

REFERENCES

- ภมร ศรีสมบุญ. 2505. พืชสกุลส้ม, กสิกร. 35 (พฤษภาคม, 2505,) 243-251.
- มาตรฐานผลิตภัณฑ์อุตสาหกรรม, สำนักงาน. 2517. น้ำผลไม้: น้ำส้ม มอก 99-2517.
กรุงเทพ. กระทรวงอุตสาหกรรม
วิทยาศาสตร์, กรม. 2504. ข่าวกรมวิทยาศาสตร์. 31 (มกราคม, 2504,) 3-5.
- วิรดา ดิษยมณฑล. 2514. น้ำส้ม รายงานเอกสารฉบับที่ 171. พระนคร.
กรมวิทยาศาสตร์, กองวิทยาศาสตร์ชีวภาพ.
- Agarwal, H.C. 1970. Gravity-Flow Falling Film Evaporator. Chemical Age of India, 21:591-594.
- Bennett, C.O, and Myers, J.E. 1962. Momentum, Heat and Mass Transfer. New York: McGraw-Hill Book Co.Inc.
- Bielig, Hans. J., and Werner Joachim. 1973. Fruit Juice Processing. Agricultural Services Bulletin NO.13; Rome: Food and Agriculture Organization of the United Nations.
- Bird, R. Byron, Stewart, Warren E., and Lightfoot, Edwin N. 1960. Transport Phenomena. Tokyo: Toppan Co. Ltd.
- Borgstrom, Georg. 1968. Principles of Food Science. vol.1. 1st ed. New York: The Macmillan Company.
- Charm, Stanley E. 1971. The Fundamental of Food Engineering. 2nd ed. Connecticut: The Avi Publishing Co. Inc.
- Clarke, R.J. 1971. The Evaporation of Heat Sensitive Foodstuff Liquids. J. Appl. Chem. Biotechnol., 21: 349-350.
- Cruess, W.V. 1948. Commercial Fruit and Vegetable Products. 3rd ed. Pennsylvania: The Maple Press Co.

- Dinsmore, H.L., and Nagy, S. 1972. Colorimetric Furfural Measurement as an Index of Deterioration in Stored Citrus Juices. Journal of Food Science, 37: 768-770.
- Earle, R.L. 1966. Unit Operations in Food Processing. New South Wales: Pergamon Press Pty. Ltd.
- Fleming, A., and Hunter, G. 1970. New Developments in Film Evaporators. Chemical Processing (London), 16: 51-55.
- Gray, R.M. 1971. The Plate Evaporator. J. Appl.Chem.Biotechnol., 21: 359-362.
- Heid, J.L., and Joslyn, Maynard A. 1967. Fundamentals of Food Processing Operations. Connecticut: The Avi Publishing Co. Inc.
- Horwitz, William. 1970. Official Methods of Analysis of the Association of Official Analytical Chemists: 11th ed. Wisconsin: George Banta Co. Inc.
- Jacobs, Morris B. 1959. Chemical Analysis of Foods and Food Products. 3rd ed. New Jersey: D. Van Nostrand Co. Inc.
- Kern, Donal Q. 1969. Process Heat Transfer. Tokyo: McGraw-Hill Kogakusha, Ltd.
- Lime, B.J., and Cruse, R.R. 1972. Beverages from Whole Citrus Fruit Puree. Journal of Food Science, 37: 250-252.
- Lowe, Clifford M., and King, Judson C. 1974. Slush Evaporation: A New Method for Concentration of Liquid Foods. Journal of Food Science, 39: 248-253.

- McCabe, Warren L., and Smith, Julian C. 1956. Unit Operations of Chemical Engineering. New York: McGraw-Hill Book Co. Inc.
- Peleg, M., and Mannheim, C.H. 1970. Production of Frozen Orange-Juice Concentrate from Centrifugally Separated Serum and Pulp. Journal of Food Science, 35: 649-651.
- Perry, John H. 1963. Chemical Engineers' Handbook. 4th ed. Tokyo: McGraw-Hill Book Co.
- Robbins, R.H., and Gresswell, D.M. 1971. The Evaporation of Fruit Juices. J. Appl. Chem. Biotechnol., 21: 363-365.
- Saravacos, G.D. 1970. Effect of Temperature on Viscosity of Fruit Juice and Purees. Journal of Food Science, 35: 122-125.
- Shah, Basit H., and Darby Ron. 1973. The Effect of Surfactant on Evaporative Heat Transfer in Vertical Film Flow. Int. J. Heat Mass Transfer, 16: 1889-1903.
- Sinclair, W.B. 1961. The Orange Its Biochemistry and Physiology. The University of California Printing Department.
- Tressler, D.K., and Joslyn, M.A. 1961. Fruit and Vegetable Juice Processing Technology. Connecticut: The Avi Publishing Company, Inc.
- Vogel, Arthur I. 1947. A Text-book of Quantitative Inorganic Analysis. London: Lowe and Brydone Printers, Ltd.

- Widmer, F., and Giger A. 1970. Residence Time Control in Thin-film Evaporators. Chemical and Process Engineering, November: 63-65.
- Wiegand, J. 1971. Falling-Film Evaporators and Their Applications. J. Appl. Chem. Biotechnol., 21: 351-358.
- Woollen, Anthony. 1969. Food Industries Manual. 20th ed. London: Leonard Hill.

APPENDIX

Appendix A

EXPERIMENTAL DATA

Part I Calibration of Meters:

Triplicated data were obtained and only the average values were reported here.

1. Calibration of hot-water orifice meter

Trial No.	Manometer reading cm.Hg	Average time to collect certain amount of water, min/sec
1	0.4	9/30.25
2	0.8	5/2.7
3	1.5	3/37.85
4	2.1	3/2.9
5	2.7	2/41.8
6	3.5	2/22.5
7	4.2	2/11.0
8	5.1	1/59.15
9	6.6	1/43.65
10	8.3	1/33.05
11	9.4	1/27.7
12	10.7	1/21.5
13	11.7	1/17.75
14	12.9	1/14.75
15	14.0	1/11.8

Weight of empty container 1.8 kg

Weight of container filled with water 34.7 kg

2. Calibration of cold-water orifice meter

Trial NO.	Manometer reading cm.Hg	Average time to collect certain amount of water min./sec.
1	0.85	4/14.3
2	1.3	3/32.6
3	2.15	2/48.7
4	3.1	2/21.7
5	4.05	2/6.0
6	5.5	1/47.6
7	6.4	1/40.75
8	7.35	1/34.25
9	8.4	1/28.4
10	9.4	1/23.75
11	10.1	1/20.8
12	11.3	1/15.9
13	11.8	1/14.5

Weight of empty container 1.8 kg

Weight of container filled with water 34.7 kg

3. Calibration of rotameter

Rotameter reading	Average cc. of fruit juice collected in 1 min.
1	10
2	37.5
3	62
4	87
5	115
6	140
7	168
8	196
9	215
10	240
11	265
12	291
13	320
14	341
15	370

Part II Physical Properties of Orange Juice Determination

1. Determination of density at various concentration at room temperature

concn Bx	wt. of bottle gm.	wt. of bottle + sample 25 ml., gm.
0	25.1562	50.0759
5	20.6434	45.9914
10	26.6652	52.5862
15	24.0045	50.2544
20	29.0276	55.7814
25	25.1562	52.6311
30	32.6967	60.5164
35	25.1602	53.6954
40	20.1559	49.3649
45	26.8783	56.4916
48.5	31.4570	61.1114

2. Determination of viscosity at various concentration
at room temperature

concn Bx	Average reading *	
	speed 60	speed 30
0	-	-
5	0.4	0.2
10	0.6	0.4
15	0.7	0.35
20	1.0	0.43
25	1.3	0.6
30	1.8	1.2
35	3.7	2.3
40	6.8	3.9
45	11.3	6.9
48.5	16.2	9.6

* the average reading was obtained from triplicated data.

3. Determination of specific heat at various concentration

concn, Bx.	fruit juice		hot water		temp. after mixing °C
	weight, gm	temp, °C	weight, gm	temp, °C	
0	410	29.0	170	55	36.5
5	500	37.6	130	62	42.8
10	500	39.0	132.5	65	44.6
15	500	36.4	127.5	68.2	43.2
20	500	31.2	117.5	70	39.2
25	500	27.2	92.5	52.5	31.6
30	315	29.0	122.5	67	40.5
35	360	28.0	100	60.2	36.5
40	450	26.5	100	61	34.0
45	420	18.6	90	62.8	28.5

4. Determination of Brix concentration of sugar solution

concn. w/w	5	10	15	20	25	30	35	40	45	50
Bx. reading	5	10	15.2	19.8	24.9	30.1	34.9	40	44.9	50.1

Part III Experimental Runs

Experimental run NO.1 Feed rate 0.24 l/m, Steam pressure 3 psi.

Time	Steam temp.		Hot water				Vapor temp.				Cooling water				Vac. mm.Hg		
	in	out	temp.		manometer		condenser NO.1		condenser NO.2		temp. cond.2		temp. cond.1			manometer	
			in	out	from	to	in	out	in	out	in	out	in	out		from	to
15:40	-	-	88	75	14.5	16.5	-	-	-	-	25	25	25	25	10	20.5	680
15:45	102	96	"	74	"	"	45	45	44	26	"	"	"	26	10	20.5	680
15:50	"	"	"	75	"	"	46	44	44	26	"	"	"	27	10	20.5	680
15:55	"	"	"	"	"	"	47	43	43	26	"	"	"	27.5	10	20.5	680
16:00	"	"	"	78	"	"	48	34	26	26	"	"	"	"	10	20.5	660
16:05	"	"	"	81	"	"	49	27	26	26	"	"	"	"	10	20.5	650
16:10	"	"	"	83.5	"	"	52.5	26	25.5	25	"	"	"	"	10	20.5	640
16:15	"	"	90	85	"	"	53.0	26	"	"	"	"	"	"	10	20.5	640
16:20	"	"	90	85.5	"	"	53.0	26	"	"	"	"	"	10	20.5	640	
16:30	"	"	"	86	"	"	53.5	26	"	"	"	"	"	10	20.5	640	
16:35	"	"	"	86	"	"	53.5	26	"	"	"	"	"	10	20.5	640	
16:40	"	"	"	86	"	"	53.5	26	"	"	"	"	"	10	20.5	640	

Feed temp. 40°C Brix 9

Feed quantity 14.7 kg

Product temp. 46°C Brix 16

Product quantity 3.2 kg

Total time consumed 1 hr.

Condensate quantity 6.5 kg

Experimental run NO.2 Feed rate 0.265 l/m , Steam pressure 3 psi

Time	Steam temp.		Hot water				Vapor temp.				Cooling water						Vac. mm.Hg
	in	out	temp.		manometer		condenser NO.1		condenser NO.2		temp, cond2		temp. cond.1		manometer		
			in	out	from	to	in	out	in	out	in	out	in	out	from	to	
14.30	-	-	91	88	13	18	-	-	-	-	25.5	25.5	25.5	25.5	10.2	20.2	680
14.35	102	93.5	91	88	"	"	45	45	44	25.5	"	"	"	26	"	"	680
14.40	"	"	90	88.5	"	"	46	42	40	"	"	"	"	27	"	"	680
14.45	"	"	90	88.5	"	"	47	33	33.5	25.5	25.5	"	26	28.5	"	"	670
14.50	"	"	91	88	"	"	49	34	33	"	"	"	"	"	"	"	660
14.55	"	"	91	87	"	"	51	36	30	"	"	"	"	"	"	"	650
15.00	"	"	91	87	"	"	53	37	29	"	"	"	25.5	28	"	"	640
15.05	"	"	90	87	"	"	53.5	37.5	28.5	"	"	"	"	29	"	"	640
15.10	"	"	90	87	"	"	54	38	"	"	"	"	"	29.5	"	"	635
15.15	"	"	90	87	"	"	54.5	34	27	"	"	"	"	"	"	"	630
15.20	"	"	90	87.5	"	"	"	30.5	26.5	"	"	"	"	"	"	"	630
15.25	"	"	90	89	"	"	"	31	"	"	"	"	"	"	"	"	630
15.30	"	"	91	87.5	"	"	55	31.5	"	"	"	"	"	"	"	"	630
15.35	"	"	90	87	"	"	54.5	35	27.5	"	"	"	"	"	"	"	630

Feed temp. 50°C Brix 9 Feed quantity 14.72 kg

Product temp. 35°C Brix 26 Product quantity 5.0 kg

Condensate quantity 9.7 kg

Total time consumed 1 hr. 6 min.

Experimental run NO.3 Feed rate 0.29 l/m, Steam pressure 3 psi

Time	steam temp.		Hot water				Vapor temp.				Cooling water				Vac. mm.Hg		
	in	out	temp.		manometer		condenser NO.1		condenser NO.2		temp. cond.2		temp. cond.1			manometer	
			in	out	from	to	in	out	in	out	in	out	in	out		from	to
15.00	-	-	89	88	12	19	-	-	-	-	25.5	25.5	26	26	10.5	19.8	
15.05	102	92	90	88	"	"	43	40	38	25.5	"	26	26	27	"	"	
15.10	"	"	90	88.5	"	"	44	42	43.5	"	"	26.5	26	28	"	"	670
15.15	"	"	89	86.5	"	"	45	46	"	"	"	27	27	29	"	"	670
15.20	"	91.5	88	85	"	"	51	47	45	"	"	26.5	26	30	"	"	650
15.25	"	"	89	85	"	"	52.5	49	49	28.0	"	26	26	30.5	"	"	640
15.30	"	"	89	86	"	"	52	51	50	25.5	"	26	25.5	30	12	19	640
15.35	"	"	90	88.5	"	"	52	49	49	"	"	26	25.5	31	13	17.5	640
15.40	"	"	90	86	"	"	53.5	51	51	28.5	"	26.5	25.5	32.5	13	17.5	640
15.45	"	"	89	85.5	"	"	53.5	49.5	49	28	"	26	26	32	13	17.5	640
15.50	"	"	90	87	"	"	54	52	52.5	"	"	26	26	32.5	14	16.5	640
15.55	"	"	90	87	"	"	54	52.5	52	"	"	26	26	32.5	14	16.5	640

Feed temp. 50°C Brix 11 Feed quantity 13.2 kg

Product temp. 37.5°C Brix 28.5 Product quantity 4.8 kg

Condensate quantity 8.4 kg

Total time consumed 58 min.

Experimental run NO.4 Feed rate 0.318 l/m, Steam pressure 3 psi

Time	steam temp.		Hat water				Vapor temp.				Cooling water				Vac. mm.Hg		
			temp.		manometer		condenser NO.1		condenser NO.2		temp. cond.2		temp. cond.1			manometer	
	in	out	in	out	from	to	in	out	in	out	in	out	in	out		from	to
13.40	102	96	94	88	12.5	18.5	-	-	-	-	26.5	26	26	27	9.5	20.5	
13.45	"	94	92	88	"	"	47	46.5	47	28	26.5	26	26	29.0	"	"	670
13.50	"	93	90	88	"	"	49	48	48	29	"	27	27	30	"	"	660
13.55	"	92	89	87	"	"	51.5	41	41	28	"	27	27	30.5	"	"	650
14.00	"	92	88	83.5	"	"	54	46.5	45.5	28	"	27	27	30.5	"	"	630
14.05	"	92	89	86	"	"	54.5	45	33	27	"	26.5	27	30.5	"	"	630
14.10	"	92	89	87	"	"	54	42	32.5	27	"	26.5	27	30.5	"	"	630
14.15	"	92	89	87	"	"	54.5	38	30.5	26.5	"	26.5	27	30.5	"	"	630
14.20	"	92	89	87	"	"	54.5	38	30.5	26.5	"	26.5	27	30.5	"	"	630

Feed temp. 60°C Brix 10 Feed quantity 9.65 kg

Product temp 40°C Brix 25 Product quantity 3.5 kg

Total time consumed 42 min. Condensate quantity 6.1 kg

Experimental run NO.5 Feed rate 0.344 l/m , Steam pressure 3 psi

Time	Steam temp.		Hot water				Vapor temp.				Cooling water				Vac. mm.Hg		
	in out		temp.		manometer		condenser NO.1		condenser NO.2		temp. cond.2		temp. cond.1			manometer	
			in	out	from	to	in	out	in	out	in	out	in	out		from	to
16.30	102	95	90	88	13	18	-	-	-	-	27.5	27.5	27.5	28	9.5	21	675
16.35	"	"	90	89	"	"	45	38	35	38	"	27.5	"	29	"	"	675
16.40	"	"	90	88	"	"	47	39.5	39	38	"	"	28	30	"	"	675
16.45	"	"	90	87	"	"	48	43.5	43	29	"	"	28	31	"	"	660
16.50	"	94.5	89	86	"	"	50	46.5	46	30.5	"	28	28	31.5	"	"	650
16.55	"	"	89	88	"	"	52.5	52.5	50.5	30.5	"	28	28	31.5	"	"	640
17.00	"	"	90	88.5	"	"	55	52	52.5	30.5	"	28	28	32	"	"	630
17.05	"	"	91	87	"	"	55	51	49.5	29.5	"	28	28	31.5	"	"	630
17.10	"	"	89	86	"	"	55	50	45.5	28	"	27.5	28	31.5	"	"	630
17.15	"	"	89	86	"	"	55	50	47.5	30	"	27.5	28	31.5	"	"	630
17.20	"	93.5	88	85	"	"	55.5	50	47.5	30.5	"	27.5	28	32	"	"	630
17.25	"	"	89	84	"	"	55	45	34	30.5	"	27.5	28	30.5	"	"	630
17.30	"	"	89	85	"	"	54	37	31	30.5	"	28	28	29.5	"	"	630
17.35	"	"	88	86	"	"	54	38	31	30.5	"	27.5	28	29.5	"	"	630
17.40	"	"	89	85	"	"	54	37	31	30.5	"	28	28	29.5	"	"	630
17.45	"	"	88	84	"	"	54	37	31	30.5	"	27.5	28	29.5	"	"	630
17.50	"	"	88	86	"	"	54	37	31	30.5	"	27.5	28	29.5	"	"	630

Feed temp. 50°C Brix 10 Feed quantity 16.35 kg

Product temp. 40°C Brix 24 Product quantity 7.1 kg

Total time consumed 1 hr 20 min. Condensate quantity 9.25 kg

Experimental run NO.6 Feed rate 0.37 l/min , Steam pressure 3 psi

Time	steam temp.		Hot water				Vapor temp.				Cooling water				Vac. mm.Hg		
	in	out	temp.		manometer		condenser NO.1		condenser NO.2		temp. cond.2		temp. cond.1			manometer	
			in	out	from	to	in	out	in	out	in	out	from	to			
14.50	102	98	91	80	15.2	16.7	--	--	--	--	28.5	28.5	28.5	29	13.5	17.5	660
14.55	"	97.5	91	81	"	"	49	46	45	29	"	29	29	31	"	"	660
15.00	"	98	90	80	"	"	49	46	46.5	29	"	30	29	32.5	"	"	660
15.05	"	"	90	81	"	"	50	49	48.5	30	"	30	30.5	33.5	"	"	650
15.10	"	"	91	81	"	"	51	50	50	31	"	30	29.5	34	"	"	650
15.15	"	"	90	79	"	"	55	42	45.5	30	"	30	29	33.5	"	"	630
15.20	"	"	90	79.5	"	"	56	39	40	30	"	30	28	33	"	"	620
15.25	"	"	91	82	"	"	55.5	35	30	29	"	23.5	28.5	31.5	"	"	630
15.30	"	"	91	83.5	"	"	55.5	34.5	29.5	28	"	28.5	28.5	32	"	"	620
15.35	"	"	90	81	"	"	56	34.5	29.5	28	"	28.5	28.5	32.5	"	"	620
15.40	"	"	91	81	"	"	56	34.5	29.5	28	"	28.5	28.5	32.5	"	"	620

Feed temp. 70°C Brix 10.5 Feed quantity 14.55 kg
 Product temp. 46°C Brix 16.8 Product quantity 8.975 kg
 Total time consumed 50 min. Condensate quantity 5.5 kg

Experimental run NO.7 Feed rate 0.265 l/m, Steam pressure 3 psi

Time	steam temp.		Hot water				Vapor temp.				Cooling water				Vac. mm.Hg		
	in	out	temp.		manometer		condenser NO.1		condenser NO.2		temp. cond.2		temp. cond.1			manometer	
			in	out	from	to	in	out	in	out	in	out	in	out		from	to
13.40	120	90.5	88	86	12.5	16.5	-	-	-	-	27	28.5	28	29	10.5	20	660
13.45	"	90	87	86	"	"	45	30	29	26	"	29	28.5	29.5	"	"	660
13.50	"	90	88	87	"	"	49	31	31.5	26	"	30.5	27	29	"	"	660
13.55	"	90	86	84.5	"	"	50	45	43.5	26.5	"	28	27	29	"	"	650
14.00	"	90	86	84.5	"	"	51	50	50.5	28	"	26	28	30.5	"	"	660
14.05	"		87	84.5	"	"	53	49	45	27	"	26	27.5	30.5	"	"	640
14.10	"	89	88	85	"	"	54.5	39	31	27	"	26	27	30	"	"	630
14.15	"	90.5	86	83	"	"	55	45	43.5	27	"	27	27	30.5	"	"	630
14.20	"	91.5	88	85.5	"	"	55	39	31	27	"	26.5	27	30	"	"	630
14.25	"	91.5	88	85	"	"	55	40.5	31.5	27	"	26.5	27	30	"	"	630
14.30	"	91.5	88	85	"	"	55	42	32	27	"	26.5	27	30	"	"	630
14.35	"	92	88	85.5	"	"	55.5	44	33.5	27	"	27	27	30.5	"	"	630
14.40	"	92	88	85	"	"	55.5	44	33.5	27	"	27	27	30.5	"	"	630

Feed temp. 60°C Brix 12.2 Feed quantity 14.4 kg
 Product temp. 38°C Brix 28 Product quantity 6.25 kg
 Total time consumed 1 hr Condensate quantity 8.05 kg

*

Part IV Analysis of Orange Juice1. Total titratable acidity

a. Juice before processing: 10 ml. juice titrate with 0.102N. NaOH

Exp. run NO	1	2	3	4	5	6	7
ml. NaOH	16.5	6.75	9.6	6.4	6.4	5.5	8.6

b. Juice after processing: 10 ml. concentrate juice diluted to 20 ml. and pipetted 10 ml. to titrate with 0.102N. NaOH

Exp. run NO	1	2	3	4	5	6	7
ml. NaOH	15.5	10.8	14.4	9.3	7.8	4.6	10.7

2. Vitamin C content

a. Juice before processing: 10 ml. juice titrate with 0.00808 N. Iodine solution.

Exp. run NO	1	2	3	4	5	6	7
ml. Iodine soln	4.15	4.60	3.45	5.30	3.80	3.30	5.70

b. Juice after processing: 25 ml. concentrate juice was titrated with the same Iodine solution, but no present of blue color occurred.

* ml. reported here was obtained from triplicated data

Appendix B

SAMPLE OF CALCULATIONS

Part I Calibration of Meters

1. Calibration of hot-water, cold-water orifice meter

(Trial NO.1 for hot-water orifice meter was illustrated here)

$$\begin{aligned} \text{wt. of water flowed during the recorded time} &= 34.7 - 1.8 \\ &= 32.9 \quad \text{kg} \end{aligned}$$

$$\text{the time recorded} = 9 \text{ min } 30.3 \text{ sec}$$

$$\text{Therefore, the flow rate of water} = \frac{32.9(60)}{(9 \times 60 + 30.3)} = 3.46 \text{ kg/min}$$

2. Calibration of rotameter (Trial NO.1)

$$\text{flow of juice} = 10 \text{ cc}$$

$$\text{time} = 1 \text{ min}$$

$$\text{Therefore, the flow rate of juice} = \frac{10}{1000} = 0.01 \text{ liter/min}$$

Part II Physical Properties of Orange Juice Determination

1. Determination of density (for concn 5 Bx.)

$$\text{wt. of bottle} = 20.6434 \text{ g}$$

$$\text{wt. of bottle + sample 25 ml.} = 45.9914 \text{ g}$$

$$\text{The wt. of sample 25 ml.} = 25.3480 \text{ g}$$

$$\text{Then, the density of juice} = 25.3480/25$$

$$= 1.0139 \text{ g/ml}$$

2. Determination of viscosity (for concn 5 Bx)

For speed 60

average reading = 0.4

factor for speed 60 rpm = 1

Then, the viscosity = $0.4 \times 1 = 0.4$ centipoise

For speed 30

average reading = 0.2

factor for speed 30 rpm = 2

Then, the viscosity = $0.2 \times 2 = 0.4$ centipoise

3. Determination of specific heat (s)

3.1 To find the heat capacity of thermos

wt. of water = 410 gm

specific heat of water = 1

Let the heat capacity of the thormos be m

The temp. increase of water and thermos = $36.5 - 29$

= 7.5°C

The temp. of hot water used = 170 gm and

its temp. = 55°C

The temp. decrease of hot water = $55 - 36.5$

= 18.5°C

The heat balance of the mixing is

$$(410 \times 1 + m)(7.5) = 170 \times 1 \times 18.5$$

$$m = 9.322 \text{ Cal}/^{\circ}\text{C}$$

3.2 To find the specific heat of orange juice at each concentration (For the sample of concn 5 Bx)

Let s be the specific heat of the sample

wt. of sample	=	500 g
temp. of sample	=	37.6° C
wt. of hot water	=	130 g
temp. of hot water	=	62° C
temp. after mixing	=	42.8° C

The heat balance is

$$\begin{aligned}
 (500s + 9.322)(42.8 - 37.6) &= 130(62 - 42.8) \\
 s &= \left[\frac{130(19.2) - 9.322}{5.2} \right] / 500 \\
 &= 0.9413 \text{ Cal/g}^\circ\text{C}
 \end{aligned}$$

Part III Experimental Run (sample shown here was for exp. run no.1)

1. The mass balance

1.1 Overall mass balance

Feed	=	14.7 kg
Product	=	8.2 kg

The overall mass balance around the evaporating chamber yields,

$$\text{calculated condensate} = 14.7 - 8.2 = 6.5 \text{ kg}$$

$$\text{But the measured condensate} = 6.5 \text{ kg}$$

$$\text{Therefore, the percentage less} = 0 \%$$

1.2 Component mass balance

1.2.1 solid content balance

Feed was 14.7 kg with 9° Brix

$$\text{Therefore, the solid content in foed} = \frac{14.7 \times 9}{100} = 1.323 \text{ kg}$$

Product was 8.2 kg with 16° Brix

Therefore, the solid content in product = $\frac{8.2 \times 16}{100} = 1.31$ kg

Hence, the solid content loss = $1.323 - 1.31$
 = 0.031 kg
 = $\frac{0.031(100)}{1.323} = 2.34\%$

1.2.2 water content balance

Water in feed = $14.7 - 1.323 = 13.377$ kg
 water in product = $8.2 - 1.31 = 6.89$ kg
 Therefore, the water in condensate = $13.377 - 6.89 = 6.487$ kg

2. Evaporation/concentration ratio

The evaporation/concentration ratio, $e = \frac{C_P}{C_F}$
 = $\frac{16}{9} = 1.78$
 or $e = \frac{F}{P}$
 = $\frac{14.7}{8.2} = 1.79$

3. The heat balance

Overall heat balance around the evaporating chamber

Let the reference temp. be 0°C

According to the definition of specific heat

$$q = ms \Delta t$$

The enthalpy of feed, $q_1 = 14.7 \times 1000 \times 0.96(40-0)$
 = 558.6×10^3 Cal.

The enthalpy of concentrate juice, $q_2 = 8.2 \times 1000 \times 0.91(46-0)$
 = 342.7×10^3 Cal

From the vacuum readings, the temperatures were correlated,
the mean temp. was then calculated as:

$$\text{min. vacuum } 640 \text{ mm.Hg} = 47^{\circ}\text{C}$$

$$\text{max. vacuum } 680 \text{ mm.Hg} = 55.5^{\circ}\text{C}$$

$$\text{Then, the average saturated vapor temp. (T}_v\text{)} = \frac{55.5 - 47}{\ln \frac{55.5}{47}} = 51.5^{\circ}\text{C}$$

From the steam table, the enthalpy of saturated steam is
619, 502 Cal/kg

Therefore, the enthalpy of sat^d. water vapor,

$$\begin{aligned} q_3 &= 6.5 \times 619,502 \\ &= 4026.7 \times 10^3 \text{ Cal} \end{aligned}$$

The enthalpy transferred from the hot water to the evaporating chamber,

$$\begin{aligned} q_4 &= (4026.7 + 342.7 - 558.6) \times 10^3 \\ &= 3810.8 \times 10^3 \text{ Cal} \end{aligned}$$

$$\text{Total time consumption} = 1 \text{ hr}$$

$$\begin{aligned} \text{Then, the rate of enthalpy transferred} &= 3810.8 \times 10^3 / 3600 \\ &= 1.059 \times 10^3 \text{ Cal/sec} \end{aligned}$$

4. To find heat transfer coefficient of hot-water

According to the Seban and Shimazaki's correlation equation for
flow in closed conduit with constant the heat transfer coeff. is
expressed as:

$$\frac{h_{loc} D}{k} = 5 + 0.025 (\text{RePr})^{0.8}$$

$$\text{For rectangular conduit, } D = 4 r_H$$

$$\text{where } r_H = \text{hydraulic radius}$$

$$= \frac{14.6 \times 2.0}{(2 \times 14.6 + 2 \times 2)} = 0.88 \text{ cm}$$

$$k = \text{thermal conductivity of water at } T_h \\ = 1.646 \times 10^{-3} \text{ Cal/sec cm}^2 \text{ } ^\circ\text{C (Kern)}$$

$$T_h = \text{average temp. of hot water} \\ = 84.6^\circ \text{C}$$

$$\text{Re} = \text{Reynold's number} = \frac{\rho u D}{\mu} = \frac{4 r_H u \rho}{\mu} \\ = \frac{4 r_H}{\mu} \frac{w}{A}$$

$$\mu = \text{viscosity of water at } T_h \\ = 0.3375 \times 10^{-2} \text{ poise (g/cm sec) (Perry)}$$

$$\text{Therefore, Re} = \frac{4 \times 0.88 \times 10.5 \times 1000}{0.3375 \times 10^{-2} \times 60 \times 14.6 \times 2.0} \\ = 6250$$

$$\text{Pr} = \text{Prandt's number} = \frac{c_p \mu}{k}$$

$$c_p = \text{specific heat at } T_h \\ = 1.00383 \text{ Cal/g}^\circ\text{C (Perry)}$$

$$\text{Therefore, Pr} = \frac{1.00383 \times 0.3375 \times 10^{-2}}{1.646 \times 10^{-3}} \\ = 2.06$$

$$\text{Consequently, } \frac{hD}{k} = 5 + 0.025(6250 \times 2.06)^{0.8} \\ = 5 + 48.5 = 53.5$$

Therefore, the heat transfer coefficient,

$$h = \frac{53.5 \times 1.646 \times 10^{-3}}{4 \times 0.88} \\ = 0.025 \text{ Cal/sec cm}^2 \text{ } ^\circ\text{C}$$

5. To find the temperature difference within the hot-water region

Referring to Fig.2, p.27 ., the rate of heat transfer from the hot water to the evaporating chamber,

$$q_4 = h A \Delta t = h A (T_h - T'_s)$$

The total surface area for heat transfer,

$$A = 14.6 \times 175 = 2555 \text{ cm}^2$$

$$\text{Then, } T_h - T'_s = \frac{1.06 \times 10^3}{0.025 \times 2555} = 16.6^\circ\text{C}$$

6. To find the temperature difference within the heated plate

According to the Fourier's equation, the rate of heat transfer from the hot water to the evaporating chamber,

$$q_4 = k A \Delta t = \frac{k A}{\Delta x} (T'_s - T_s)$$

where k = thermal conductivity of the heated plate

$$= 9.4 \text{ Btu/hr ft } ^\circ\text{F}$$

$$= 0.039 \text{ Cal/sec cm } ^\circ\text{C}$$

$$A = 2555 \text{ cm}^2$$

$$\Delta x = \text{thickness of the plate} = 0.64 \text{ cm}$$

$$\text{Therefore, } T'_s - T_s = \frac{1.06 \times 10^3 \times 0.64}{0.039 \times 2555} = 6.8^\circ\text{C}$$

7. Temperature difference between the plate surface (T_s) and the vaporization temp. (T_v)

From the experimental data,

$$T_h - T_v = 84.6 - 51.5 = 33.1^\circ\text{C}$$

$$\begin{aligned} \text{Therefore, } T_s - T_v &= (T_h - T_v) - (T_h - T_s) - (T'_s - T_s) \\ &= 33.1 - 16.6 - 6.8 = 9.7^\circ\text{C} \end{aligned}$$

8. The theoretical mass flow-rate of concentrate juice

According to the theoretically derived equation as shown in chapter 3, the relationship between the initial mass flow rate and the final mass flow rate is expressed as:

$$\left(\Gamma_0^{4/3} - \Gamma_L^{4/3} \right) = 0.925 \frac{(T_s - T_v)}{\lambda} \left(\frac{\rho^2 k g \cos \theta}{\mu} \right)^{1/3}$$

where Γ_0 is the initial mass flow rate per unit width, calculated from data of rotameter reading and feed density.

$$\text{Hence, } \Gamma_0 = \frac{0.24 \times 1000 \times 1.032}{60 \times 14.6}$$

$$= 0.2827 \quad \text{g/sec cm}$$

$$\text{and } \Gamma_0^{4/3} = 0.1856$$

Γ_L is the final mass flow rate per unit width.

It was calculated from the collected weight of concentrate juice divided by the total time consumed and the plate width.

Therefore, experimental mass flow rate of concentrate juice

$$= \frac{8.2 \times 1000}{14.6 \times 3600} = 0.1560 \quad \text{g/sec cm}$$

$$T_s - T_v = 9.7^\circ \text{C}$$

$$\lambda = 6.195 \times 10^2 \quad \text{Cal/g}$$

$$f = 1.045 \quad (\text{from average concn}) \quad \text{g/ml}$$

$$k = 1.534 \times 10^{-3} \quad \text{Cal/sec cm } ^\circ\text{C} \quad (\text{Perry})$$

(based on the assumption that the thermal conductivity of orange juice was equal to that of water)

$$g = 981 \quad \text{cm/sec}^2$$

$$\cos \theta = \cos 60^\circ = \frac{1}{2}$$

$$\mu = 0.55 \times 10^{-2} \quad \text{g/cm sec}$$

$$\begin{aligned}
 \text{When, } \int_0^{4/3} \int_0^{4/3} &= \frac{0.925(9.7)}{6.195 \times 10^2} \left[\frac{(1.045)^2 (1.534 \times 10^{-3})^3 981}{2 \times 0.55 \times 10^{-2}} \right]^{1/3} \\
 &= 0.1785 \\
 \int_0^{4/3} &= \int_0^{4/3} \dots 0.1785 = 0.1856 - 0.1785 \\
 &= 0.0071
 \end{aligned}$$

Therefore the theoretical mass flow-rate per unit width of concentrated juice,

$$\int_0^{4/3} = 0.0245 \text{ g/sec cm}$$

Part IV Analysis of Juice

1. Total titratable acidity (example a of run no.1)

Normality of NaOH	=	0.102
ml. of NaOH used	=	16.5
Molecular wt. of citric	=	192.12
Therefore, citric content	=	$\frac{0.102(16.5)}{100} \times \frac{192.12}{3} \times 10$
	=	1.08 g/100 ml.

2. Vitamin C content (example a. of run no.1)

Normality of Iodine solution	=	0.00808
From standard Iodine solution		
1 ml. 0.01 N	=	0.88 mg ascorbic acid
which is equal to		1.2376 ml of 0.00808 N.
ml. of Iodine solution used	=	4.15
Therefore, vitamin C content	=	$\frac{0.88 \times 4.15}{1.2376} \text{ mg ascorbic/10 ml}$
	=	29.5 mg/100 ml

VITA

Miss Suwanna Roongtanapirom received her Bachelor Degree of Science in the field of Food Technology from Faculty of Science, Chulalongkorn University in 1970.

She has been joining the teaching staff in the Department of Chemical Technology where she graduated since then. The subjects which she used to handle in collaboration with other senior lecturers are: Raw Materials for Food Processing, Food and Nutrition, Food Chemistry, Food Evaluation, Food Processing, and Food Quality Control.

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