

REFERENCES

- Ahmed, T. (2012). Reservoir Engineering Handbook 4th ed.
- Al-adasani, A. and Bai, B. (2010) Recent developments and updated screening criteria of enhanced oil recovery techniques. Paper presented at the International Oil and Gas Conference and Exhibition in China, Beijing, China.
- Al-Harbi, A.S., Ghedan, S.G., Brantferger, K.M. and Kompanik, G. (2012) Can simulation models validated with waterflooding data reliably predict three phase flow processes of gas and WAG flooding? Paper presented at the Abu Dhabi International Petroleum Conference and Exhibition, Abu Dhabi, UAE.
- Alajmi, A.F., Gharbi, R. and Algharaib, M. (2009) Performance of hot water injection in heterogenous reservoirs using multilateral wells. Paper presented at the SPE Saudi Arabia Section Technical Symposium, AlKhobar, Saudi Arabia.
- Altunina, L. (2006) Improved cyclic-Steam well treatment with employing thermoreversible polymer gels. Paper presented at the SPE Russian Oil and Gas Technical Conference and Exhibition, Moscow, Russia.
- Anderson, W.G. (1987) Wettability literature survey-Part 6: the effects of wettability on waterflooding. SPE Journal of Petroleum Technology, 39(12), 1605-1622.
- Bahlani, A.M.M.A. and Babadagli, T. (2008) A critical review of the status of SAGD: where are we and what is next? Paper presented at the SPE Western Regional and Pacific Section AAPG Joint Meeting, Bakersfield, California, USA.
- Bahonar, M., Ataei, A., Masoudi, R. and Mirkalei, S.M.M. (2007) Evaluation of steam injection in a fractured heavy-oil carbonate reservoir in Iran. Paper presented at the SPE Middle East Oil and Gas Show and Conference, Kingdom of Bahrain.

- Bai, B., Liu, Y., Coste, J.-P. and Li, L. (2007) Preformed particle gel for conformance control: transport mechanism Through Porous Media. SPE Reservoir Evaluation & Engineering, 10(2), 176-184.
- Belgrave, J.D.M. and Win, T. (1993) Vertical sweep efficiency and oil recovery from gas injection in heterogeneous horizontal reservoirs. Paper presented at the SPE Western Regional Meeting, Anchorage, Alaska.
- Bouabboune, M., Hammouch, N. and Benhadid, S. (2006) Comparison between micro-emulsion and surfactant solution flooding efficiency for enhanced oil recovery in tinFouye oil field. Paper presented at the Canadian International Petroleum Conference, Calgary, Alberta.
- Brashear, J.P. and Kuuskraa, V.A. (1978) The potential and economics of enhanced oil recovery. SPE Journal of Petroleum Technology, 30(9), 1231-1239.
- Callaway, F.H. (1959) Evaluation of Waterflood Prospects.
- Craig, F.F.J. (1971) The reservoir engineering aspects of waterflooding. Paper presented at the Society of Petroleum Engineers., Dallas, Texas.
- Crawford, P.B. and Collins, R.E. (1954) Estimated Effect of Vertical Fractures on Secondary Recovery.
- Das, S.K. (1998) Vapex: An efficient process for the recovery of heavy oil and bitumen. SPE Journal, 3(3), 232-237.
- Derakhshanfar, M., Nasehi, M. and Asghari, K. (2012) Simulation study of CO₂-assisted waterflooding for enhanced heavy oil recovery and geological storage. Paper presented at the Carbon Management Technology Conference, Orlando, Florida, USA.
- Dong, M., Wu, Y. and Li, A. (2011) Sweep efficiency improvement by alkaline flooding for pelican lake heavy oil. Paper presented at the Canadian Unconventional Resources Conference, Alberta, Canada.
- Dong, X., Liu, H., Zhang, H. and Pang, Z. (2011) Flexibility research of hot-water flooding followed steam injection in heavy oil reservoirs. Paper presented at the SPE Enhanced Oil Recovery Conference, Kuala Lumpur, Malaysia.
- Doorwar, S. and Mohanty, K.K. (2011) Viscous fingering during non-thermal heavy oil recovery. Paper presented at the SPE Annual Technical Conference and Exhibition, Denver, Colorado, USA.

- Fadaei, H., Debenest, G., Kamp, A.M., Quintard, M. and Renard, G. (2010) How the in-situ combustion process works in a fractured system: 2D core- and block-scale simulation. SPE Reservoir Evaluation & Engineering, 13(1), 118-130.
- Fatemi, S.M., Ghotbi, C., Kharrat, R. and Badakhshan, A.-. (2011) Application of Toe-to-Heel air injection (THAI) process in fractured carbonate systems: 3D simulation of the effect of fractures geometrical properties, reservoir and operational parameters. Paper presented at the SPE EUROPEC/EAGE Annual Conference and Exhibition, Vienna, Austria.
- Feng, A., Zhang, G., Ge, J., Jiang, P., Pei, H., Zhang, J. and Li, R. (2012) Study of surfactant-polymer flooding in heavy oil reservoirs. Paper presented at the SPE Heavy Oil Conference Canada, Calgary, Alberta, Canada.
- Gao, C.H. (2011) Advances of polymer flood in heavy oil recovery. Paper presented at the SPE Heavy Oil Conference and Exhibition, Kuwait City, Kuwait.
- Ghoodjani, E., Kharrat, R., Vossoughi, M. and Bolouri, S.H. (2012) A review on thermal enhanced heavy oil recovery from fractured carbonate reservoirs. Paper presented at the SPE Heavy Oil Conference Canada, Calgary, Alberta, Canada.
- Gogarty, W.B. (1976) Status of surfactant or micellar methods. SPE Journal of Petroleum Technology, 28(1), 93-102.
- Gogarty, W.B. (1978) Micellar/polymer flooding an overview. SPE Journal of Petroleum Technology, 30(8), 1089-1101.
- Gogarty, W.B. and Tosch, W.C. (1968) Miscible-Type Waterflooding: Oil Recovery with Micellar Solutions.
- Haghighi, M.B., Ayatollahi, S. and Shabaninejad, M. (2012) Comparing the performance and recovery mechanisms for steam flooding in heavy and light oil reservoirs. Paper presented at the SPE Heavy Oil Conference Canada, Calgary, Alberta, Canada.
- Hascakir, B., Castanier, L.M. and Kovscek, A.R. (2010) In-situ combustion dynamics visualized with X-ray computed tomography. Paper presented at the SPE Annual Technical Conference and Exhibition, Florence, Italy.

- Heller, J.P. and Taber, J.J. (1986) Influence of reservoir depth on enhanced oil recovery by CO₂ flooding. Paper presented at the Permian Basin Oil and Gas Recovery Conference, Midland, Texas.
- Holm, L.W. (1976) Status of CO₂ and hydrocarbon miscible oil recovery methods. SPE Journal of Petroleum Technology, 28(1), 76-84.
- Holm, L.W. (1986) Miscibility and Miscible Displacement.
- Holm, W.L. (1987) Evolution of the carbon dioxide flooding processes. SPE Journal of Petroleum Technology, 39(11), 1337-1342.
- Howes, B.J. (1988) Enhanced oil recovery in Canada: success in progress. Journal of Canadian Petroleum Technology, 27(6).
- Issever, K. and Topkaya, I. (1998) Use of Carbon Dioxide to Enhance Heavy Oil Recovery.
- Jadhunandan, P.P. and Morrow, N.R. (1991) Spontaneous imbibition of water by crude oil/brine/rock systems. Petroleum Recovery Research Center, 15(4), 319-346.
- Jadhunandan, P.P. and Morrow, N.R. (1995) Effect of wettability on waterflood recovery for crude-oil/brine/rock systems. SPE Reservoir Engineering, 10(1), 40-46.
- James, L.A. and Chatzis, I. (2007) Mass transfer coefficients in vapour extraction (VAPEX). Paper presented at the Canadian International Petroleum Conference, Calgary, Alberta.
- Jha, K.N. (1985) A laboratory study of heavy oil recovery with carbon dioxide. Paper presented at the Technical Meeting / Petroleum Conference Of The South Saskatchewan Section, Regina, Canada.
- Johns, R.T. and Orr, J., F.M. (1996) Miscible gas displacement of multicomponent oils. SPE Journal, 1(1), 39-50.
- Joshi, S.D. (1991) Thermal oil recovery with horizontal wells. Journal of Petroleum Technology, 43(11), 1302-1304.
- Kamath, V.A., Sinha, S. and Hatzignatiou, D.G. (1993) Simulation study of steam-assisted gravity drainage process in ugnu tar sand reservoir. Paper presented at the SPE Western Regional Meeting, Anchorage, Alaska.

- Kang, X., Zhang, J., Sun, F., Zhang, F., Feng, G., Yang, J. and Xiang, W. (2011) A review of polymer eor on offshore heavy oil field in bohai bay. Paper presented at the SPE Enhanced Oil Recovery Conference, Kuala Lumpur, Malaysia.
- Khatib, A.K., Earlougher, R.C. and Kantar, K. (1981) co₂ injection as an immiscible application for enhanced recovery in heavy oil reservoirs. Paper presented at the SPE California Regional Meeting, Bakersfield, California.
- Kumar, M., Sahni, A., Alvarez, J.M., Heny, C., Vaca, P., Hoadley, S.F. and Portillo, M. (2001) Evaluation of ior methods for the boscán field. Paper presented at the SPE International Thermal Operations and Heavy Oil Symposium, Porlamar, Margarita Island, Venezuela.
- Liu, Q., Dong, M. and Ma, S. (2006) Alkaline/surfactant flood potential in western canadian heavy oil reservoirs. Paper presented at the SPE/DOE Symposium on Improved Oil Recovery, Tulsa, Oklahoma, USA.
- Mai, A., Bryan, J., Goodarzi, N. and Kantzas, A. (2009) Insights into non-thermal recovery of heavy oil. Journal of Canadian Petroleum Technology, 48(3), 27-35.
- Mai, A. and Kantzas, A. (2010) Mechanisms of heavy oil recovery by low rate waterflooding. Journal of Canadian Petroleum Technology, 49(3), 44-50.
- Mohanty, K.K., Masino, W.H., Ma, T.D. and Nash, L.J. (1995) Role of three-hydrocarbon-phase flow in a gas-displacement process. SPE Reservoir Engineering, 10(3), 214-221.
- Mondragon, J.J., Yang, Z., Ershaghi, I., Hara, P.S., Bailey, S. and Koerner, R. (2000) Post-steamflood reservoir management using a full-scale 3d deterministic thermal reservoir simulation model, wilmington field, california. Paper presented at the SPE/AAPG Western Regional Meeting, Long Beach, California.
- Morrow, N.R., Lim, H.T. and Ward, J.S. (1986) Effect of crude-oil-induced wettability changes on oil recovery. SPE Formation Evaluation, 1(1), 89-103.
- Mungan, N. (1991) An evaluation of carbon dioxide flooding. Paper presented at the SPE Western Regional Meeting, Long Beach, California.

- Nourozieh, H., Kariznovi, M., Abedi, J. and Chen, Z. (2009) A new approach to simulation of the boundary layer in the vapor extraction process. Paper presented at the Canadian International Petroleum Conference, Calgary, Alberta.
- Ordenez, A., Belgrave, J.D.M., Fernandez, F., Comas, J.C., Lobo, A. and Ramirez, H.B. (2012) ECO-GSAI "Gravity Stable Air Injection" pilot test, an enhanced oil recovery opportunity to be implemented in chichimene field - colombia. Paper presented at the SPE Improved Oil Recovery Symposium, Tulsa, Oklahoma, USA.
- Orr Jr., F.M., Silva, M.K. and Lien, C.-L. (1983) Equilibrium phase compositions of co₂/crude oil mixtures-part 2: comparison of continuous multiple-contact and slim-tube displacement tests. Society of Petroleum Engineers Journal, 23(2), 281-291.
- Oskouei, S.J.P., Moore, R.G., Maini, B.B. and Mehta, S.A. (2010) Feasibility of in-situ combustion in the mature sagd chamber. Paper presented at the Canadian Unconventional Resources and International Petroleum Conference, Calgary, Alberta, Canada.
- Pei, H., Zhang, G., Ge, J., Ding, L., Tang, M. and Zheng, Y. (2012) A comparative study of alkaline flooding and alkaline/surfactant flooding for zhuangxi heavy oil. Paper presented at the SPE Heavy Oil Conference Canada, Calgary, Alberta, Canada.
- Rafiee, M.M. and Ramazanian, M. (2011) Simulation study of enhanced gas recovery process using a compositional and a black oil simulator. Paper presented at the SPE Enhanced Oil Recovery Conference, Kuala Lumpur, Malaysia.
- Robertson, E.P. (2007) Low-salinity waterflooding to improve oil recovery-historical field evidence. Paper presented at the SPE Annual Technical Conference and Exhibition, Anaheim, California, U.S.A.
- Roebuck, I.F. (1987) Gas-Injection Pressure Maintenance in Oil Reservoirs. In Bradley, H.B. (Ed.), Petroleum Engineering Handbook. Richardson, Texas: SPE. (pp. (43-1)-(43-19)).

- Sayyafzadeh, M., Mamghaderi, A., Pourafshari, P. and Haghghi, M. (2011) A new method to forecast reservoir performance during immiscible and miscible gas-flooding via transfer functions approach. Paper presented at the SPE Asia Pacific Oil and Gas Conference and Exhibition, Jakarta, Indonesia.
- Shen, C. (2002) Limitations and potentials of in-situ combustion processes for heavy oil reservoirs . Paper presented at the Canadian International Petroleum Conference, Calgary, Alberta.
- Shen Pingping, Y.S., Deng Baorong, Song Jie and Shen Kuiyou (2005) Effects of sweep efficiency and displacement efficiency during chemical flooding on a heterogeneous reservoir. Effects of Sweep Efficiency and Displacement Efficiency During Chemical Flooding on a Heterogeneous Reservoir.
- Singh, S.P. and Kiel, O.G. (1982) Waterflood design (pattern, rate, and timing). Paper presented at the International Petroleum Exhibition and Technical Symposium, Beijing, China.
- Sobers, L., LaForce, T.C. and Blunt, M.J. (2010) Optimizing oil recovery and carbon dioxide storage in heavy oil reservoirs. Paper presented at the Trinidad and Tobago Energy Resources Conference, Port of Spain, Trinidad.
- Spivak, A. and Chima, C.M. (1984) Mechanisms of immiscible CO₂ injection in heavy oil reservoirs, wilmington field, CA. Paper presented at the SPE Enhanced Oil Recovery Symposium, Tulsa, Oklahoma.
- Stalkup, F.I. (1978) Carbon dioxide miscible flooding: past, present, and outlook for the future. SPE Journal of Petroleum Technology, 30(8), 1102-1112.
- Taber, J.J., Martin, F.D. and Seright, R.S. (1997) EOR screening criteria revisited part 2: applications and impact of oil prices. SPE Reservoir Evaluation & Engineering, 12(3), 199-206.
- Tang, G.Q. and Morrow, N.R. (1997) Salinity, temperature, oil composition, and oil recovery by waterflooding. SPE Reservoir Engineering, 12(4), 269-276.
- Thomas, S. and Ali, S.M.F. (1992) Micellar-polymer flooding: status and recent advances. Journal of Canadian Petroleum Technology, 31(8).
- Thomas, S., Scoular, J.R., Verkoczy, B. and Ali, S.M.F. (1999) Chemical methods for heavy oil recovery. Paper presented at the Technical Meeting / Petroleum Conference Of The South Saskatchewan Section, Regina.

- Trigos, E.M., Gonzales, A., Torres, J.M.P., MuC1oz, S. and Sierra, D.P.M. (2010) Feasibility study of applying steamflooding in a reservoir with high shale/sand: teca field. Paper presented at the Trinidad and Tobago Energy Resources Conference, Port of Spain, Trinidad.
- Ursenbach, M.G., Moore, R.G. and Mehta, S.A. (2010) Air injection in heavy oil reservoirs - a process whose time has come (again). Journal of Canadian Petroleum Technology, 49(1), 48-54.
- Wang, J. and Dong, M. (2009) Simulation of O/W emulsion flow in alkaline/surfactant flood for heavy oil recovery. Paper presented at the Canadian International Petroleum Conference, Calgary, Alberta.
- Wang, J., Dong, M. and Arhuoma, M. (2010) Experimental and numerical study of improving heavy oil recovery by alkaline flooding in sandpacks. Journal of Canadian Petroleum Technology, 49(3), 51-57.
- Wassmuth, F.R., Green, K., Arnold, W. and Cameron, N. (2009) Polymer flood application to improve heavy oil recovery at east bodo. Journal of Canadian Petroleum Technology, 48(2), 55-61.
- Wingen, N.V. and Melkonian, B.L. (1961) Review of California Waterflooding Operations.
- Wyatt, K., Pitts, M.J. and Surkalo, H. (2002) Mature waterfloods renew oil production by alkaline-surfactant-polymer flooding. Paper presented at the SPE Eastern Regional Meeting, Lexington, Kentucky.
- Yellig, W.F. and Metcalfe, R.S. (1980) Determination and prediction of co2 minimum miscibility pressures. SPE Journal of Petroleum Technology, 32(1), 160-168.
- Yildiz, H.O., Valat, M. and Morrow, N.R. (1999) Effect of brine composition on wettability and oil recovery of a prudhoe bay crude oil. Journal of Canadian Petroleum Technology, 38(1).
- Zhang, J., Ravikiran, R., Freiberg, D. and Thomas, C.P. (2012) ASP formulation design for heavy oil. Paper presented at the SPE Improved Oil Recovery Symposium, Tulsa, Oklahoma, USA.

Zheng, S. and Yang, D. (2013) Pressure maintenance and improving oil recovery by means of immiscible water-alternating-co₂ processes in thin heavy-oil reservoirs. SPE Reservoir Evaluation & Engineering. 16(1), 60-71.

APPENDICES

Appendix A Graphs from CMG Results

The following graphs that were generated from CMG Result are the relationship between recovery factor and pore volumes.

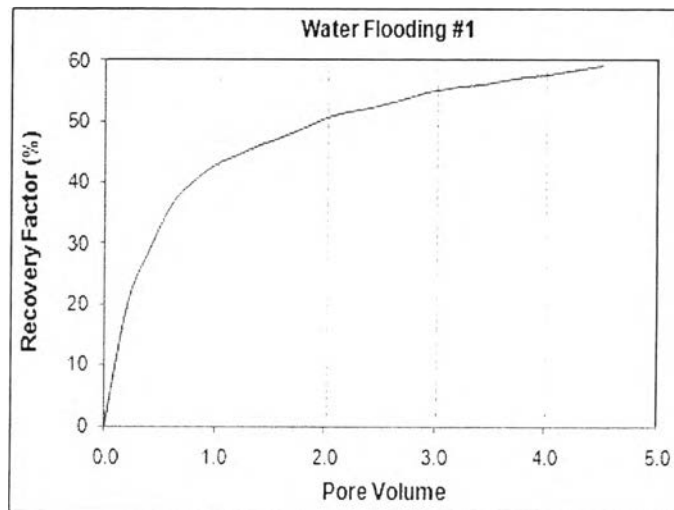


Figure A1 The simulation result of waterflooding with high permeability sand pack of 41.5 darcy and low oil viscosity of 440 cp.

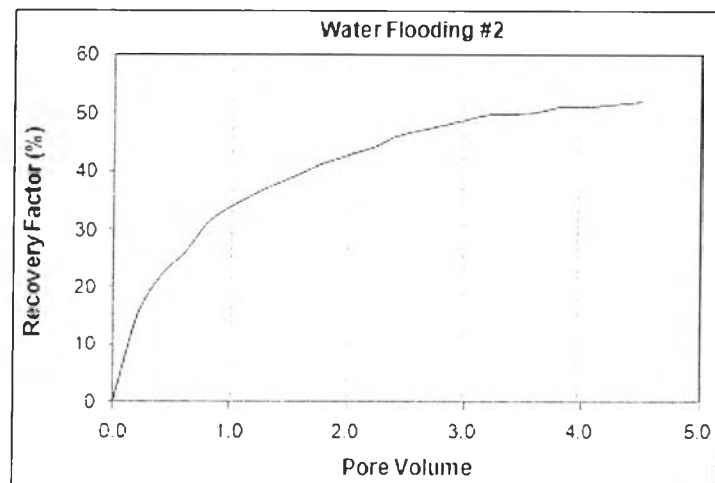


Figure A2 The simulation result of waterflooding with high permeability sand pack of 38.6 darcy and high oil viscosity of 1500 cp.

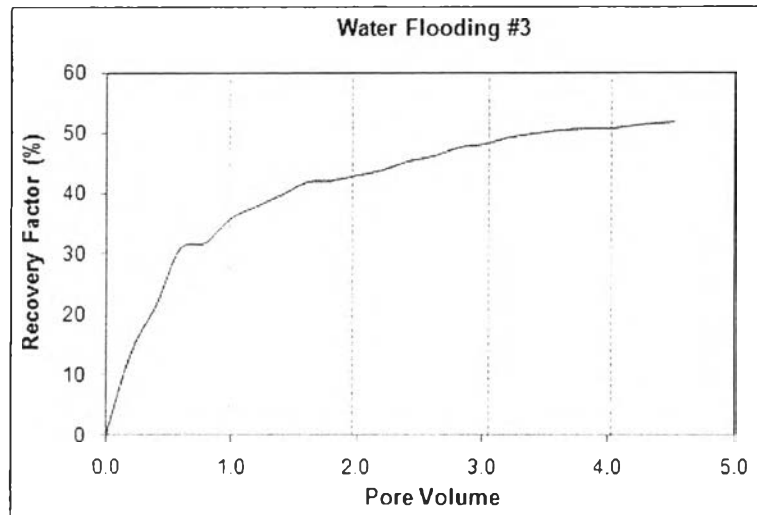


Figure A3 The simulation result of waterflooding with high permeability sand pack of 11.4 darcy and high oil viscosity of 1500 cp.

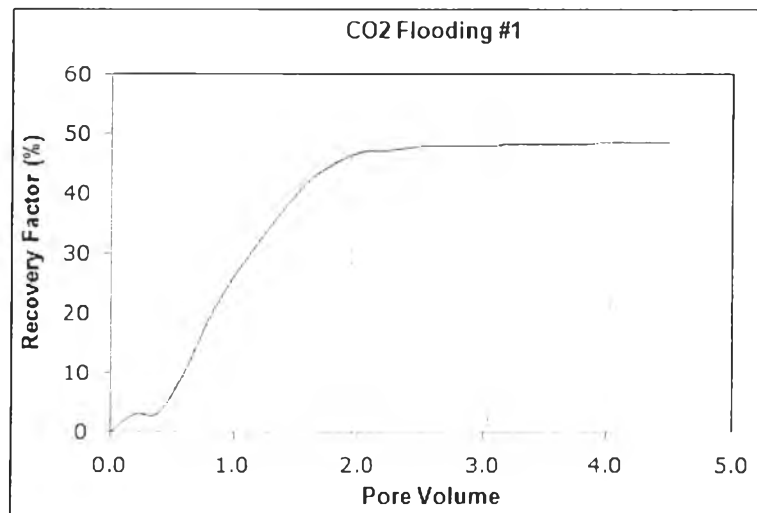


Figure A4 The simulation result of carbon dioxide flooding with high permeability sand pack of 41.5 darcy and low oil viscosity of 440 cp.

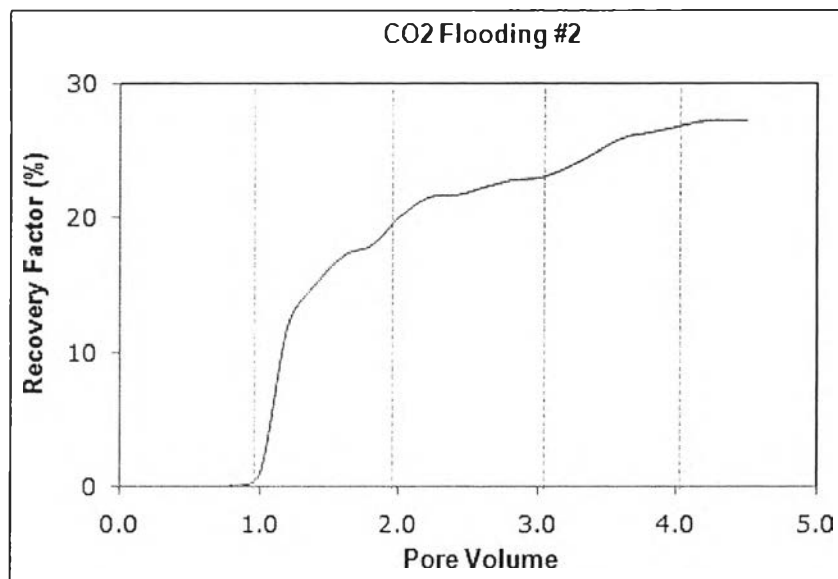


Figure A5 The simulation result of carbon dioxide flooding with high permeability sand pack of 38.6 dar γ and high oil viscosity of 1500 cp.

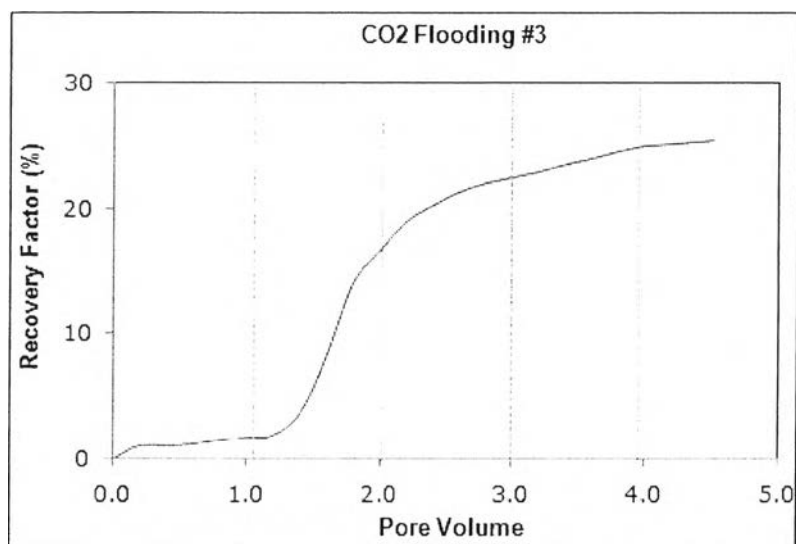


Figure A6 The simulation result of carbon dioxide flooding with low permeability sand pack of 11.4 darcy and high oil viscosity of 1500 cp.

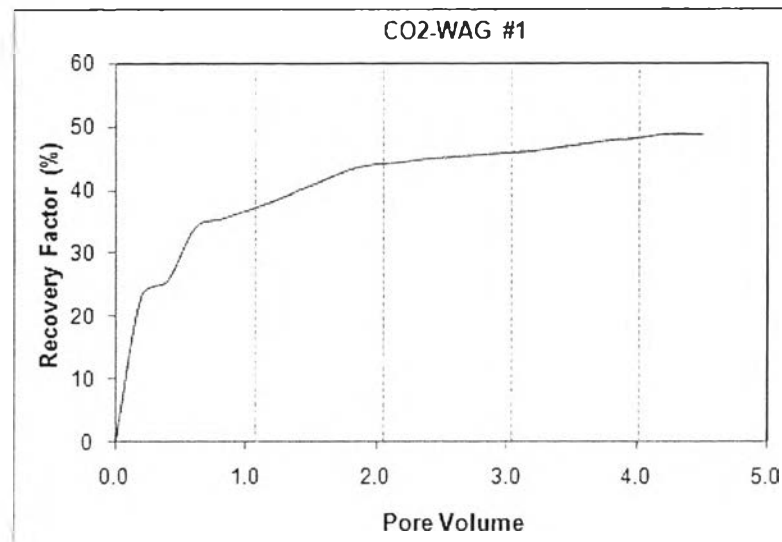


Figure A7 The simulation result of water-alternating-carbon dioxide with high permeability sand pack of 43 darcy, low oil viscosity of 440 cp and CO₂/water slug ratio of 1:1.

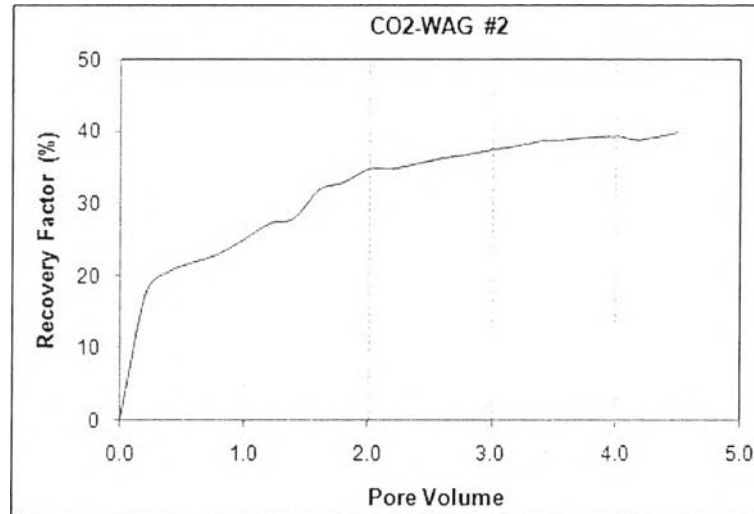


Figure A8 The simulation result of water-alternating-carbon dioxide with high permeability sand pack of 40.6 darcy, high oil viscosity of 1500 cp and CO₂/water slug ratio of 1:1.

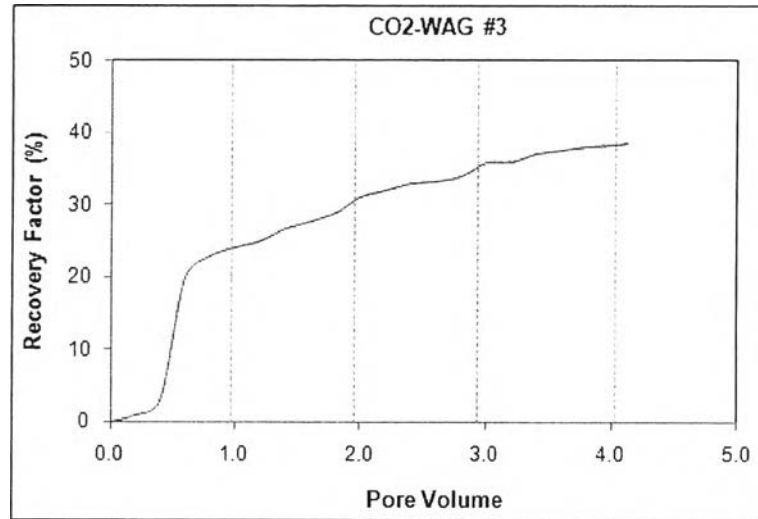


Figure A9 The simulation result of water-alternating-carbon dioxide with low permeability sand pack of 12.6 darcy, high oil viscosity of 1500 cp and CO₂/water slug ratio of 1:1.

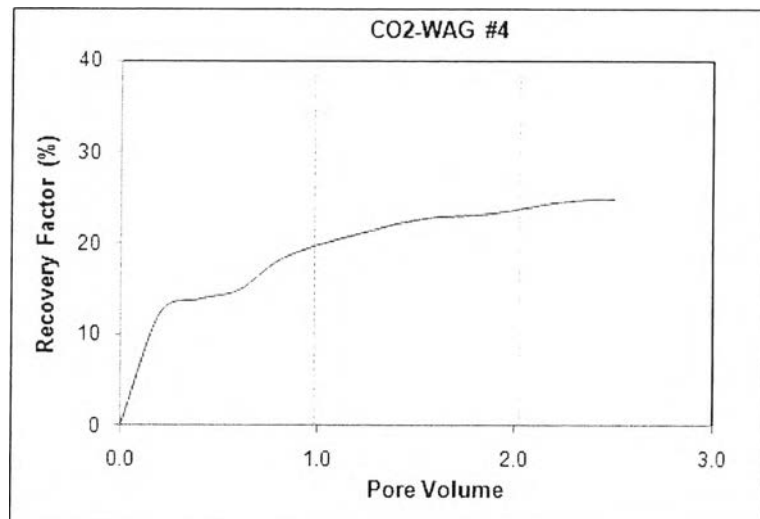


Figure A10 The simulation result of water-alternating-carbon dioxide with high permeability sand pack of 41.9 darcy, high oil viscosity of 1500 cp and CO₂/water slug ratio of 1:2.

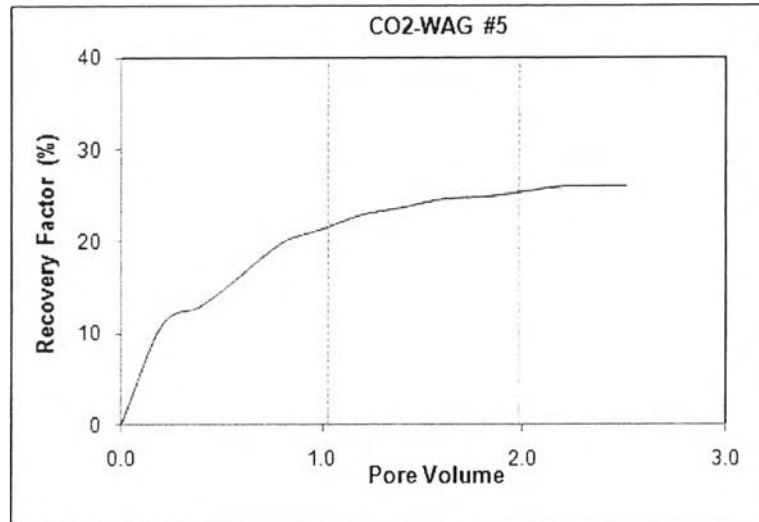


Figure A11 The simulation result of water-alternating-carbon dioxide with high permeability sand pack of 41.95 darcy, low oil viscosity of 1500 cp and CO₂/water slug ratio of 2:1.

Appendix B Simulation Steps of Three Recovery Methods

The following data are presented the simulation steps of waterflooding, carbon dioxide flooding and water-alternating-carbon dioxide, respectively.

B1 Simulation Steps of Waterflooding

- 1) Click Reservoir package.
- 2) Click Create grid.
- 3) Click Cartesian.
- 4) Insert I-direction, J-direction and K-direction equal to 1.
- 5) Insert block width for I-direction equals to 0.0257 meters.
- 6) Insert block width for J-direction equals to 0.0955 meters.
- 7) Click Reservoir package.
- 8) Click Edit grid.
- 9) Click Refinement wizard.
- 10) Select Current Fundamental Layer.
- 11) Select Cartesian option.
- 12) Insert 10 in the block of j-direction for refinement j-direction.
- 13) Click Reservoir package.
- 14) Click Edit grid.
- 15) Click Refinement wizard.
- 16) Select Hybrid option
- 17) Select Radial equals to 10 for refinement r-direction.
- 18) Select Along well equals to 4 for refinement j-direction.
- 19) Select Theta equals to 4 for refinement θ -direction.
- 20) Select K-direction in the wellbore parallel option.
- 21) Click Specify property

- 22) Insert porosity, permeability I, permeability J and permeability K equal to the value in the experimental data.
- 23) Click Components package.
- 24) Click Imex PVT Regions.
- 25) Select water and oil.
- 26) Insert reservoir temperature, reservoir pressure and API gravity equal to the value in the experimental data.
- 27) Click Rock-Fluid package.
- 28) Click Rock types.
- 29) Select Relative permeability correlations.
- 30) Select the function of unconsolidated sandstone.
- 31) Insert connate water saturation (S_{wc}), original oil saturation (S_{or}).
- 32) Click Initial Conditions package.
- 33) Select water, oil option.
- 34) Insert reference pressure and depth equals to 345 kpa and 0.01285 meters, respectively.
- 35) Insert depth of water-oil contact equals to 0.01285 meters.
- 36) Click Wells& Recurrent option.
- 37) Click Create new well.
- 38) Create water injection well.
- 39) Insert water injector as a name in the option of ID & type.
- 40) Click Constraints.
- 41) Select parameter as BHW reservoir water rate.
- 42) Insert injection rate as same as the experimental procedure.
- 43) Create production well.

- 44) Insert producer as a name in the option of ID & type.
- 45) Create production well.
- 46) Click Constraints.
- 47) Select parameter as Minimum bottom hole pressure.
- 48) Insert Minimum bottom hole equal to 200 kPa.
- 49) Click Wells& Recurrent option
- 50) Click Perforate.
- 51) Perforate water injector at (1,1,1/1,10,1/1,1,4).
- 52) Perforate producer at (1,1,1/1,1,1/1,1,1)
- 53) Click Wells & Recurrent.
- 54) Click Dates.
- 55) Select range of date.
- 56) Select steps as hour.
- 57) Save this file.
- 58) Run this file with IMEX module.
- 59) Create graph between pore volume and recovery factor from Result CMG.

B2 Simulation Steps of Carbon Dioxide Flooding

- 1) Click Reservoir package.
- 2) Click Create grid.
- 3) Click Cartesian.
- 4) Insert I-direction, J-direction and K-direction equal to 1.
- 5) Insert block width for I-direction equals to 0.0257 meters.
- 6) Insert block width for J-direction equals to 0.0955 meters.
- 7) Click Reservoir package.
- 8) Click Edit grid.

- 9) Click Refinement wizard.
- 10) Select Current Fundamental Layer.
- 11) Select Cartesian option.
- 12) Insert 10 in the block of j-direction for refinement j-direction.
- 13) Click Reservoir package.
- 14) Click Edit grid.
- 15) Click Refinement wizard.
- 16) Select Hybrid option
- 17) Select Radial equals to 10 for refinement r-direction.
- 18) Select Along well equals to 4 for refinement j-direction.
- 19) Select Theta equals to 4 for refinement θ -direction.
- 20) Select K-direction in the wellbore parallel option.
- 21) Click Specify property
- 22) Insert porosity, permeability I, permeability J and permeability K equal to the value in the experimental data.
- 23) Click Components package.
- 24) Click Imex PVT Regions.
- 25) Select miscible option.
- 26) Insert carbon dioxide density.
- 27) Insert the value of gas and solvent mixing parameter equals to zero (immiscible condition)
- 28) Insert reservoir temperature, reservoir pressure and API gravity equal to the value in the experimental data.
- 29) Click Rock-Fluid package.
- 30) Click Rock types.
- 31) Select Relative permeability correlations.

- 32) Select the function of unconsolidated sandstone.
- 33) Insert connate water saturation (S_{wc}), original oil saturation (S_{or}).
- 34) Click Initial Conditions package.
- 35) Select water, oil and gas option.
- 36) Insert reference pressure and depth equals to 345 kpa and 0.01285 meters, respectively.
- 37) Insert depth of water-oil contact equals to 0.01285 meters.
- 38) Click Wells & Recurrent option.
- 39) Click Create new well.
- 40) Create solvent injection well.
- 41) Insert solvent injector as a name in the option of ID & type.
- 42) Click Constraints.
- 43) Select parameter as BHS reservoir solvent rate.
- 44) Insert injection rate as same as the experimental procedure.
- 45) Create production well.
- 46) Insert producer as a name in the option of ID & type.
- 47) Create production well.
- 48) Click Constraints.
- 49) Select parameter as Minimum bottom hole pressure.
- 50) Insert Minimum bottom hole equal to 200 kPa.
- 51) Click Wells & Recurrent option
- 52) Click Perforate.
- 53) Perforate solvent injector at (1,1,1/1,10,1/1,1,4).
- 54) Perforate producer at (1,1,1/1,1,1/1,1,1)

- 55) Click Wells & Recurrent.
- 56) Click Dates.
- 57) Select range of date.
- 58) Select steps as hour.
- 59) Save this file.
- 60) Run this file with IMEX module.
- 61) Create graph between pore volume and recovery factor from Result CMG.

B3 Simulation Steps of Water-Alternating-Carbon Dioxide

- 1) Click Reservoir package.
- 2) Click Create grid.
- 3) Click Cartesian.
- 4) Insert I-direction, J-direction and K-direction equal to 1.
- 5) Insert block width for I-direction equals to 0.0257 meters.
- 6) Insert block width for J-direction equals to 0.0955 meters.
- 7) Click Reservoir package.
- 8) Click Edit grid.
- 9) Click Refinement wizard.
- 10) Select Current Fundamental Layer.
- 11) Select Cartesian option.
- 12) Insert 10 in the block of j-direction for refinement j-direction.
- 13) Click Reservoir package.
- 14) Click Edit grid.
- 15) Click Refinement wizard.
- 16) Select Hybrid option

- 17) Select Radial equals to 10 for refinement r-direction.
- 18) Select Along well equals to 4 for refinement j-direction.
- 19) Select Theta equals to 4 for refinement θ -direction.
- 20) Select K-direction in the wellbore parallel option.
- 21) Click Specify property
- 22) Insert porosity, permeability I, permeability J and permeability K equal to the value in the experimental data.
- 23) Click Components package.
- 24) Click Imex PVT Regions.
- 25) Select miscible option.
- 26) Insert carbon dioxide density.
- 27) Insert the value of gas and solvent mixing parameter equals to zero (immiscible condition)
- 28) Insert reservoir temperature, reservoir pressure and API gravity equal to the value in the experimental data.
- 29) Click Rock-Fluid package.
- 30) Click Rock types.
- 31) Select Relative permeability correlations.
- 32) Select the function of unconsolidated sandstone.
- 33) Insert connate water saturation (S_{wc}), original oil saturation (S_{or}).
- 34) Click Initial Conditions package.
- 35) Select water, oil and gas option.
- 36) Insert reference pressure and depth equals to 345 kpa and 0.01285 meters, respectively.
- 37) Insert depth of water-oil contact equals to 0.01285 meters.
- 38) Click Wells & Recurrent option.

- 39) Click Create new well.
- 40) Create water injection well.
- 41) Insert water injector as a name in the option of ID & type.
- 42) Click Constraints.
- 43) Select parameter as BHW reservoir water rate.
- 44) Insert injection rate as same as the experimental procedure.
- 45) Create solvent injection well.
- 46) Insert solvent injector as a name in the option of ID & type.
- 47) Click Constraints.
- 48) Select parameter as BHS reservoir solvent rate.
- 49) Insert injection rate as same as the experimental procedure.
- 50) Create production well.
- 51) Insert producer as a name in the option of ID & type.
- 52) Create production well.
- 53) Click Constraints.
- 54) Select parameter as Minimum bottom hole pressure.
- 55) Insert Minimum bottom hole equal to 200 kPa.
- 56) Click Dates
- 57) Select range of date
- 58) Select step as hour.
- 59) Click Wells
- 60) Click options
- 61) Set the constraints as same as the experimental procedure.
- 62) Click Wells & Recurrent option

- 63) Click Perforate.
- 64) Perforate solvent injector at (1,1,1/1,10,1/1,1,4).
- 65) Perforate producer at (1,1,1/1,1,1/1,1,1)
- 66) Click Wells & Recurrent.
- 67) Click Dates.
- 68) Select range of date.
- 69) Select steps as hour.
- 70) Save this file.
- 71) Run this file with IMEX module.
- 72) Create graph between pore volume and recovery factor from Result CMG.

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Proceedings:

1. Teerasukakul, W.; Torabi, F.; and Saiwan, C. (2013, April 23) Simulation of Waterflooding, Carbon Dioxide Flooding and Water-Alternating-Carbon Dioxide in Heavy Oil Reservoir: Comparative Evaluation. Proceedings of the 4th Research Symposium on Petrochemicals and Materials Technology and The 19th PPC Symposium on Petroleum, Petrochemicals, and Polymers, Bangkok, Thailand.
2. Teerasukakul, W.; Torabi, F.; and Saiwan, C. (2013, September 29-October 2) Simulation of Waterflooding, Carbon Dioxide Flooding and Water-Alternating-Carbon Dioxide in Heavy Oil Reservoir: Comparative Evaluation. The 16th Conference Process Integration, Modelling and Optimisation for Energy Saving and Pollution Reduction, Rhodes Island, Greece.