C_P Selectivity =
$$P \times Mole \text{ of } C_P \text{ produced } \times 100$$
 (B.3)
 $R \times Mole \text{ of } C_R \text{ converted}$

where

P = number of carbon atom in product R = number of carbon atom in reactant C_P = product that has carbon P atom C_R = reactant that has carbon R atom

The selectivity of Hydrogen is defined as follows:

% H₂ Selectivity = Mole of H₂ produced × 100 (B.4) $2 \times Mole of CH_4 converted$

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