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APPENDICES

APPENDIX A

CALCULATION FOR CATALYST PREPARATION

Calculation for the preparation of cobalt loading catalyst

Preparation of Co/Al₂O₃ with different Co loadings (5, 10, 15, and 20 wt%) by the incipient wetness impregnation method are shown as follows:

Reagent:- Cobalt (II) nitrate hexahydrate (Co(NO3)2 · 6H2O)Molecular weight= 290.93 g/mol- Support:- Solvothermal synthesized-alumina support

Calculation:

5% Co/Al₂O₃

Based on 100 g of catalyst used, the composition of the catalyst will be as follows:

Cobalt = 5 gAlumina = 100-5 = 95 g

For 2 g of alumina

Cobalt required = $2 \times (5/95)$ = 0.11 g

Cobalt 0.11 g was prepared from $Co(NO_3)_2 \cdot 6H_2O$ and molecular weight of Co is 58.93

 $Co(NO_3)_2 \cdot 6H_2O \text{ required} = \frac{MW \text{ of } Co(NO_3)_2 \cdot 6H_2O \times \text{ cobalt required}}{MW \text{ of } Co}$ $= (290.93/58.93) \times 0.11 = 0.54 \text{ g}$

Since the pore volume of the alumina support is 2.0 ml/g, 1.8 ml/g, 1.6 ml/g, and 1.3 ml/g for alumina support prepared with AIP 10 g, 15 g, 25 g, and 35 g, respectively. Thus, the total volume of impregnation solution which must be used is 4 ml for alumina support prepared with AIP 10 g, 3.6 ml for alumina support prepared with AIP 15 g, 3.2 ml for alumina support prepared with AIP 25 g, and 2.6 ml for alumina support prepared with AIP 35 g by the requirement of incipient wetness

impregnation method, the de-ionized water is added until equal pore volume for dissolve Cobalt (II) nitrate hexahydrate.

The others cobalt loading (10, 15, and 20 wt%) are calculated in the same method with calculation for 5% Co/Al_2O_3 .

Calculation for the preparation of iron loading catalyst (Based catalyst)

Preparation of 1%Cu/20%Fe/Al₂O₃ by the sequential incipient wetness impregnation method is shown as follows:

Reagent:	- Iron (III) nitrate nonahydrate (Fe(NO ₃) ₃ . 9H ₂ O)		
	Molecular weight = 403.99 g/mol		
	- Copper (II) nitrate trihydrate (Cu(NO ₃) ₂ . 3H ₂ O)	
	Molecular weight = 241.60 g/mol		
	- Support: - Commercial γ-alumina support		

Calculation:

1%Cu/20%Fe/Al₂O₃

Based on 100 g of catalyst used, the composition of the catalyst will be as follows:

Iron	=	20 g		
Copper	=	l g		
Alumina	=	100-20-1	=	79 g

For 5 g of alumina

Iron required	=	5×(20/79)	=	1.27 g
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Iron 1.27 g was prepared from $Fe(NO_3)_3$. $9H_2O$ and molecular weight of Fe is 55.847

 $Fe(NO_3)_3 \cdot 9H_2O \text{ required} = \frac{MW \text{ of } Fe(NO_3)_3 \cdot 9H_2O \times \text{ iron required}}{MW \text{ of } Fe}$ $= (403.99/55.847) \times 1.27 = 9.19 \text{ g}$

Copper required = $5 \times (1/79)$ = 0.063 g Copper 0.063 g was prepared from Cu(NO₃)₂. 3H₂O and molecular weight of Cu is 63.546

 $Cu(NO_3)_2 \cdot 3H_2O \text{ required} = \frac{MW \text{ of } Cu(NO_3)_2 \cdot 3H_2O \times \text{ iron required}}{MW \text{ of } Cu}$ $= (241.60/63.546) \times 0.063 = 0.24 \text{ g}$

Since the pore volume of the alumina support is 1.0 ml/g for commercial γ alumina support. Thus, the total volume of impregnation solution which must be used is 5 ml for commercial γ -alumina support by the requirement of incipient wetness impregnation method, the de-ionized water is added until equal pore volume for dissolve Iron (III) nitrate nonahydrate and Copper (II) nitrate trihydrate.

Calculation for the preparation of Cu-modified alumina iron loading catalyst

Preparation of Cu-modified alumina having 10 wt% of Cu by the incipient wetness impregnation method is shown as follows:

Reagent:	- Copper (II) nitrate trihydrate (Cu(NO ₃) ₂ . 3H ₂ O)
	Molecular weight = 241.60 g/mol
	- Support: - Commercial γ-alumina support

Calculation:

10% Cu/Al₂O₃

Based on 100 g of catalyst used, the composition of the catalyst will be as follows:

Copper	=	10 g		
Alumina	=	100-10	=	90 g

For 5 g of alumina

Copper required = $5 \times (10/90)$ = 0.55 g

Copper 0.55 g was prepared from $Cu(NO_3)_2$. $3H_2O$ and molecular weight of Cu is 63.546

$$Cu(NO_3)_2 \cdot 3H_2O \text{ required} = \frac{MW \text{ of } Cu(NO_3)_2 \cdot 3H_2O \times \text{ copper required}}{MW \text{ of } Cu}$$
$$= (241.60/63.546) \times 0.55 = 2.09 \text{ g}$$

Since the pore volume of the alumina support is 1.0 ml/g for commercial γ alumina support. Thus, the total volume of impregnation solution which must be used is 5 ml for commercial γ -alumina support by the requirement of incipient wetness impregnation method, the de-ionized water is added until equal pore volume for dissolve Copper (II) nitrate trihydrate.

Preparation of Cu-modified alumina iron loading catalysts by the incipient wetness impregnation method is shown as follows:

- 1%Cu-promoted 20%Fe/10%Cu/Al₂O₃

Reagent:	- Iron (III) nitrate nonahydrate (Fe(NO ₃) ₃ . 9H ₂ O)		
	Molecular weight = 403.99 g/mol		
	- Copper (II) nitrate trihydrate (Cu(NO ₃) ₂ . $3H_2O$)		
	Molecular weight = 241.60 g/mol		
	- Support: - 10% Cu/Al ₂ O ₃		

Calculation:

1%Cu/20%Fe/10%Cu/Al₂O₃

Based on 100 g of catalyst used, the composition of the catalyst will be as follows:

Iron	=	20 g		
Copper	=	1 g		
10%Cu/Al ₂ O	3 =	100-20-1	=	79 g

For 5 g of 10%Cu/Al₂O₃

Iron required = $5 \times (20/79)$ = 1.27 g

.

Iron 1.27 g was prepared from $Fe(NO_3)_3$. $9H_2O$ and molecular weight of Fe is 55.847

$$Fe(NO_3)_3 \cdot 9H_2O \text{ required} = MW \text{ of } Fe(NO_3)_3 \cdot 9H_2O \times \text{ iron required}$$

$$MW \text{ of } Fe$$

$$= (403.99/55.847) \times 1.27 = 9.19 \text{ g}$$
Copper required = $5 \times (1/79) = 0.063 \text{ g}$
Copper 0.063 g was prepared from Cu(NO₂)₂ = 3H₂O and molecular weight

Copper 0.063 g was prepared from $Cu(NO_3)_2$. $3H_2O$ and molecular weight of Cu is 63.546

$$Cu(NO_3)_2 \cdot 3H_2O \text{ required} = \frac{MW \text{ of } Cu(NO_3)_2 \cdot 3H_2O \times \text{ iron required}}{MW \text{ of } Cu}$$
$$= (241.60/63.546) \times 0.063 = 0.24 \text{ g}$$

The de-ionized water is added until equal pore volume of 10%Cu/Al₂O₃ for dissolve Iron (III) nitrate nonahydrate and Copper (II) nitrate trihydrate.

- 20%Fe/10%Cu/Al₂O₃ (without 1%Cu-promoted)

Reagent:	- Iron (III) nitrate nonahydrate (Fe(NO ₃) ₃ . 9H ₂ C			
	Molecular weight = 403.99 g/mol			
	- Support: - 10% Cu/Al ₂ O ₃			

Calculation:

20%Fe/10%Cu/Al₂O₃

Based on 100 g of catalyst used, the composition of the catalyst will be as follows:

Iron = 20 g $10\% \text{Cu/Al}_2\text{O}_3 = 100-20 = 80 \text{ g}$

For 5 g of 10%Cu/Al₂O₃

Iron required = $5 \times (20/80)$ = 1.25 g

Iron 1.25 g was prepared from $Fe(NO_3)_3$. $9H_2O$ and molecular weight of Fe is 55.847

$$Fe(NO_3)_3 \cdot 9H_2O \text{ required} = MW \text{ of } Fe(NO_3)_3 \cdot 9H_2O \times \text{ iron required}$$
$$MW \text{ of } Fe$$
$$= (403.99/55.847) \times 1.25 = 9.04 \text{ g}$$

The de-ionized water is added until equal pore volume of 10%Cu/Al₂O₃ for dissolve Iron (III) nitrate nonahydrate.

APPENDIX B

CALCULATION OF BET SURFACE AREA BY THE SINGLE POINT METHOD

From Brunauer-Emmett-Teller (BET) equation:

$$\frac{X}{V(1-X)} = \frac{1}{VmC} + \frac{(C-1)X}{VmC}$$
(B.1)

Where: X = relative partial pressure of N₂, P/P_o

- P_o = saturated vapor pressure of N_2 (or adsorbed gas) at the experimental temperature
- $P = equilibrium vapor pressure of N_2$
- V = volume of gas adsorbed at a pressure P; ml at the NTP/ g of sample
- V_m = volume of gas adsorbed at monolayer, ml. at the NTP / g of sample

$$C = constant$$

Assume $C \rightarrow \infty$, then

$$\frac{X}{V(1-X)} = \frac{X}{Vrr}$$

$$Vrr = V(1-P/P_0)$$
(B.2)

From the gas law,

$$\frac{P_b V}{273} = \frac{P_t V}{T}$$
(B.3)

Where: V = constant volume P_b = pressure at 0 °C P_t = pressure at t °C T = 273.15 + t, K $P_t = 1$ atm and thus, $P_b = (273.15 / T)$

Partial pressure of Nitrogen:

$$P = \frac{[Flow of (He+N_2) - Flow of He]}{Flow of (He+N_2)}$$

$$= 0.3 \text{ atm}$$
(B.4)

 N_2 saturated vapor pressure, $P_0 = 1.1$ atm

$$p = P / P_o = P / 1.1 = 0.3 / 1.1 = 0.2727$$

How to measure V



$$V = \frac{S_2}{S_1} \times \frac{1}{W} \times \frac{273.15}{T} \quad \text{ml. / g of catalyst} \quad (B.5)$$

Where, S_1 = Nitrogen 1 ml/1 atm of room temperature area S_2 = Desorption of nitrogen area W = Weight of the sample (g) T = Room temperature (K)

Therefore,

$$Vm = \frac{S_2}{S_1} \times \frac{1}{W} \times \frac{273.15}{T} \times (1-p)$$
$$Vm = \frac{S_2}{S_1} \times \frac{1}{W} \times \frac{273.15}{T} \times 0.7273 \quad (B.6)$$

Surface area of catalyst:

S =
$$\frac{N\sigma V_m}{M}$$

Where, N = Avogadro number =
$$6.02 \times 10^{23}$$

 σ = area occupied by one molecule of adsorbed nitrogen = 16.2×10^{-20}
M = volume of one mole nitrogen = $22410 \text{ cm}^3/\text{mol}$

Then,

$$S = 4.352 \text{ Vm}$$

$$S = \frac{S_2}{S_1} \times \frac{1}{W} \times \frac{273.15}{T} \times 0.7273 \times 4.352$$

$$S = \frac{S_2}{S_1} \times \frac{1}{W} \times \frac{273.15}{T} \times 3.1582 \quad (B.7)$$



APPENDIX C

CALCULATION FOR TOTAL H₂ CHEMISORPTION AND DISPERSION

Calculation of the total H_2 chemisorption and metal dispersion of the catalyst, a stoichiometry of H/Co = 1, measured by H_2 chemisorption is as follows:

Let the weight of catalyst used		=	W	g
Integral area of H ₂ peak after adsorp	otion	=	А	unit
Integral area of 45 μ l of standard H ₂	peak	=	В	unit
Amounts of H ₂ adsorbed on catalyst		=	B-A	unit
Concentration of Co (by AAS)		=	С	% wt
Volume of H_2 adsorbed on catalyst		=	45×[(B-A)/B]	μl
Volume of 1 mole of H_2 at $100^{\circ}C$		=	28.038	μl
Mole of H_2 adsorbed on catalyst		=	[(B-A)/B]×[45/28.038]	μmole
Total hydrogen chemisorption	= [(B-	A)/B	×[45/28.038]×[1/W] μm	ole /g of catalyst
	=	Ν	µmole /g of catalyst	
Molecular weight of cobalt		=	58.93	
Metal dispersion (%)		=	2×H _{2 tot} /g of catalyst>	<100
			No µmole Cotot/g of c	atalyst
		=	2×N×100	
			No µmole Cotot	
		=	2×N×58.93×100	
			C×10 ⁶	
		=	1.179× N	
			C	

APPENDIX D

*

CALCULATION FOR TOTAL CO CHEMISORPTION

Calculation of the total CO chemisorption of the catalyst, a stoichiometry of CO/Fe = 1, measured by CO chemisorption is as follows:

Let the weight of catalyst used		=	W	g
Integral area of CO peak after adsorption of CO peak after	otion	=	А	unit
Integral area of 50 μ l of standard H ₂	peak	=	В	unit
Amounts of CO adsorbed on catalys	t	=	B-A	unit
Concentration of Fe (by AAS)		=	С	% wt
Volume of CO adsorbed on catalyst		=	50×[(B-A)/B]	μl
Volume of 1 mole of CO at 50°C		=	24.86	μl
Mole of CO adsorbed on catalyst		=	[(B-A)/B]×[50/24.86]	μmole
Total CO chemisorption	=[(B-	A)/B	s]×[50/24.86]×[1/W] μmo	ole/g of catalyst
	=	Ν	umole /g of catalyst	

µmole /g of catalyst Ν

APPENDIX E

CALIBRATION CURVES

CO hydrogenation reaction

This appendix showed the calibration curves for calculation of composition of reactant and products in CO hydrogenation reaction. The reactant is CO and the main product is methane. The other products are linear hydrocarbons of heavier molecular weight that are C_2 - C_4 such as ethane, ethylene, propane, propylene and butane.

The thermal conductivity detector, gas chromatography Shimadzu model 8A was used to analyze the concentration of CO by using Molecular sieve 5A column. The chromatograms of catalyst sample are shown in Figure E.1.

The VZ10 column are used with a gas chromatography equipped with a flame ionization detector, Shimadzu modal 14B, to analyze the concentration of products including of methane, ethane, ethylene, propane, propylene and butane. The chromatograms of catalyst sample are shown in Figure E.2. Conditions uses in both GC are illustrated in Table E.1.

Mole of reagent in y-axis and area reported by gas chromatography in x-axis are exhibited in the curves. The calibration curves of CO, methane, ethane, ethylene, propane, propylene and butane are illustrated in the following figures. s may set a subsection of the set of the set



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11 13 13	1130	diff fe	N KIR	12.121 4	1、跨設	N 114
1	0.045	1.6	÷		(1, 1)(1)	
1	1.02	5430	1919		0. 1017	
1	1. 30 2	56.548	be, del		5.7351	
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	1. 111	11110	29.5		1.03463	
• _T .	8, 115	118424	3184		15.7189	
3.4 9	16: 108	1:11:	711		0.9111	
	liii Vi	15 7 13 12	111,81		100	



Figure E.1 The chromatograms of catalyst sample from thermal conductivity detector, gas chromatography Shimadzu model 8A (Molecular sieve 5A column).

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Figure E.2 The chromatograms of catalyst sample from flame ionization detector, gas chromatography Shimadzu modal 14B (VZ10 column).

Cone	dition
Shimadzu GC-8A	Shimadzu GC-14B
5	5
50	50
0	0
10	10
0	0
50	60
0	0
2	2
41	41
1	1
100	100
1	1
	Cond Shimadzu GC-8A 5 50 0 10 0 50 0 50 0 2 41 1 1 100 1

 Table E.1 Conditions use in Shimadzu modal GC-8A and GC-14B.



Figure E.3 The calibration curve of CO.



Figure E.4 The calibration curve of methane.



Figure E.5 The calibration curve of ethane.



Figure E.6 The calibration curve of ethylene.



Figure E.7 The calibration curve of propane.



Figure E.8 The Calibration curve of propylene.



Figure E.9 The calibration curve of butane.

Fischer-Tropsch Synthesis reaction

This appendix showed the calibration curves for calculation of composition of reactant and products in FTS reaction. The reactant is CO. The products are hydrocarbons of $C_1-C_7^+$ (such as methane, ethane, ethylene, propane, propylene, butane, butene, pentane, pentene, hexane, hexene, heptane, and heptene) and CO_2 .

Analysis of CO and CO₂ were performed in a Carbosphere 80/100 6' x 1/8'' x 0.085'' SS packed column using a thermal conductivity detector. Analysis of hydrocarbon was carried out in a AT-Q 30m x 0.53 mm Heliflex capillary column using a flame ionization detector.

Mole of reagent in y-axis and area reported by gas chromatography in x-axis are exhibited in the curves. The calibration curves of CO, methane, ethane, ethylene, propane, propylene and butane are illustrated in the following figures.



Figure E.10 The calibration curve of CO.



Figure E.11 The calibration curve of CO₂.



Figure E.12 The calibration curve of methane.



Figure E.13 The calibration curve of ethane.



Figure E.14 The calibration curve of ethylene.



Figure E.15 The calibration curve of propane.



Figure E.16 The Calibration curve of propylene.



Figure E.17 The calibration curve of butane.



Figure E.18 The calibration curve of butene.



Figure E.19 The calibration curve of pentane.



Figure E.20 The calibration curve of pentene.



Figure E.21 The calibration curve of hexane.



Figure E.22 The calibration curve of hexene.



Figure E.23 The calibration curve of heptane.



Figure E.24 The calibration curve of heptene.

APPENDIX F

CALCULATION OF CO CONVERSION, REACTION RATE, TOF, AND SELECTIVITY

The catalyst performance for the CO hydrogenation and FTS were evaluated in terms of activity for CO conversion, reaction rate, TOF, and selectivity.

CO conversion

Activity of the catalyst performed in term of carbon monoxide conversion and reaction rate. Carbon monoxide conversion is defined as moles of CO converted with respect to CO in feed:

$$\frac{\text{CO conversion (\%)}}{\text{mole of CO in feed}} = \frac{100 \times [\text{mole of CO in feed}]}{\text{mole of CO in feed}}$$
(i)

where mole of CO can be measured employing the calibration curve of CO in Figure E.3 (for CO hydrogenation) and E.10 (for FTS reaction), Appendix E., i.e.,

For CO hydrogenation:

mole of CO = (area of CO peak from integrator plot on GC-8A) $\times 3 \times 10^{-11}$ (ii)

Reaction rate

Reaction rate was calculated from CO conversion that is as follows:

For example, the reaction rate from CO hydrogenation can be calculated as:

Let the weight of catalyst used		W	g
Flow rate of CO	=	8	cc/min
Reaction time	=	60	min

	·	W×22400					
Reaction rate (g CH ₂ /g of catalyst/h)	=	[% conversion of CO/100]×60×14×8					(iii)
Volume of 1 mole of gas at 1 atm		=		22400		сс	
Weight of CH ₂		=		14		g	

<u>TOF</u>

TOF was calculated from reaction rate and H_2 chemisorption (Or CO chemisorption) that is as follows:

$$TOF (s^{\cdot 1}) = \frac{[reaction rate]}{[H_2 chemisorption/2]}$$
(in case of H₂ chemisorption) (iv)
$$= \frac{[reaction rate]}{[CO chemisorption]}$$
(in case of CO chemisorption) (v)

Selectivity

Selectivity of product is defined as mole of product (B) formed with respect to mole of CO converted:

Selectivity of B (%) =
$$100 \times [mole of B formed/mole of total products]$$
 (vi)

Where B is product, mole of B can be measured employing the calibration curve of products such as methane, ethane, ethylene, propane, propylene, butane, butene, pentane, pentene, hexane, hexene, heptane, and heptene in Figure E.4-E.9 (for CO hydrogenation) and E.12-E.24 (for FTS reaction), Appendix E., i.e.,

For CO hydrogenation:

mole of CH₄ = (area of CH₄ peak from integrator plot on GC-14B)×
$$6 \times 10^{-13}$$
 (vii)

APPENDIX G

LIST OF PUBICATIONS

- Kamonchanok Pansanga, Okorn Mekasuwandumrong, Joongjai Panpranot, and Piyasan Praserthdam, "Synthesis of Nanocrystalline Alumina by Thermal Decomposition of Aluminum Isopropoxide in 1-Butanol and their Applications as Cobalt Catalyst Supports", Kor. J. Chem. Eng., In Press, Corrected Proof.
- Kamonchanok Pansanga, Joongjai Panpranot, Okorn Mekasuwandumrong, Chairit Satayaprasert, James G. Goodwin, Jr., and Piyasan Praserthdam, "Effect of Mixed γ and χ Crystalline Phases in Nanocrystalline Al₂O₃ on the Dispersion of Cobalt on Al₂O₃", Catal. Commun., Revised.
- Kamonchanok Pansanga, Nattaporn Lohitharn, Andrew C. Y. Chien, Edgar Lotero, Joongjai Panpranot, James G. Goodwin, Jr., and Piyasan Praserthdam, "Copper-Modified Alumina as a Support for Iron Fischer Tropsch Synthesis Catalysts", Catal. Lett., Submitted.

VITAE

Miss Kamonchanok Pansanga was born on 23th March 1981, in Samutsongkhram, Thailand. She received her Bachelor degree of Engineering with Chemical Engineering from King Mongkut's Institute of Technology Ladkrabang, Thailand in March 2003. Since June 1, 2003, she has been studying for her Doctor degree of Engineering from the department of Chemical Engineering, Chulalongkorn University.

